

ANALYSIS OF THERMAL BOUNDARY LAYER FLOW OVER A VERTICAL PLATE WITH ELECTRICAL CONDUCTIVITY AND CONVECTIVE SURFACE BOUNDARY CONDITIONS

O.J. Fenuga¹ I.O. Abiala² and S.O. Salawu³

^{1,2} Department of Mathematics, University of Lagos, Akoka, Lagos, Nigeria

E-mails: ofenuga@unilag.edu.ng

iabiala@unilag.edu.ng

³ Department of Mathematics, University of Ilorin, Ilorin, Nigeria

E-mail: kunlesalawu@yahoo.com

Abstract

This paper analyses the thermal boundary layer flow over a vertical plate with electrical conductivity and convective surface boundary conditions. Transforming the governing nonlinear partial differential equations into a set of coupled non-linear ordinary differential equations by using the usual similarity transformation, the resulting coupled nonlinear ordinary differential equations are solved numerically by Runge- Kutta fourth order method with shooting technique. The behaviour and properties of thermo physical parameters in the fluid flow on the structure of the velocity and temperature fields are presented graphically and discussed.

Keywords: Electrical conductivity, Thermal boundary layer, Vertical plate, Convective surface boundary conditions.

*- Corresponding Author

1. Introduction

The study of heat transfer is an integral part of natural convection flow and a class of boundary layer theory. The quantity of heat transferred is highly dependent on the fluid motion within the boundary layer.

Convective heat transfer studies are very important in processes involving high temperatures such as gas turbines, nuclear plants, thermal energy storage, etc. The solution for the laminar boundary layer problem on a horizontal flat plate was obtained by Heinrich Blasius [1] and since then it has been a subject of current research. Cortell [4] in his work presented a numerical solution of the Classical Blasius Flat-Plate Problem using a Runge-Kutta algorithm for higher order initial value problem. Gabriella [6] used an iterative transformation method for the solution of boundary layer problem of a non-Newtonian power law fluid flow along a moving plate surface. There is a drag coefficient dependence on the velocity ratio and on the power law exponent. He [7] worked on a simple perturbation approach to Blasius equation. In his paper, he coupled the iteration method with the perturbation method to solve the well-known Blasius equation. Bataller [3] presented a numerical solution for the combined effects of thermal radiation and convective surface heat transfer on the laminar boundary layer about a flat-plate in a uniform stream of fluid (Blasius flow) and about a moving plate in a quiescent ambient fluid.

The study of an incompressible viscous and electrically conducting fluid in the presence of a uniform transverse magnetic field was investigated by Watunade and Pop [13]. Shrama and Gurminder [12] looked at the effect of temperature dependent electrical conductivity on steady natural convection flow of a viscous incompressible low Prandtl ($Pr \ll 1$) electrically conducting fluid along an isothermal vertical non-conducting plate in the presence of transverse magnetic field and exponentially decaying heat generation. Aziz [2] investigated a similarity solution for laminar thermal boundary layer over a flat-plate with a convective

surface boundary condition. Makinde and Sibanda [11] conducted a study on magneto hydrodynamic mixed convective flow and heat and mass transfer past a vertical plate in a porous medium with constant wall suction.

Makinde [10] studied analysis of non-newtonian reactive flow in a cylindrical pipe. Cortell [5] investigated a similarity solution for flow and heat transfer of a quiescent fluid over a nonlinearly stretching surface.

Makinde and Olanrewaju [8] conducted a study on the effects of buoyancy force on thermal boundary layer over a vertical plate with convective surface boundary conditions. In Olanrewaju[9], it was assumed that the lower surface of the plate is in contact with the hot fluid while a stream of cold fluid flows steadily over the upper surface with a heat source that decayed exponentially. This paper is an extension of [8] with buoyancy force, convective surface boundary condition and electrical conductivity parameters. The numerical solutions of the resulting momentum and the thermal similarity equations are reported for representative values of thermo physical parameters characterizing the fluid convective process.

2. Materials and Methods

Consider a two-dimensional steady incompressible fluid flow coupled with heat transfer by convection over a vertical plate. A stream of cold fluid at temperature T_∞ moving over the right surface of the plate with a uniform velocity U_∞ while the left surface of the plate is heated by convection from a hot fluid at temperature T_f , which provides a heat transfer coefficient h_f (see Fig.3.1) .The x -axis is taken along the plate and y -axis is normal to the plate. Magnetic field of intensity B_o is applied in the y - direction. It is assumed that the external field is zero. Incorporating the Boussinesq's approximation within the boundary layer, the governing equations of continuity, momentum and energy equations according to [8] are respectively given as:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad (1)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2} + g\beta(T - T_\infty) - \frac{\sigma^* B_0^2}{\rho} u \quad (2)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} \quad (3)$$

where u and v are the x (along the plate) and the y (normal to the plate) components of the velocity respectively; g is the acceleration due to gravity; x, y are the Cartesian coordinates, B_0 is the Magnetic field intensity, β is the coefficient of thermal expansion, ρ is the density of the fluid, ν is the Kinematic viscosity, α is the coefficient of thermal conductivity, T is the temperature of the fluid, σ^* is the electrical conductivity and it is variable with temperature as given below

$$\sigma^* = \frac{\sigma}{1 + \varepsilon \theta} \quad (4)$$

ε is the electrical conductivity parameter. All prime symbols denotes differentiation with respect to η

The velocity boundary conditions can be expressed as:

$$u(x, 0) = v(x, 0) = 0 \quad (5)$$

$$u(x, \infty) = U_\infty \quad (6)$$

The boundary conditions at the plate surface and far into the cold fluid may be written as:

$$-k \frac{\partial T}{\partial y}(x, 0) = h_f [T_f - T(x, 0)] \quad (7)$$

$$T(x, \infty) = T_\infty$$

(8)

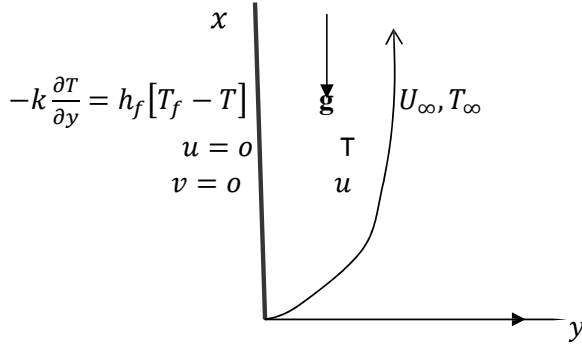


Fig 1 Flow Configuration and coordinate system

Introducing the stream function $\psi(x,y)$ such that

$$\left. \begin{aligned} u &= \frac{\partial \psi}{\partial y} \\ v &= -\frac{\partial \psi}{\partial x} \end{aligned} \right\} \quad (9)$$

$$\text{where } \Psi = (x, y) = x \sqrt{\frac{U_{\infty} V}{x}} f(\eta), \quad U_{\infty} = ax \quad (10)$$

The similarity variable η , a dimensionless stream function $f(\eta)$ and temperature $\theta(\eta)$ are given as

$$\eta = y \sqrt{\frac{U_{\infty}}{vx}}, \quad u = ax f'(\eta), \quad v = -\sqrt{av} f(\eta), \quad \theta = \frac{T - T_{\infty}}{T_f - T_{\infty}} \quad (11)$$

Thus, the continuity equation (1) is satisfied with u and v of equations (11). Using (11), equations (2) and (3) are transformed into a set of coupled non-linear ordinary differential equation as

$$f'''(\eta) - f'(\eta)^2 + f(\eta) f''(\eta) - \frac{M}{1 + \varepsilon \theta} f'(\eta) + Gr \theta(\eta) = 0 \quad (12)$$

$$\theta''(\eta) + Pr f(\eta) \theta'(\eta) = 0 \quad (13)$$

The boundary conditions (5), (6), (7) and (8) reduced to

$$f(0) = f'(0) = 0, \quad f'(\eta) = 1 \quad \text{as } \eta \rightarrow \infty \quad (14)$$

$$\theta'(0) = -Bi [1 - \theta(x, 0)], \quad \theta(\infty) = 0 \quad (15)$$

where $Gr = \frac{g\beta(T_f - T_\infty)}{\alpha x^2}$ is the dimensionless Grashof number, $M = \frac{\sigma\beta_o^2}{\rho a}$ is the magnetic parameter, $Pr = \frac{\nu}{\alpha}$ is the Prandtl number and $Bi = -\frac{h}{k}\sqrt{\frac{\nu}{a}}$ is the Biot number.

It is assumed that equations (12) and (13) have a similarity solution where the parameters Gr and Bi are defined as constants.

Solving the governing boundary layer equations (12) and (13) with the boundary conditions (14) and (15) numerically using Runge-Kutta fourth order method along with shooting technique and implemented on Maple 17. The step size of 0.001 is used to obtain the numerical solution correct to four decimal places as the criterion of the convergence.

3. Results and Discussion

Numerical calculations have been carried out for different values of the thermo physical parameters controlling the fluid dynamics in the flow region.

4. Tables and Figures

Table 4.1: Computations Showing Comparison of the Makinde (2010) and the Present Result

M = Gr = 0 and Pr =0.72				
Makinde 2010			Present Work	
Bi	$-\theta'(0)$	$\theta(0)$	$-\theta'(0)$	$\theta(0)$
0.05	0.0428	0.1447	0.0428	0.1447
0.10	0.0747	0.2528	0.0747	0.2528
0.20	0.1139	0.4035	0.1139	0.4035
0.40	0.1700	0.5750	0.1700	0.5750
0.60	0.1981	0.6699	0.1981	0.6699
0.80	0.2159	0.7302	0.2159	0.7302
1.00	0.2282	0.7718	0.2282	0.7718
5.00	0.2791	0.9442	0.2791	0.9442
10.00	0.2871	0.9713	0.2871	0.9713
20.00	0.2913	0.9854	0.2913	0.9854

Source: Maple 17 Output

Table 4.1 shows the comparison of Makinde's work (2010) with the present work for Prandtl number $Pr=0.72$ and it is noted that there is a perfect agreement in the absence of Grashof number G_r . Table 4.2, illustrates the values of the skin-friction coefficient $f'(0)$ and the local Nusselt number $-\theta'(0)$ for various values of embedded parameters.

Table 4.2: Computational table showing $f''(0)$, $-\theta'(0)$ and $\theta(0)$

Pr	M	Gr	ε	Bi	$f''(0)$	$-\theta'(0)$	$\theta(0)$
0.72	0.1	0.1	0.1	0.1	0.0780	0.0684	0.3157
1	0.1	0.1	0.1	0.1	0.0739	0.0704	0.2959
3	0.1	0.1	0.1	0.1	0.0613	0.0767	0.2335
0.72	0.1	0.1	0.1	0.1	0.0780	0.0684	0.3157
0.72	1	0.1	0.1	0.1	0.0348	0.0602	0.3977
0.72	3	0.1	0.1	0.1	0.0231	0.0574	0.4260
0.72	0.1	0.1	0.1	0.1	0.0780	0.0684	0.3157
0.72	0.1	1	0.1	0.1	0.3053	0.0744	0.2565
0.72	0.1	3	0.1	0.1	0.6182	0.0779	0.2207
0.72	0.1	0.1	0.1	0.1	0.0780	0.0684	0.3157
0.72	0.1	0.1	1	0.1	0.0798	0.0686	0.3144
0.72	0.1	0.1	3	0.1	0.0825	0.0688	0.3122
0.72	0.1	0.1	0.1	0.1	0.0780	0.0684	0.3157
0.72	0.1	0.1	0.1	1	0.1360	0.1934	0.8066
0.72	0.1	0.1	0.1	10	0.15452	0.2405	0.9760

Source: Maple 17 Output

The Graphs below Show the Velocity and the Temperature Profiles at Various Parameters Values

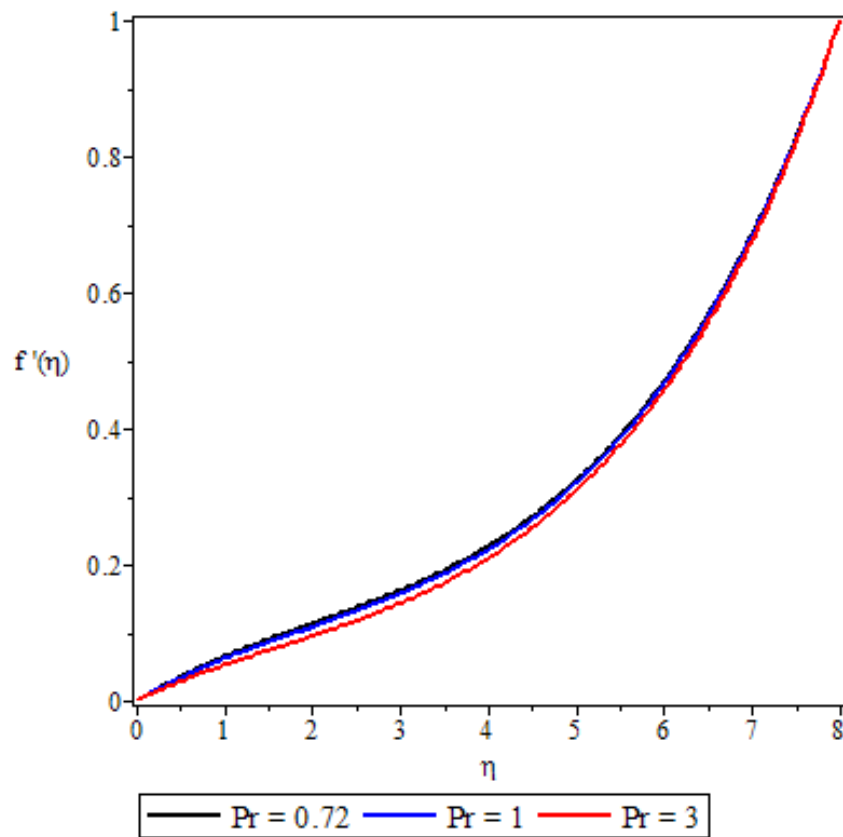


Fig. 4.1: Velocity profile for Pr

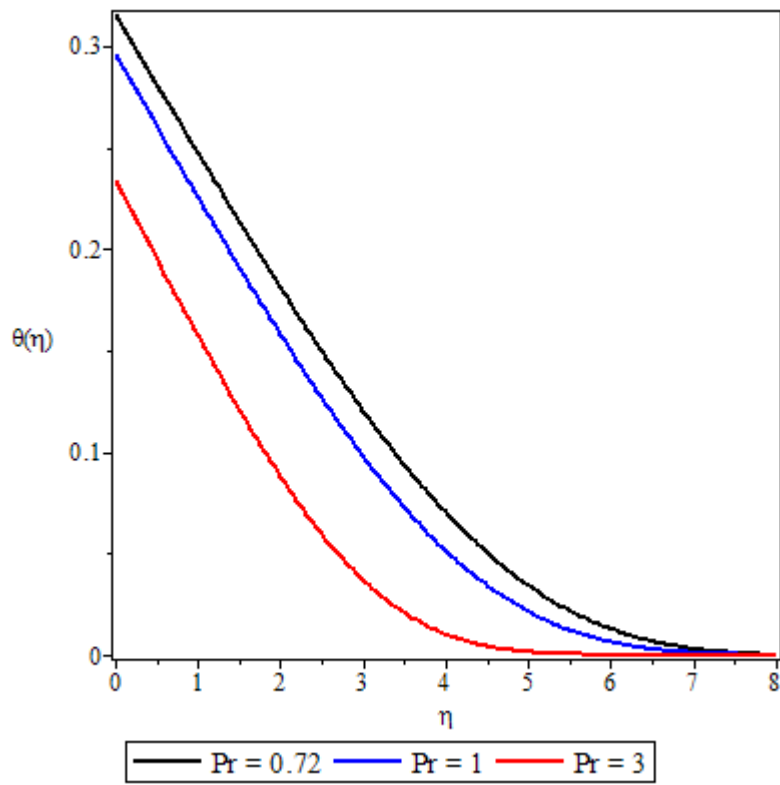


Fig. 4.2: Temperature profile for Pr

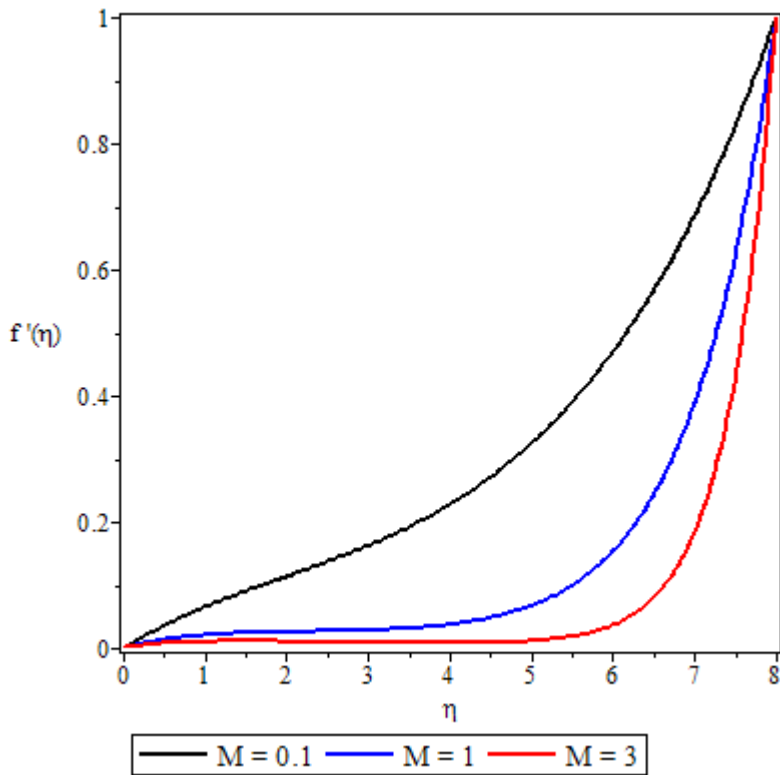


Fig. 4.3 :Velocity profile for M

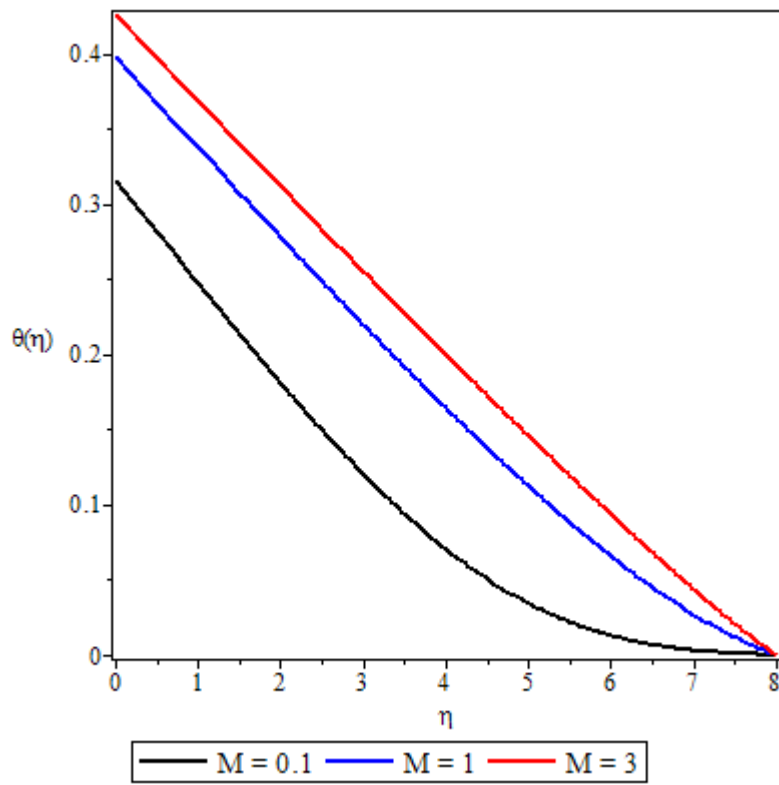


Fig. 4.4 :Temperature profile for M

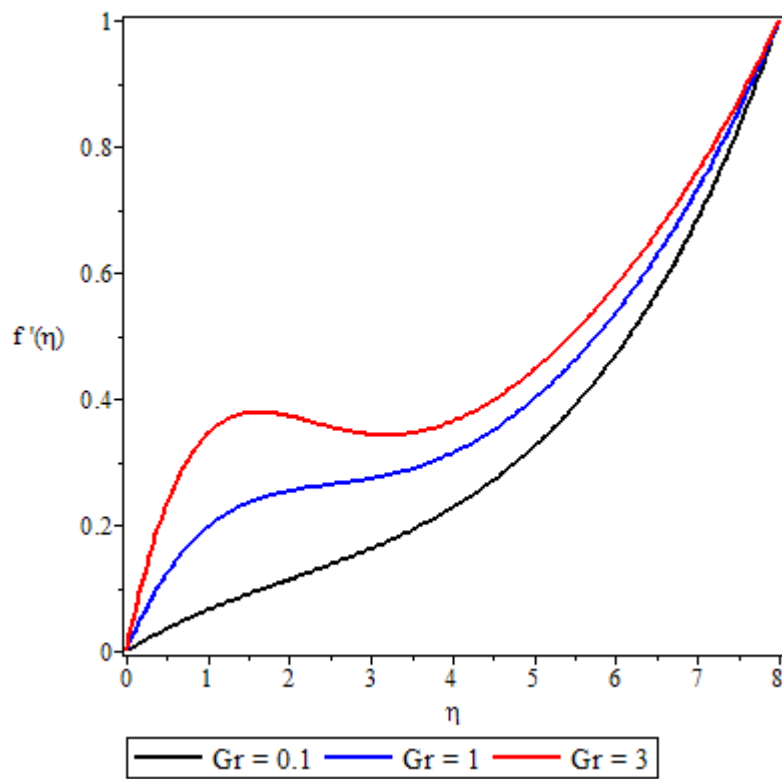


Fig. 4.5 :Velocity profile for Gr

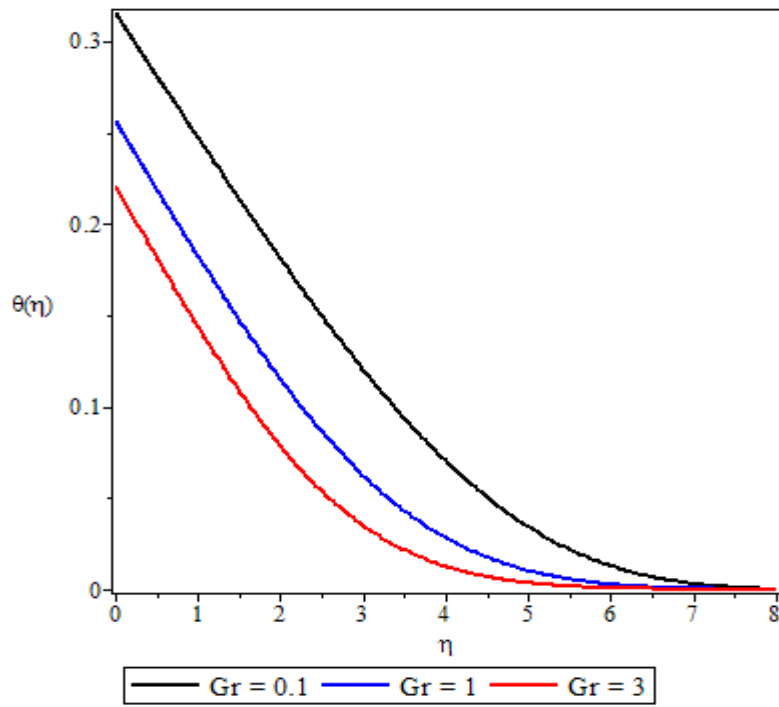


Fig. 4.6 :Temperature profile for Gr

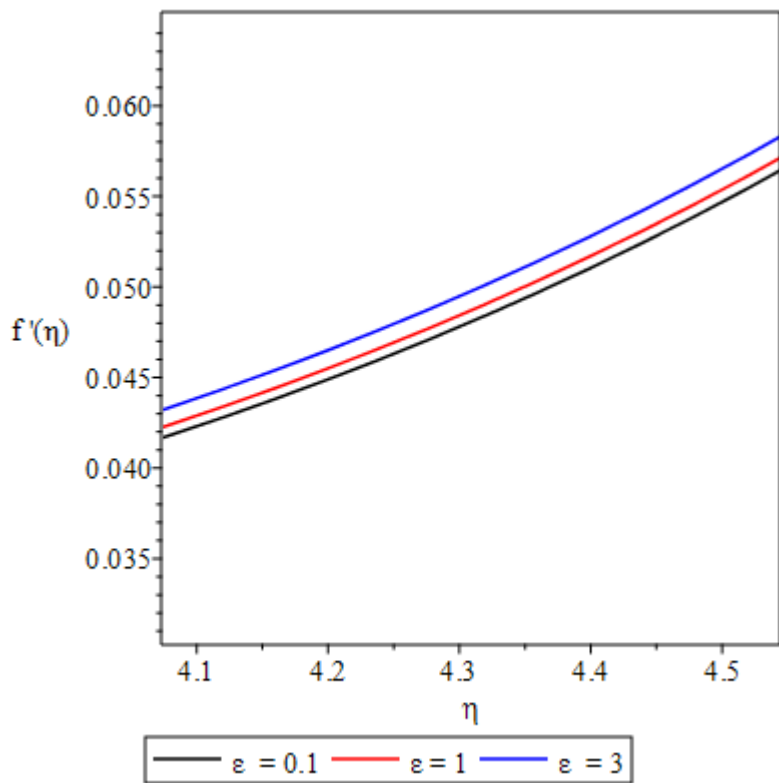


Fig. 4.7 :Velocity profile for ε

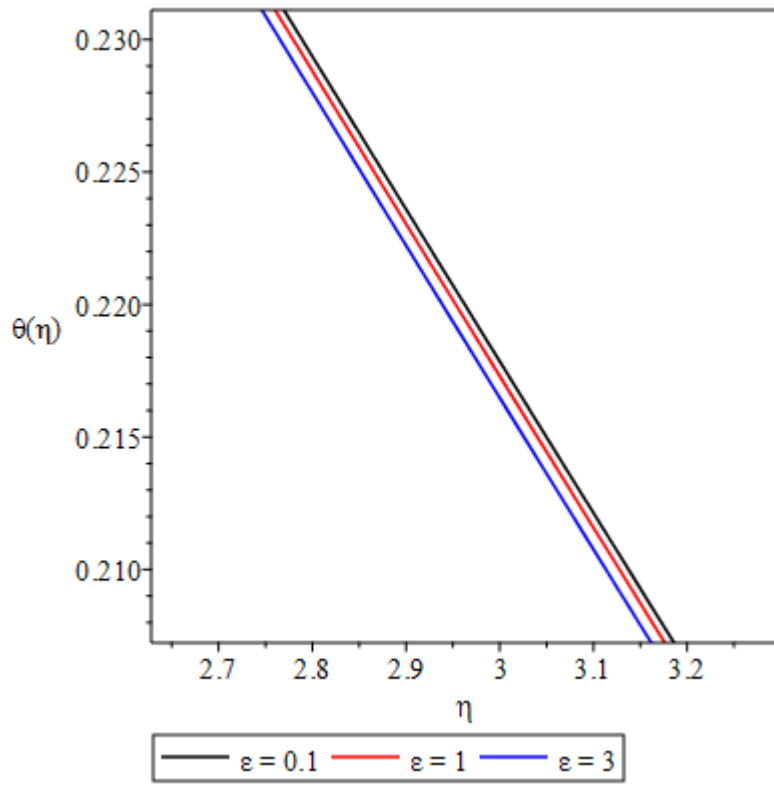


Fig.4.8 :Temperature profile for ε

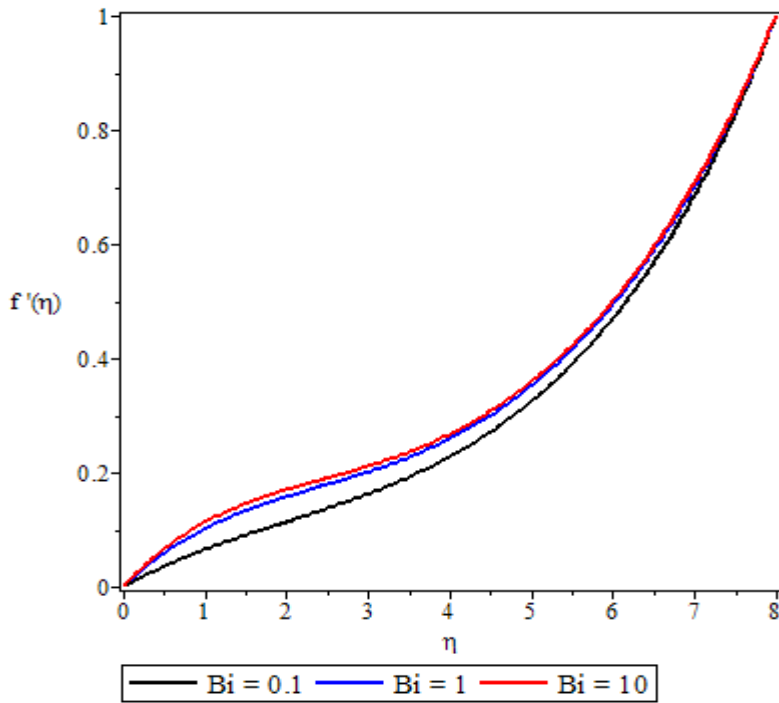


Fig. 4.9 :Velocity profile for Bi

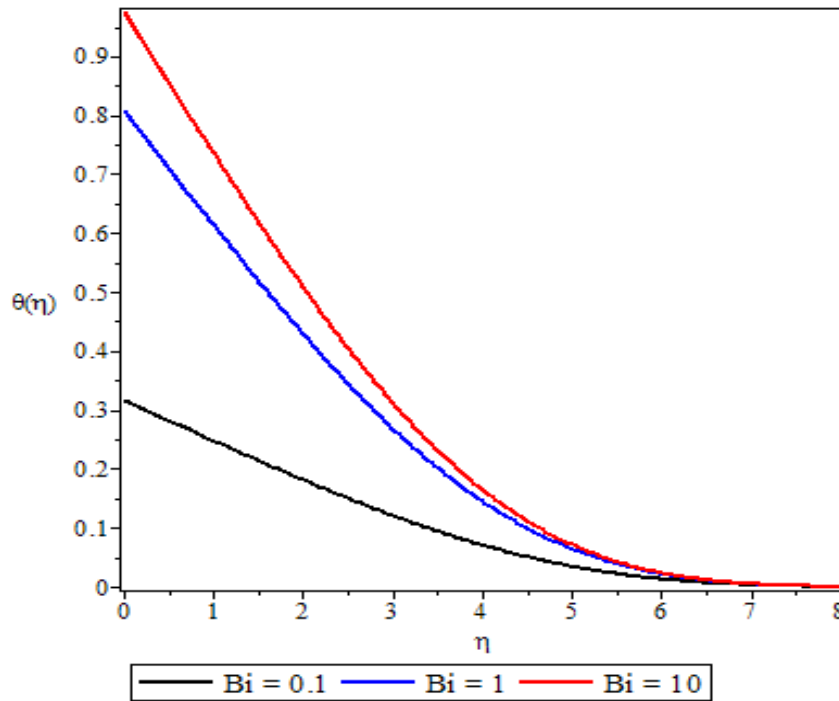


Fig. 4.10 : Temperature profile for B_i

From Table 4.2 and Fig. 4.5, 4.7 and 4.9, it is observed that the skin-friction and the rate of heat transfer at the plate surface increases with an increase in local Grashof number Gr , electrical conductivity parameter ε and convective surface heat transfer parameter B_i . It is also observed that for values of $Gr > 0$ as in Fig.4.6 there is decrease in the temperature profile which corresponds to the cooling problem. The cooling problem is often encountered in engineering applications; for example, in the cooling of electronic components and nuclear reactors.

However, in Fig. 4.1 and Fig.4.3, an increase in the Prandtl number Pr and magnetic field parameter M decreases the skin-friction but increases the rate of heat transfer at the plate surface. This is attributed to the fact that as the prandtl number decrease, the thermal boundary layer thickness increases, causing reduction in the temperature gradient $\theta'(0)$ at the surface of the plate.

In Fig. 4.2, the temperature gradient reduces at the surface because low prandtl number has high thermal conductivity, causing the fluid to attain higher temperature thereby reducing the

heat flux at the surface. Moreover, for such low Prandtl number, the velocity boundary layer is inside the thermal boundary layer and its thickness reduces as Prandtl number decreases and so the fluid motion is confined in more and more thinner layer near the surface and thereby experiencing drag increase (skin-friction) by the fluid. In other words there is more straining motion inside velocity boundary layer resulting in the increase of skin-friction coefficient. It is also observed from table 4.2 that increase in magnetic field intensity, the skin-friction coefficient decreases the rate of heat transfer near the surface; hence the surface experiences reduction in drag.

Figures 4.1, 4.3, 4.5, 4.7 and 4.9 show that the fluid velocity is zero at the plate surface and increases gradually away from the plate towards the free stream value satisfying the boundary conditions. Also, figures 4.2, 4.4, 4.6, 4.8 and 4.10 show that the fluid temperature is maximum at the plate surface and decreases exponentially to zero value far away from the plate satisfying the boundary conditions.

5. Conclusion

From the numerical solutions and graphical representations, increasing the Prandtl number and the Grashof number tend to reduce the thermal boundary layer thickness. Fluid temperature increases with increase in magnetic field intensity and decreases with increase in electrical conductivity parameter. Fluid velocity increases with increase in electrical conductivity parameter while it decreases with increase in magnetic field intensity.

Thermal boundary layer thickness increases with an increase in Biot numbers B_i and decreases with an increase in Grashof Gr and Prandtl Pr numbers. Thus, convective surface heat transfer enhances thermal diffusion while an increase in the Prandtl number slows down the rate of thermal diffusion within the boundary layer. Fluid temperature increases due to increase in magnetic field intensity while it decreases due to increase or decrease in electrical conductivity parameter.

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Appendix

```
> restart
> with(ODETools) :
> with(student) :
> with(plots) :
> with(plottools) :
> inf := 8 :
> equ1 := diff(f(η), η$3) - diff(f(η), η) + f(η) · diff(f(η), η$2) -  $\frac{m}{1 + \varepsilon \cdot \theta(\eta)}$ 
    · diff(f(η), η) + Gr · θ(η) = 0
    equ1 :=  $\frac{d^3}{d\eta^3} f(\eta) - \left( \frac{d}{d\eta} f(\eta) \right) + f(\eta) \left( \frac{d^2}{d\eta^2} f(\eta) \right) - \frac{m \left( \frac{d}{d\eta} f(\eta) \right)}{1 + \varepsilon \theta(\eta)} + Gr \theta(\eta) = 0$ 
> equ2 := diff(θ(η), η$2) + Pr · f(η) · diff(θ(η), η) = 0
    equ2 :=  $\frac{d^2}{d\eta^2} \theta(\eta) + Pr f(\eta) \left( \frac{d}{d\eta} \theta(\eta) \right) = 0$ 
> Bi := 0.1 :
> Bcs := f(0) = 0, f'(0) = 0, f'(inf) = 1, θ'(0) = -Bi · (1 - θ(0)), θ(inf) = 0
    Bcs := f(0) = 0, D(f)(0) = 0, D(f)(8) = 1, D(θ)(0) = -0.1 + 0.1 θ(0), θ(8) = 0
> Params := [m = 0.1, ε = 0.1, Gr = 0.1, Pr = 0.72] :
> S1 := dsolve({subs(Params, equ1), subs(Params, equ2), Bcs}, {f(η), θ(η)}, type
    = numeric) :
> F1 := odeplot(S1, [ [η, f(η)] ], 0..inf, linestyle = solid, color = black, legend = "m = 0.1",
    labels = [ "η", "f(η)" ], axes = "boxed" ) :
> T1 := odeplot(S1, [ [η, θ(η)] ], 0..inf, linestyle = solid, color = black, legend = "m = 0.1",
    labels = [ "η", "θ(η)" ], axes = "boxed" ) :
> #####
    #####
> Params := [m = 1, ε = 0.1, Gr = 0.1, Pr = 0.72] :
> S2 := dsolve({subs(Params, equ1), subs(Params, equ2), Bcs}, {f(η), θ(η)}, type
    = numeric) :
> F2 := odeplot(S2, [ [η, f(η)] ], 0..inf, linestyle = solid, color = red, legend = "m = 1", axes
    = "boxed" ) :
> T2 := odeplot(S2, [ [η, θ(η)] ], 0..inf, linestyle = solid, color = red, legend = "m = 1", axes
    = "boxed" ) :
> #####
    #####
```



```

> Params := [ m = 3, ε = 0.1, Gr = 0.1, Pr = 0.72 ] :
> S3 := dsolve( {subs(Params, equ1), subs(Params, equ2), Bcs}, {f(η), θ(η)}, type
    = numeric) :
> F3 := odeplot(S3, [ [η, f(η)] ], 0..inf, linestyle = solid, color = blue, legend = "m = 3", axes
    = "boxed") :
> T3 := odeplot(S3, [ [η, θ(η)] ], 0..inf, linestyle = solid, color = blue, legend = "m = 3", axes
    = "boxed") :
>
> plots[display](F1, F2, F3); plots[display](T1, T2, T3);

```

References

- [1] **Blasius. H.** Grenzschichten in Flüssigkeiten and Mit Kleiner reibung . Zeitschrift für Angewandte Mathematik und Physik. 1908; 56; 1-37. French
- [2] **Aziz, A.** A Similarity Solution for Laminar Thermal Boundary Layer over a Flat Plate with a Convective Surface Boundary Condition. *Communications in Nonlinear Science and Numerical Simulation*. 2009;14: 1064–1068.
- [3] **Bataller, R. C.** Radiation Effects for the Blasius and Sakiadis Flows with a Convective Surface Boundary Condition. *Journal of Applied Mathematics and computation*. 2008; 206: 832–840.
- [4] **Cortell, R.** Numerical Solutions of the Classical Blasius Flat-Plate Problem. *Applied Mathematics and computation*. 2005;170: 706–710.
- [5] **Cortell, R.** Similarity Solutions for Flow and Heat Transfer of a Quiescent Fluid Over a Nonlinearly Stretching Surface. *Journal of Matter Process Technology*. 2008;203:176–183.
- [6] **Gabriella, Bognar.** Numerical Method for the Boundary Layer Problem of non-Newtonian fluid flow along moving surfaces. *Electronic Journal of Qualitative theory of Differential Equations*. 2016;122:1-11
- [7] **He, J. H.** A Simple Perturbation Approach to Blasius Equation. *New York journal of applied mathematics and computation*. 2003;140: 217–222.

- [8] **Makinde, O. D and Olanrewaju P.O.** Buoyancy Effects on Thermal Boundary Layer over a Vertical Plate with Convective Surface Boundary Conditions. *ASME Journal of Fluids Engineering*. 2010; 132: 231-241
- [9] **Olanrewaju, P.O, Arulogun. O.T, Adebimpe, K.** Internal Heat Generation Effect on Thermal Boundary layer with a convective boundary condition. *America Journal of Fluid Dynamics*.2012;2(1):1-4.
- [10] **Makinde, O. D.** Analysis of Non-Newtonian Reactive Flow in a Cylindrical Pipe. *ASME Journal of Applied Mechanics*. 2009;76: 034502.
- [11] **Makinde, O. D. and Sibanda, P.** Magnetohydrodynamic Mixed Convective Flow and Heat and Mass Transfer Past a Vertical Plate in a Porous Medium With Constant Wall Suction. *ASME Journal of Heat Transfer*.2008;130: 112602.
- [12] **Shrama P. R and Gurminder S.** Steady MHD Natural Convection Flow with Variable Electrical Conductivity and Heat Generation along an Isothermal Vertical Plate. *Tamkang Journal of Science and Engineering*vol.2010;13:235-242
- [13] **Watunade, .T. and Pop, .I.** Thermal Boundary Layer in Magnetohydrodynamics flow over a flat plate in the presence of a transverse magnetic field. “*ActaMechanica*”. 1994;105:233-238.