

Identity that Connects Thermal Expansion and Isothermal Compressibility is Not an Identity for Condensed Phases

ABSTRACT

In thermodynamics, there is a relation that connects the thermal expansion coefficient and the isothermal compressibility. It has been supposed that it was a universal identity. It is shown that it is often not an identity for condensed phases. Experimental measurements confirm this conclusion. This relation is used in the derivation of Mayer's relation; therefore Mayer's relation also produces the wrong results for condensed phases, which is confirmed experimentally.

Keywords: isothermal compressibility; adiabatic compressibility; isobaric heat capacity; isochoric heat capacity; Mayer's relation; ice 7

1. INTRODUCTION

There is a relationship in thermodynamics [1]:

$$\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T \left(\frac{\partial P}{\partial T} \right)_V = \beta \left(\frac{\partial P}{\partial T} \right)_V \quad (1)$$

where α is the thermal expansion coefficient, V is volume, T is temperature, P is pressure, and β is the isothermal compressibility. It has been supposed that this is a universal identity. However, one can show that it often fails for condensed phases. The third Maxwell relation is:

$$\left(\frac{\partial P}{\partial T} \right)_V = \left(\frac{\partial S}{\partial V} \right)_T \quad (2)$$

where S is entropy. Often when the internal energy U varies, then T varies and vice versa; hence in these cases:

$$\left(\frac{\partial S}{\partial V} \right)_T = \left(\frac{\partial S}{\partial V} \right)_U \quad (3)$$

From Eqs. (1), (2), and (3) and the first law of thermodynamics:

$$\delta Q \leq TdS = dU + PdV \quad (4)$$

it follows that

$$\left(\frac{\partial S}{\partial V} \right)_T = \left(\frac{\partial S}{\partial V} \right)_U = \frac{\alpha}{\beta} = \frac{P}{T} \quad (5)$$

41 Let us check this equation. For Fe at room temperature and atmospheric pressure, $\alpha =$
 42 $3.6 \times 10^{-5} \text{ K}^{-1}$ [2] and $\beta = 0.594 \times 10^{-11} \text{ m}^2/\text{N}$ [3]. Hence α/β equals $6 \times 10^6 \text{ m}^2/(\text{N}\cdot\text{K})$, but P/T equals 336
 43 $\text{m}^2/(\text{N}\cdot\text{K})$. For NaCl under the same conditions, $\alpha = 1.2 \times 10^{-4} \text{ K}^{-1}$ [4], $\beta = 0.42 \times 10^{-10} \text{ m}^2/\text{N}$ [3] and α/β
 44 equals $2.9 \times 10^6 \text{ m}^2/(\text{N}\cdot\text{K})$. It is clear that P in Eq. (4) is not atmospheric pressure but the sum of
 45 atmospheric pressure and pressure due to surface tension, with the former being negligibly small
 46 compared to the latter. This pressure is not independent of temperature. It is evident that Eq. (1) does
 47 not describe the processes in this case precisely. One can show that it is often not an identity for
 48 condensed phases.

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50 2. THEORY

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52 Let us perform a process of heat exchange: we introduce a quantity of heat into a solid or liquid (Eq.
 53 (4)). Its temperature will increase, its volume will increase, and the surface tension pressure will
 54 increase. Therefore, the volume is a function of temperature, and temperature is a function of
 55 pressure: $V = V(T(P))$. The process will be described like this:

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$$57 \quad dV = \frac{dV}{dT} \frac{dT}{dP} dP. \quad (6)$$

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59 From that, one can obtain the following equation:

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$$61 \quad \alpha = \frac{1}{V} \frac{dV}{dT} = \frac{1}{V} \frac{dV}{dP} \frac{dP}{dT} = \beta' \frac{dP}{dT} \quad (7)$$

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63 The thermal expansion coefficient here is the same as that in Eq. (1). The one in Eq. (1) is measured
 64 under a constant atmospheric pressure; however, the pressure in the system is not constant. The
 65 compressibility β' in Eq. (7) is not at a constant temperature and is not the coefficient of compression
 66 but that of expansivity, which differs noticeably from that of compression. One can see that Eq. (1)
 67 cannot describe the process because it is derived for a function of two independent arguments:
 68 $V(T,P)$. It is instructional to present the derivation of Eq. (1). This equation follows from the triple
 69 product rule for three variables such that each variable is an implicit function of the other two [5,6]:

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$$71 \quad \left(\frac{\partial x}{\partial y} \right)_z \left(\frac{\partial y}{\partial z} \right)_x \left(\frac{\partial z}{\partial x} \right)_y = -1. \quad (8)$$

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73 Let us perform a simplified derivation of it. Suppose that there is a function $f(x, y, z) = 0$ (in
 74 thermodynamics, three variables can frequently be related by a function of such a form). The total
 75 differential of z is

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$$77 \quad dz = \left(\frac{\partial z}{\partial x} \right)_y dx + \left(\frac{\partial z}{\partial y} \right)_x dy. \quad (9)$$

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79 Consider a curve with $dz = 0$ that is parameterised by x . On this curve

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$$81 \quad dy = \left(\frac{\partial y}{\partial x} \right)_z dx. \quad (10)$$

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83 Therefore, the equation for $dz = 0$ becomes

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$$85 \quad 0 = \left(\frac{\partial z}{\partial x} \right)_y dx + \left(\frac{\partial z}{\partial y} \right)_x \left(\frac{\partial y}{\partial x} \right)_z dx. \quad (11)$$

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87 This is true for all dx ; hence rearranging terms gives

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$$\left(\frac{\partial z}{\partial x}\right)_y = -\left(\frac{\partial z}{\partial y}\right)_x \left(\frac{\partial y}{\partial x}\right)_z. \quad (12)$$

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Dividing this equation by its right hand side gives the triple product rule, Eq. (8).

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In the present paper, Eq. (1) has been experimentally checked for a number of solid substances and liquid gallium. In Table 1, the physical values of these substances are presented, and in Table 2, the bulk moduli ratios and heat capacity ratios are presented. The bulk modulus is the inverse of the compressibility. Here the isothermal bulk modulus, B , and the isentropic one, B_S , are considered.

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Mayer's relation is:

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$$C_P - C_V = \frac{T\alpha^2}{\rho\beta}, \quad (13)$$

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where C_P and C_V are the isobaric and isochoric heat capacities respectively, and ρ is density. The heat capacity ratio is:

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$$\frac{C_P}{C_V} = \frac{\beta}{\beta_S} \quad (14)$$

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where β_S is the isentropic compressibility. Equations (13) and (14) are derived using Eq. (1) without simplification, and therefore the heat capacity ratios in both equations must be equal. However, from Table 2 one can see that they differ greatly.

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142 **Table 1. Physical values of some solids and a liquid at room temperature**

Substance	ρ , kg/m ³	α , 10 ⁻⁵ K ⁻¹	C_p , J/(kgK)
Magnesiowüstite	3566 (5) [7]	3.12 [7]	924 [2]
MgO			
Zr	6510.7 [2]	2.0 [8]	277.3 [2]
Ga	6094.8 [2]	5.5 [2]	373.9 [2]
Liquid			
Fluorite	3181.5 (7) [12]	5.7 (7) [12]	878.5 ^{a)} [12]
CaF ₂			
Diopside	3286 (5) [13]	1.88 [13]	384.7 [13]
MgCaSi ₂ O ₆			
Forsterite	3233 [15]	2.2599 [16]	844.3 [16]
Mg ₂ SiO ₄			

143 The standard deviation in the last digit is shown in parentheses. a) In [12], an erroneous value was
 144 reported: 87.85.

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162 **Table 2. Bulk moduli of substances from Table 1 and their ratios**

Substance	B , GPa	B_S , GPa	B_S/B	C_P/C_V
				Eq. (13)
Magnesiowüstite	135.0 (10)	163.5 (11) [9]	1.21	1.012
MgO	Eq. (15)	167.1 (4) ^a [9]		
Zr	75.1 (32) [8]	95.3 [10]	1.27	1.005
Ga	23.6 (0.5) [11]	50 (3) [11]	2.12	1.009
Liquid	12.1 (6) [24]	50.4 (4) [25]	4.17	
Fluorite	74.6 (65) [12]	84.5 (5) [12]	1.13	1.027
CaF ₂				
Diopside	88.3 (3) [14]	116.5 (9) [13]	1.32	1.007
MgCaSi ₂ O ₆				
Forsterite	63.6 [15]	128.32 [16]	2.02	1.004
Mg ₂ SiO ₄	80.9 [17]	128.8 (5) [18]	1.59	

163 For all substances except Ga, the isothermal bulk modulus was obtained in this work using the
 164 dependence of V on P in the cited literature. In [15] there are misprints: V/V_0 for $P = 0.7$ GPa should
 165 be 0.989, and for $P = 1.3$ GPa it should be 0.986. The data for 0.7 and 1.3 GPa have been
 166 interchanged. The standard deviation in the last digit is shown in parentheses. a) Calculated from the
 167 speeds of sound at ambient pressure.

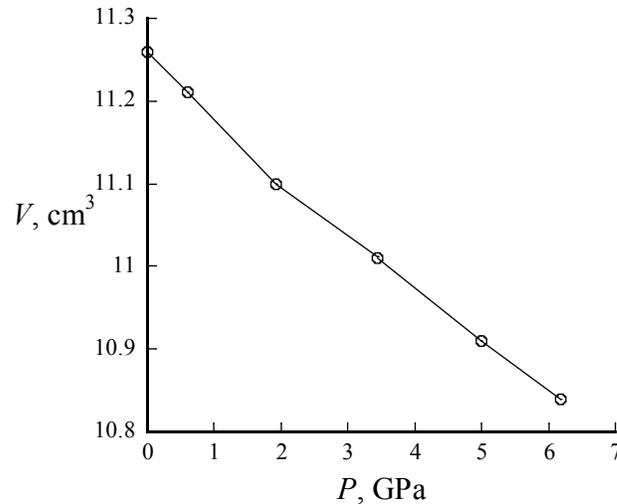
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169 The authors of [7,9] report another value of B for MgO, but it is wrong because, at small
 170 deformations, solids obey Hooke's law with very high accuracy [3,19], but the authors use a third-
 171 order Birch-Murnaghan equation of state (which takes into account all points in the broad interval of
 172 pressures and deformations) in this linear region. For example, in [9] the deformation of MgO obeys
 173 Hooke's law up to 1.92 GPa (figure 1). The dependence of the volume on pressure can be given by
 174 the following equation:

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$$V = 11.26 - 0.083434P \tag{15}$$

where the volume is in cubic centimetres per mole and the pressure is in gigapascals. From it, the isothermal bulk modulus at standard ambient temperature and pressure is equal to 135.0 ± 1.0 GPa. In this paper, the bulk modulus for all substances was calculated from the data that obeyed Hooke's law.



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Fig. 1. Dependence of the volume on pressure for MgO [9]

In [20], physical properties of ice VII were measured (Table 3). Its volume depends on pressure at room temperature like this:

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$$V = 7.564 + 2.743 \times 10^{-2} P - 9.557 \times 10^{-4} P^2, \quad P \leq 42.0 \text{ GPa}$$

$$V \approx 7.792 - 2.47 \times 10^{-2} P, \quad P \geq 58.4 \text{ GPa} \tag{16}$$

It is evident that the ratio B_S/B is significantly larger than C_p/C_v obtained from Eq. (13), particularly at higher pressures. It increases up to 2 at 42 GPa and then decreases drastically.

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Table 3. Compressibilities of ice VII and their ratios at room temperature

Pressure, GPa	B , GPa,	B_S , GPa	B_S/B	C_p/C_v ,
[20]	Eq. (16)	[20]		Eq. (13)
34.4 (4)	192 (17)	233 (2)	1.21	1.00
37.3 (1)	165 (24)	237 (3)	1.44	1.00
38.7 (9)	155 (12)	245 (3)	1.58	1.00
40.3 (5)	143 (9)	260 (3)	1.82	1.00

42.0 (5)	133 (4)	261 (3)	1.96	1.00
58.4 (9)	315 (21)	383 (3)	1.22	1.00
59.7 (14)	315 (21)	395 (3)	1.25	1.00
61.8 (14)	315 (21)	417 (3)	1.32	1.00

198 The standard deviation in the last digit is shown in parentheses.

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200 3. DISCUSSION AND CONCLUSIONS

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202 One can see that the identity Eq. (1), Mayer's relation, and the heat capacity ratio, Eqs. (13) and (14),
 203 cannot describe condensed matter correctly. The derivations of these relations can be found in [21].
 204 In the derivation of Mayer's relation and the heat capacity ratio, Eq. (1) is used. Also, one can show
 205 that the derivation of Mayer's relation is not correct. Let us consider the key part of this derivation and
 206 expand S as a function of T and V :
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$$208 \quad dS(T, V) = \left(\frac{\partial S}{\partial T} \right)_V dT + \left(\frac{\partial S}{\partial V} \right)_T dV \quad (17)$$

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210 whence

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$$212 \quad \left(\frac{\partial S}{\partial T} \right)_P = \left(\frac{\partial S}{\partial T} \right)_V + \left(\frac{\partial S}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_P \quad (18)$$

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$$216 \quad C_P - C_V = T \left(\frac{\partial S}{\partial V} \right)_T \left(\frac{\partial V}{\partial T} \right)_P. \quad (19)$$

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218 One can see that this consideration is equivalent to the following one. Let us take the following
 219 expansion:
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$$221 \quad dS(T, V, P = \text{const}) = \left(\frac{\partial S}{\partial T} \right)_{V, P} dT + \left(\frac{\partial S}{\partial V} \right)_{T, P} dV \quad (20)$$

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223 and divide it by dT . The derivatives on the right hand side are equal to zero, and at a constant P the
 224 arguments V and T are not independent. Equation (1) is valid only in the ideal case where in $V(T, P)$
 225 temperature and pressure are independent parameters.

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227 It is interesting to note that Eq. (1) was experimentally checked for rubber and the authors
 228 reported a value of -0.88 for the right hand side of Eq. (8) [22]. Nevertheless, even this value is not
 229 reliable. In [22,23] and references therein, the tension of a rubber band, F , as a function of
 230 temperature and length, L , was measured. The authors of [22] check the following equation:

$$231 \quad \left(\frac{\partial F}{\partial L} \right)_T \left(\frac{\partial L}{\partial T} \right)_F \left(\frac{\partial T}{\partial F} \right)_L = -1. \quad (21)$$

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233 The authors measure $(\partial F / \partial T)_L > 0$, where F is the tension of a rubber band, and assume that it

234 equals $\left[(\partial T / \partial F)_L \right]^{-1}$, which means that both derivatives have the same sign. This is not true. It

235 should be noted that the sign of $(\partial F/\partial L)_T$ differs from that of $(\partial L/\partial F)_T$. The former is the
 236 dependence of the tension on the length of expansion measured experimentally (the greater the
 237 expansion ΔL the greater the tension ΔF , and $\Delta F/\Delta L > 0$.) The latter can be obtained only
 238 theoretically: let us increase the force of attraction between the atoms ($\Delta F > 0$), and hence the rubber
 239 will contract ($\Delta L < 0$). The sign of $(\partial L/\partial T)_F$ is negative because the rubber band contracts when
 240 heated under tension (the Gough–Joule effect) [22,23]. The derivative $(\partial T/\partial F)_L$ will be negative.
 241 Let us increase the tension by increasing the force of attraction between the atoms. As a result, the
 242 rubber band will contract. To keep the band length constant, we have to decrease its temperature
 243 according to the Gough–Joule effect. So, the experiment produces the value +0.88 instead of –1. The
 244 signs of the partial derivatives of Eq. (1) obtained in [22] have been confirmed by many other papers
 245 [23]. One can see that Eqs. (1) and (8) are not reliable in the description of condensed phases
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247 **COMPETING INTERESTS**

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 249 Author has declared that no competing interests exist.
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