

Energy Generation Using Wearable Thermoelectric Power Generator (WTEPG) from the Living Body

ABSTRACT

In this paper, a general idea about wearable thermoelectric generator from the body heat has been discussed. First, a thermoelectric generator, which is usually used for the industrial purpose (Tellurex-G2-40-0329 series) was used for lab experiment to observe the output results at low-temperature difference (i.e., $\Delta T=6-18$ K). At this temperature range, the power output was approximately 0.0192-0.35 μW which was very low for practical use. Different configurations of TEG (single, double, single TEG with fin) were used to find out the best one, which could generate maximum power. It is found that a single thermoelectric generator with a fin can harvest maximum power output of around 2.5 μW compared to other configurations. A list of low temperature based thermoelectric n-type and p-type materials were presented. n-type 75% Bi_2Te_3 , 25% Bi_2Se_3 and p-type 25% Bi_2Te_3 0.75% Sb_2Te_3 (1.75%Se) were used for numerical and finite element analysis for wearable thermoelectric generator. Maximum 6.5 μW power can be harvested from the body heat when body temperature is 37 $^{\circ}\text{C}$ and the ambient temperature is considered as 25 $^{\circ}\text{C}$ ($\Delta T=12$ K) for this thermoelectric element. Maple, FlexPDE, and SolidWorks software were used for numerical analysis and finite element analysis (FEA).

Keywords: Thermoelectric generator; wearable TEG; Seebeck effect; Figure of Merit, thermal resistance.

1. INTRODUCTION

Over the last two decades, advancements in microelectromechanical system (MEMS) and miniaturization of electronic devices have made the power demand at the range of mili (mW) to micro (μW) watts level for wireless sensor networks (WSN) [1]. The chemical battery, which has a finite lifetime, has biohazard impact on the environment and also needs extra labor for replacement is the common energy source to keep these micro electric devices active [2]. However, it needs replacement after a certain period of time. Therefore, researchers are trying to overcome this energy requirement with an alternative energy source i.e., renewable energy sources: solar, wind, tide, vibration, thermal gradient, acoustic etc. But these traditional renewable energy sources are much larger in size, costly initial set-up, and also not suitable for microelectronic devices [3]. Therefore, the thermoelectric power generator (TEG) is one of the attractive solutions for fulfilling the power demand of mobile electron devices.

From 2000 to till date a huge research has been carried out and is still going on to develop the energy harvesting technology through TEG. In 1960s, first practical thermoelectric module has been introduced for harvesting power, cooling, pumping as well as heating applications [4]. The first TEG from body heat was fabricated in the shirt in 2009 [5]. Over the last decade, starting from 2005, many researchers from all over the world have done many theoretical, simulation-based and practical experiments on TEGs to harvest energy from the human body.

Leonov et al. [6] discussed the power generation capability from the human body and found that forehead is the suitable location to harvest energy using TEG. The output of their developed devices was 30-70 μW from the body heat. Mitcheson [7] compared kinetic power generator and TEG and reported that the generation efficiency is better for kinetic energy harvester even though the thermoelectric generator is suitable for wireless sensors, powered by the body heat. The power density was 20 $\mu\text{W}/\text{cm}^2$ during running whereas it was 10 $\mu\text{W}/\text{cm}^2$ during walking. In 2010, Lossec et al. [8] proposed to improve the power generation by introducing a new factor Z_E and using DC-DC converter for TEG. TEG module (TM-450.0.8.3.0) was used for their experiments and showed that it can generate 7 $\mu\text{W}/\text{cm}^2$ with a heat sink while normal walking and 30 $\mu\text{W}/\text{cm}^2$ while running. Leonov presented that human body has a high thermal resistance, which has an effect on the design of TEG [9]. After the close observations through the experiments, it was mentioned that thermal resistance of the TEG should be hundreds of cm^2K^{-1} . Jo et al. [10] proposed dispenser-printing technology for

TEG developed by a polydimethylsiloxane (PDMS) substrate, which made it flexible and had a low thermal conductivity. The power output of TEG was 2.1 μW at 19 K. Suemori et al. [11] used very light weight composite materials i.e., polystyrene and carbon nanotubes as a thermoelectric (TE) materials for their proposed TEG. It was developed on the polyethylene naphthalate film using printing technology. The prototype can generate 55 mW/m^2 at 70 K temperature difference. Kim et al. [12] designed a wearable TEG, which consisted of 12 couple of $\text{Bi}_{0.5}\text{Sb}_{1.5}\text{Te}_3$ and $\text{Bi}_2\text{Se}_{0.3}\text{Te}_{2.7}$ materials that was fabricated on polymer based fabric. The power and voltage outputs were 224 nW and 14.2 mV at 15K temperature difference. Kim et al. [13] designed a glass-fabric based flexible-TEG using printing process with *n*-type Bi_2Te_3 and *p*-type Sb_2Te_3 TE materials. The power density of the prototype is 3.8 mW/cm^2 at 50K.

Typical TEGs are used for industrial purpose where there is a huge temperature difference between two surfaces of the TEG. Therefore, the wearable thermoelectric power generator (WTEPG) is becoming a new platform for wireless sensor networks to provide the green, less costly, and energy efficient power. WTEGs are attached to the human body to harvest the thermal energy and convert it into electrical energy. Normally the human body temperature is around 37 $^{\circ}\text{C}$ [9] whereas the ambient temperature is not fixed. It varies randomly around the world and hourly basis as well. For this research, the range of ambient temperatures is considered from 19 $^{\circ}\text{C}$ to 31 $^{\circ}\text{C}$. But most of the TEGs available in the market are designed for high temperature (typically $\Delta T > 50$ $^{\circ}\text{C}$), which is not suitable for harvesting energy from body heat. Therefore, one of the objectives of this research work is to determine if the commercial TEGs are used for harvesting energy from the human body what will be the power output. Moreover, another objective is to investigate the properties of thermoelectric materials, which are suitable at low temperature ($\Delta T = 6\text{--}18$ $^{\circ}\text{C}$) and analyze their behavior.

2. THERMOELECTRIC GENERATOR

Thermoelectric generator (TEG) is a solid-state static device. TEG generates electrical energy from thermal energy due to the temperature difference across its two surfaces. Thomas Johann Seebeck first discovered this technology in 1821 [14]. This energy harvesting technology is environmental friendly. The size of the TEG varies from mili (m) to micro (μ) range, no maintenance cost, has 20-30 years of operational lifetime which has made this technology very popular nowadays. Recently, TEGs are used in many applications including: micro self-powered wireless platforms, industrials areas, hot pipelines, aircrafts, biosensors, automobiles, human body, telemetry systems, in the internal combustion engine as a heat recovery device, and in small electronic devices for various applications. Especially, in coming decades, tracking, monitoring sensors and surveillance system of health are going to be expanded very quickly, which is one of the big platforms of mobile sensor networks.

2.1 Wearable TEG

Wearable thermoelectric power generator (WTEG) is nothing but a specially designed TEG, which uses the temperature difference of any living body and surrounding temperature to harvest energy. The human body is a great source of energies such as heat, motion, and vibration. These energies can be used to convert into electrical energy. Therefore, WTEG can be used to convert this heat energy into electrical energy.

2.2 Basic Principal

The fundamental principle of TEG is based on the Seebeck effect of TE materials. It can generate voltage if there is a temperature gradient between two sides of the element. According to Seebeck effect, the generated voltage is directly proportional to the temperature difference.

$$V = \alpha \Delta T \quad (1)$$

where, α is the Seebeck coefficient of the materials. A typical value of Seebeck coefficient of commercially used *n*-type material Bismuth Telluride (Bi_2Te_3) is 287×10^{-6} V/K at 54 $^{\circ}\text{C}$ and for *p*-type material Antimony Telluride (Sb_2Te_3), it is $101\text{--}161 \times 10^{-6}$ V/K at room temperature [15], [16].

A thermoelectric element consists of *p*-type and *n*-type semiconductors where *p*-type has excess holes and *n*-type have excess electrons to carry the energy. Typically, a large number of TE materials

are connected electrically in series to increase the generation of voltage and thermally in parallel for increasing the thermal conductivity. The standard size of TEG modules is vary from 4 mm × 4 mm × 3 mm to around 50 mm × 50 mm × 50 mm [17]. Figure 1 illustrates a typical single thermoelectric cell.

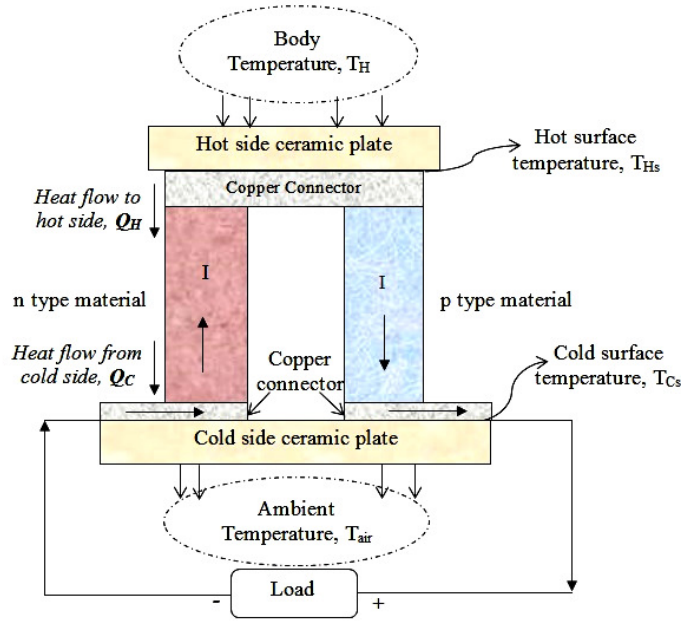


Fig. 1. Schematic diagram of a thermoelectric pair with *n*-type and *p*-type TE leg.

The thermal efficiency of thermoelectric materials depends on the figure of merit (Z). The typical value for ZT (dimensionless unit, T is the temperature in K) is around 1 [18] for most materials such as for Bi_2Te_3 is 0.8 at room temperature [19]. This figure of merit depends on:

$$Z = \frac{\alpha^2}{\rho k} \quad (2)$$

where, ρ is electrical resistivity and k is thermal conductivity. The Power generation from thermoelectric module not only depends on these parameters but also depends on area ($A_t = A_n + A_p$, here A_t is total area, A_n is cross-sectional area of *n*-type materials, A_p is cross-sectional area of *p*-type materials) of the one pair, length of the materials lag (l), hot surface and cold surface temperature of TEG module (T_{Hs} and T_{Cs}), internal electrical resistance of the materials (R_{in}) and number of couples (n) in one module as well.

2.3 Mathematical Modeling of TEG

The difference between the rate of heat energy entering to hot side Q_H and going out from the cold side of the module Q_C is the amount of generated power (P) by the module.

$$P = n(\dot{Q}_H - \dot{Q}_C) \quad (3)$$

where,

$$\dot{Q}_H = n[\alpha T_{Hs} + K(T_{Hs} - T_{Cs}) - 0.5I^2 R_{in}] \quad (4)$$

$$\dot{Q}_C = n[\alpha T_{Cs} + K(T_{Hs} - T_{Cs}) + 0.5I^2 R_{in}] \quad (5)$$

In Eqn. (4) and (5), $\alpha = (\alpha_n + \alpha_p)$, α_n and α_p are the Seebeck coefficients of *n*-type and *p*-type materials, respectively and the thermal conductance K is given by:

$$K = k_n \gamma_n + k_p \gamma_p \quad (6)$$

where,

$$k_n = \frac{\alpha_n^2}{\rho_n Z_n} \quad 7(a)$$

$$k_p = \frac{\alpha_p^2}{\rho_p Z_p} \quad 7(b)$$

$$\gamma = \frac{Area}{length} = \frac{A}{l} \quad 7(c)$$

where, k_n and k_p are the thermal conductivities, γ_n and γ_p are the ratios of area to the length, ρ_n and ρ_p are the electrical resistivity, Z_n and Z_p are the figure of merits of n -type and p -type materials, respectively. Internal resistance of the module is calculated by:

$$R_{in} = \frac{\rho_n}{\gamma_n} + \frac{\rho_p}{\gamma_p} \quad (8)$$

3. EXPERIMENTAL TESTS AND RESULTS

A commercial TEG module (Tellurex, G2-40-0329 series) was used for the experiment in the lab. Bi-Te based thermoelectric materials are used in this module which is designed for industrial purposes. It can generate maximum power when hot side temperature is 250 °C and cold side is 50 °C. But for this lab experiment, low temperatures were used. The specification and testing parameters are given in Table 1 and Fig. 2 shows the experimental setup.

Table 1. Parameters used for the Experimental test [20].

Specification	Value
Hot surface temperature, T_H	37 °C
Ambient temperature, T_{air}	19-31 °C
Module size	4 mm × 4 mm × 3.5 mm
Internal Resistance of TEG, R_{in}	3.1 Ω
Seebeck coefficient of n -type, α_n	225×10 ⁻⁶ V/K
Seebeck coefficient of p -type, α_p	230×10 ⁻⁶ V/K
Thermal resistivity of n -type, ρ_n	1.3×10 ⁻⁵ ohm-cm
Thermal resistivity of p -type, ρ_p	1.27×10 ⁻⁵ ohm-cm
Thermal conductivity of n -type, k_n	1.14 Watt/cm.K
Thermal conductivity of p -type, k_p	1.14 Watt/cm.K
Total area, A_t	1.96 mm ²
Length, $l_n=l_p$	1.4 mm
Thickness of the copper plate	0.3mm
Gap between two lags	1.08mm
Number of Couples, n	128
Load resistance, R_L	3.3 Ω

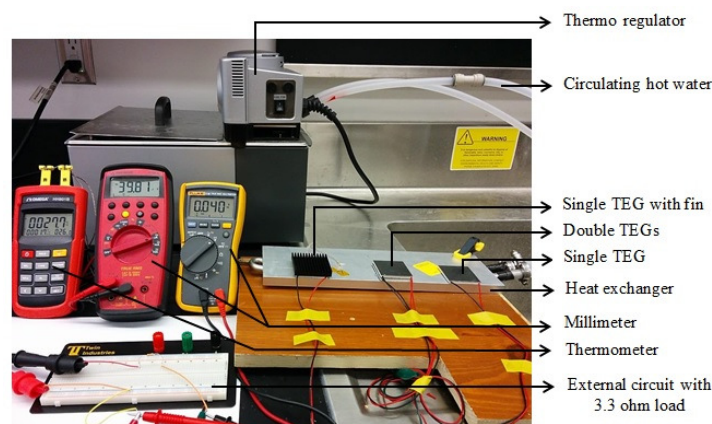


Fig. 2. Experimental setup.

In this experiment, a thermo-regulator was used for circulating hot water through the heat exchanger plate, which can be considered as a human body. Different temperatures can be set in the thermo-regulator to change the plate temperature because the ambient temperature is fixed in the lab. The resistance of 3.3Ω was used as a load in the external circuit to match with internal resistance of the module. A Multi-meter was used for measuring the generated voltage and current. A thermometer was used for measuring the plate and ambient temperatures. Three different cases were considered for experimental tests and for comparing the results to determine the optimum case for harvesting maximum power.

3.1 Single TEG Module

At first, only one TEG module was used for experiment. Figure 3 shows the single module of Tellurex G2-40-0329 series.

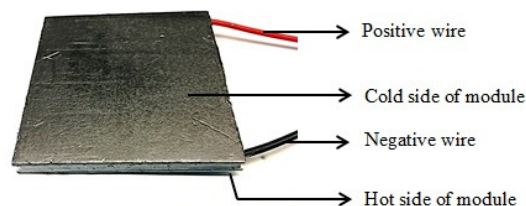


Fig. 3. Single TEG module.

Figure 4 represents the experimental results of open circuit voltage and short circuit current at different temperature gradients ($6-18^{\circ}\text{C}$). The open circuit voltage and short circuit current increase with increasing temperature difference between hot surface and the ambient temperature. Therefore, the output power also increases.

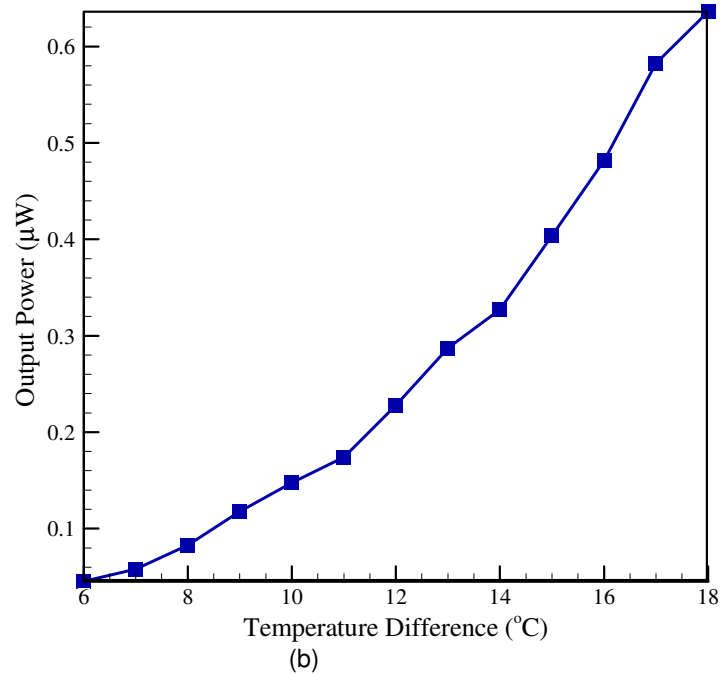
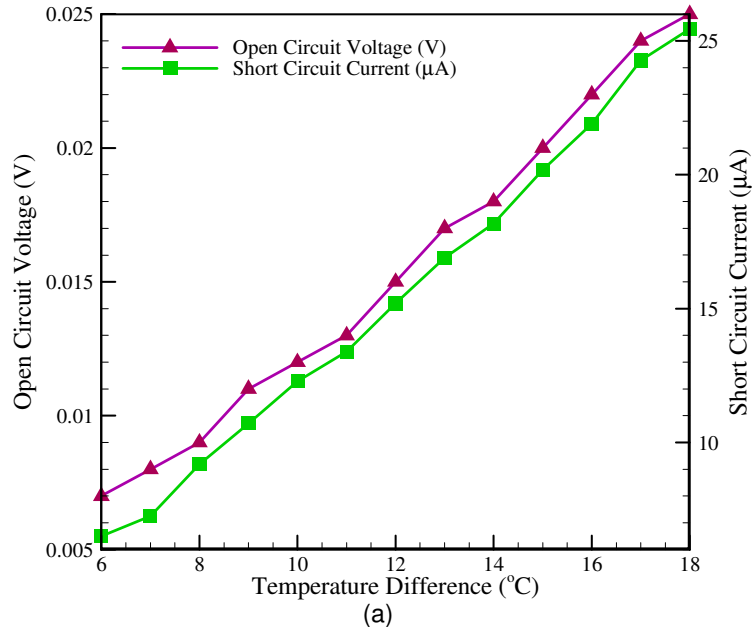


Fig. 4. (a) Open circuit voltage and short circuit current and (b) output power with respect to temperature difference between hot and ambient temperature for single module.

Figure 5 indicates the matched load voltage, load current and load power output with respect to temperature differences. Comparing these graphs with Fig. 4, it is clear that the voltage and current output decrease after adding load resistance and thus output power decreases.

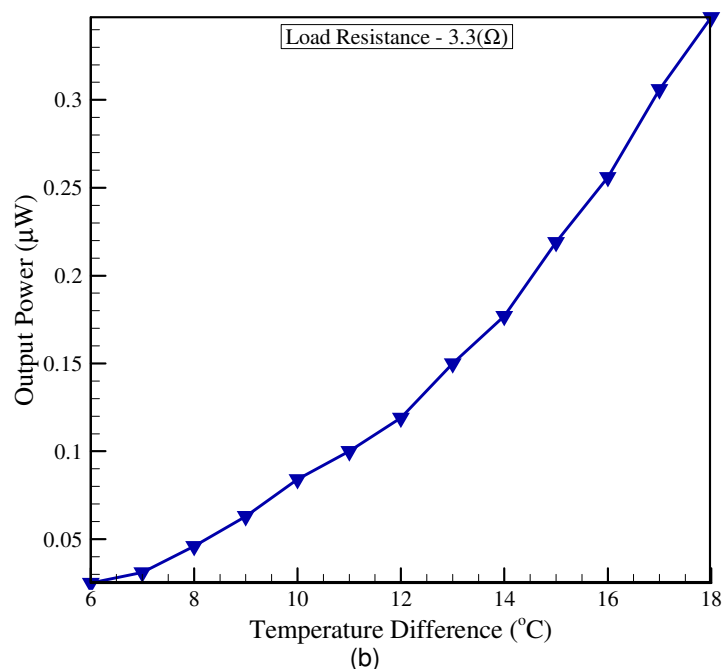
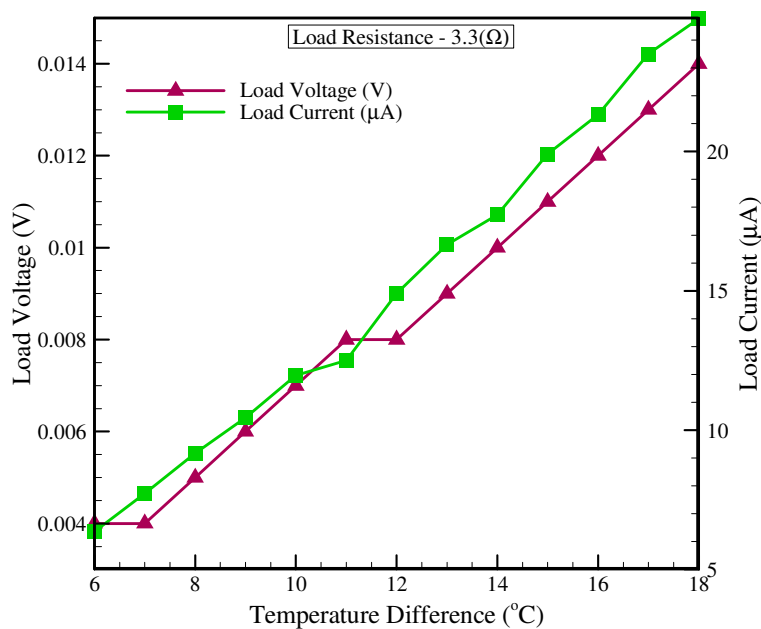


Fig. 5. (a) Load voltage and Load current, (b) Output power with respect to temperature difference between hot and ambient temperature for single module.

3.2 Double TEG Module

In this case, two back-to-back TEG modules were connected in series to increase the output voltage. Figure 6 shows the configuration of double TEG modules. Same steps were followed to get the open circuit voltage, short circuit current, power and then load voltage, load current, load power.

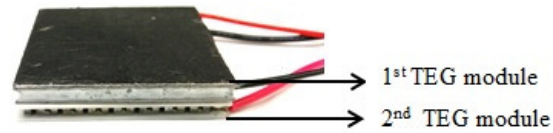


Fig. 6. Double TEG modules.

Figure 7 and Figure 8 represent open circuit voltage, short circuit current and power, and load voltage, load current and load power, respectively, with respect to temperature differences. The voltage, current, and power output is more than single TEG module.

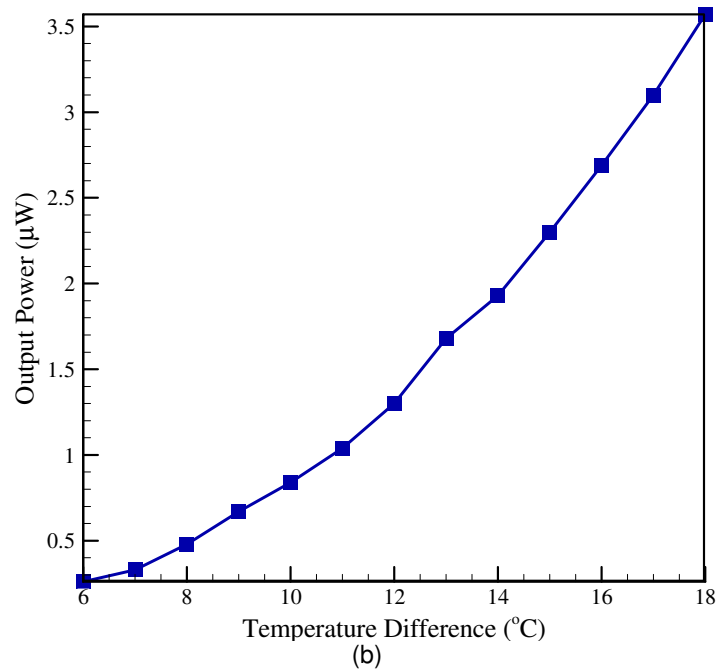
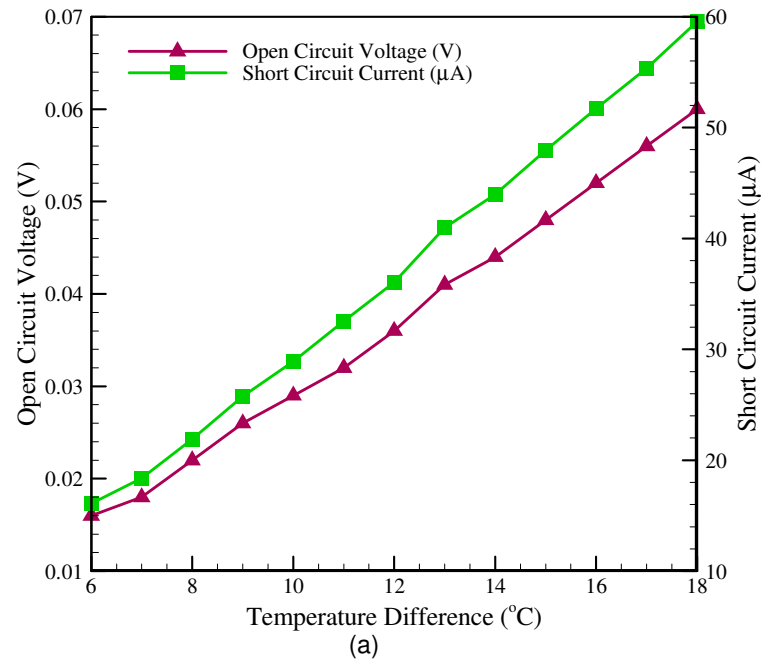


Fig. 7. (a) Open circuit voltage and short circuit current (b) Output power with respect to temperature for double modules.

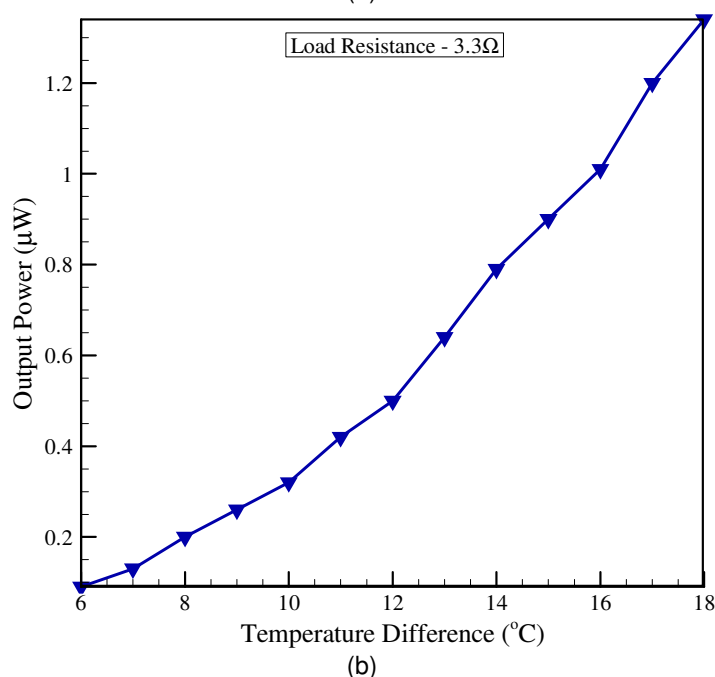
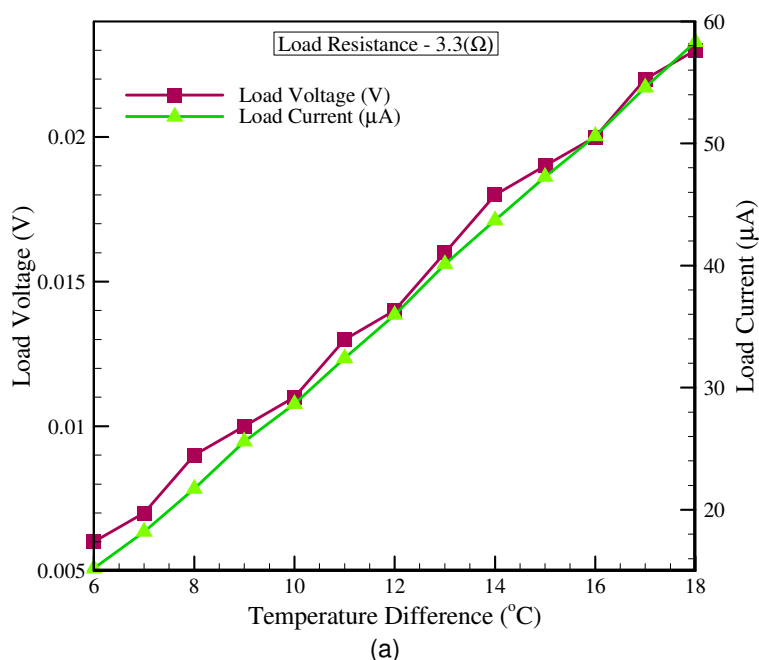


Fig. 8. (a) Load voltage and Load current, and (b) Output power with respect to temperature difference for double modules.

Comparing Fig. 7(b) with Fig. 8(b), the power output is almost double at matched load at maximum temperature difference. It is because of two back-to-back modules were connected in series, which increases the thermal resistance of the modules between two surfaces and also increases the thickness of the module. Therefore, the temperature difference between two surfaces was more than one module, which increases the output power as well.

3.3 Single TEG Module with Fin

At last, a fin of size 45.97 mm × 45.97 mm × 9.02 mm was attached to the cold surface of TEG. Usually, the fin is used to increase the heat dissipation rate from any hot surface. The thermal heat energy goes parallel from a hot surface to cold surface and increases the temperature of cold surface gradually. At the same time, the heat dissipates from the cold surface to the surrounding environment through convection process. If the fin is attached then this dissipation rate will be increased. Figure 9 shows the arrangements of the set-up of the fin with a single module.

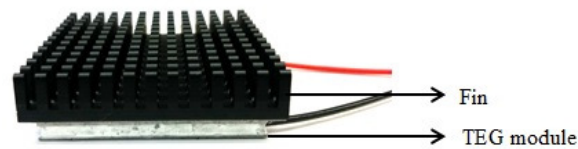
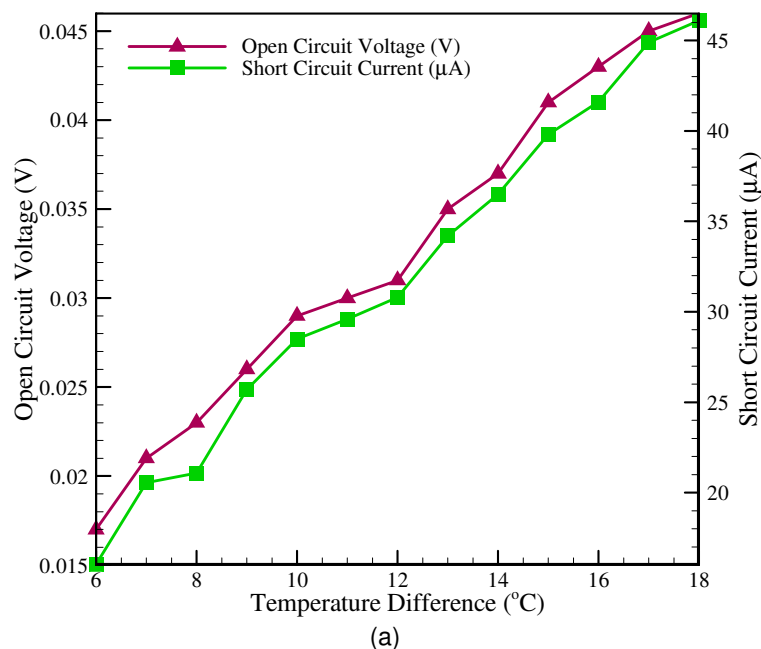


Fig. 9. Single TEG module with fin.

Figure 10 and Figure 11 illustrate voltage, current and power output without and with load resistance, respectively, against the temperature differences. It is noticeable that output voltage, current and power is more than previous two cases.



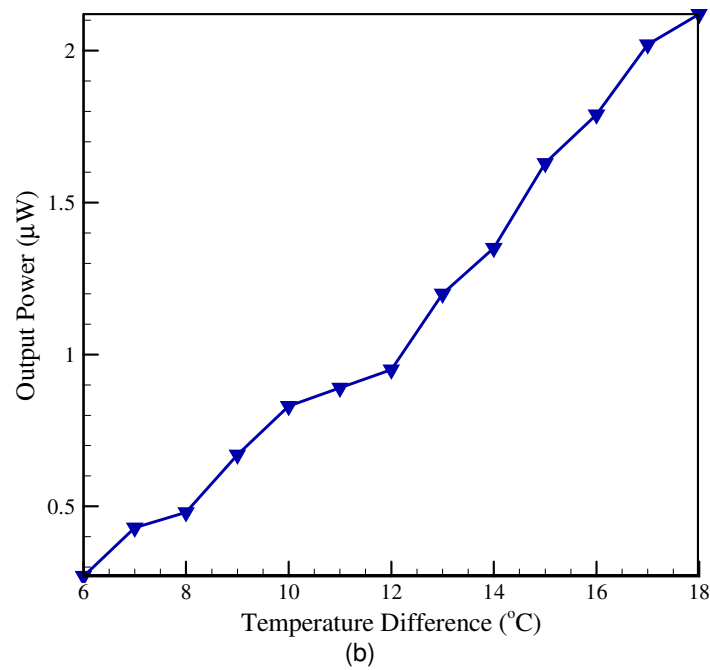
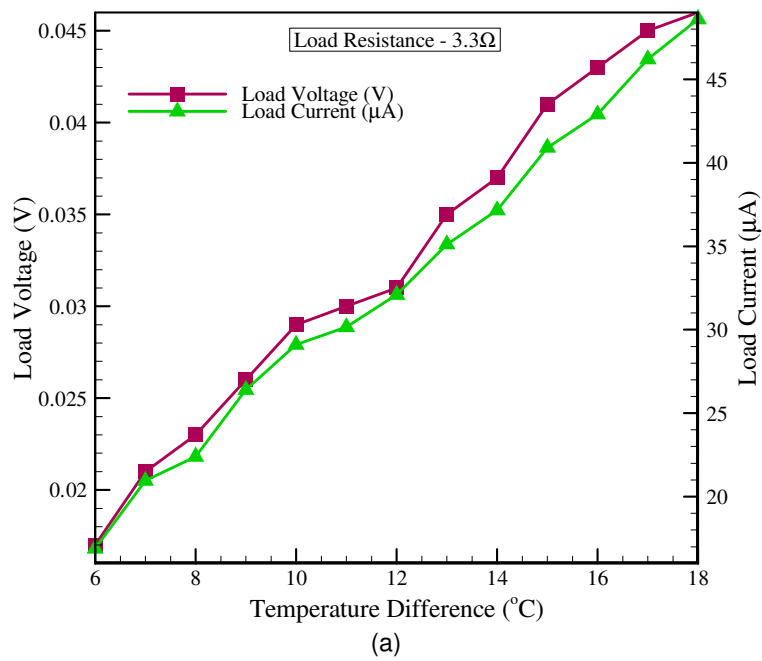


Fig. 10. (a) Open circuit voltage and short circuit current, (b) Output power with respect to temperature difference.



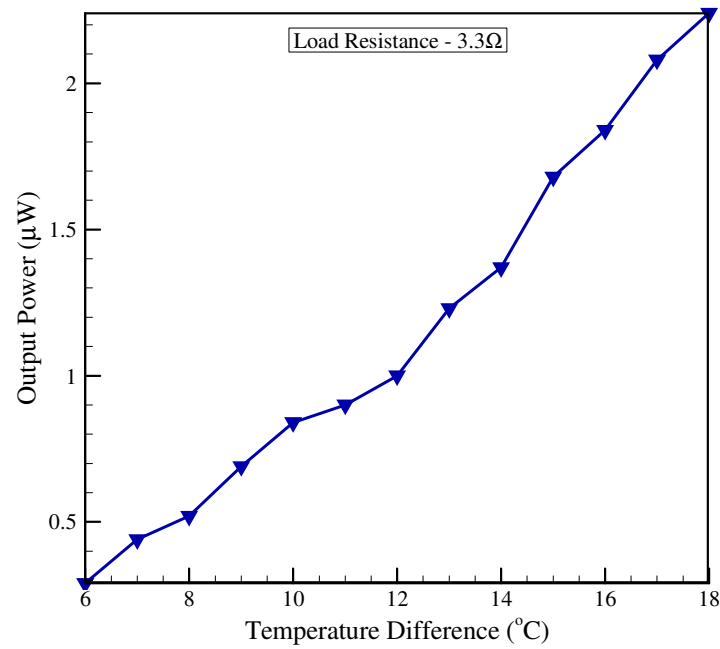


Fig. 11. (a) Load voltage and Load current, (b) Output power with respect to temperature difference at $R_L=3.3 \Omega$.

Comparing these three different cases, the single TEG with fin is more suitable than only single and double TEG configurations. Figure 12 indicates the output power for three different cases at matched load. Considering wearable TEG, it should be small, light, and thin. In that case, double TEG configuration is suitable as it is thinner but the output power is not higher than a single TEG with fin configuration. However, the price of TEG module is also quite high than a fin. In the double module, another problem may occur if one of the modules becomes inactive then the output power will become zero. Therefore, the single TEG with a fin can be considered the suitable one for power harvesting from the human body.

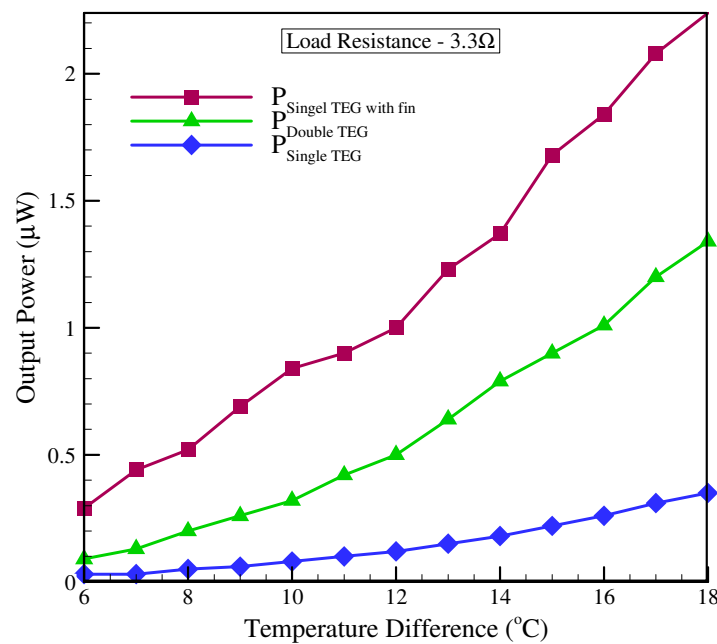


Fig. 12. Output power for three different configurations.

4. ANALYSIS OF THERMOELECTRIC MATERIALS

The module, which is used for the experiment, is not suitable for low-temperature environment. Therefore, it is important to find out thermoelectric materials those have a good material profile to work at low temperature, must be used in TE module for the wearable thermoelectric generator. Most of the cases, Bi_2Te_3 and Bi_2Se_3 are used for low-temperature applications in TEGs [2]. Now researchers are trying to modify these material properties and mixing with other nanomaterials to increase the figure of merit (Z).

4.1 Low Temperature based Materials

There are different n-type and p-type semiconductor materials available to be used, but most of the materials have high-temperature profile. For wearable applications, the temperature range is $\Delta T=6-18$ K, where the body and ambient temperatures are 37°C and $19-31^\circ\text{C}$, respectively. The hot side and cold side temperatures are considered as 310 K and 298 K. Therefore, the average temperature of these two surfaces is 304 K, which is considered for investigating the materials properties. To find such materials for this temperature range, different handbooks are studied and listed the suitable materials in Table 2.

Table 2. The n-type and p-type TE material properties at low temperature [21], [22].

Type	Material	Seebeck coefficient, 10^{-6} (V/K)	Electrical resistivity (10^{-3} ohm-cm)	Figure of merit (10^{-3} K^{-1})
n-type	75% Bi_2Te_3 , 25% Bi_2Se_3	-159.2	1.02	2.03
	bismuth telluride ($\text{Bi}_{1.75}\text{Te}_{3.25}$)-sulfur ball milled	-110	6	0.23
	25% Bi_2Te_3 0.75% Sb_2Te_3 (1.75%Se)	201	1.03	3.47
	AgSbTe_2	204.2857	4.9	1.13
p-type	$\text{Si}_{0.7}\text{Ge}_{0.3}$	221.1111	4.02	0.19
	TAGS-85-(AgSbTe_2)1- 85,(GeTe)85	78.08	0.68	0.68
	antimony telluride (Sb_2Te_3) sulfur ball milled	120	0.002	0.82

From Table 2, n-type 75% Bi_2Te_3 , 25% Bi_2Se_3 and p-type 25% Bi_2Te_3 0.75% Sb_2Te_3 (1.75%Se) were considered for further numerical and finite element analysis due to its high figure of merit for wearable TEG.

4.2 Numerical Analysis

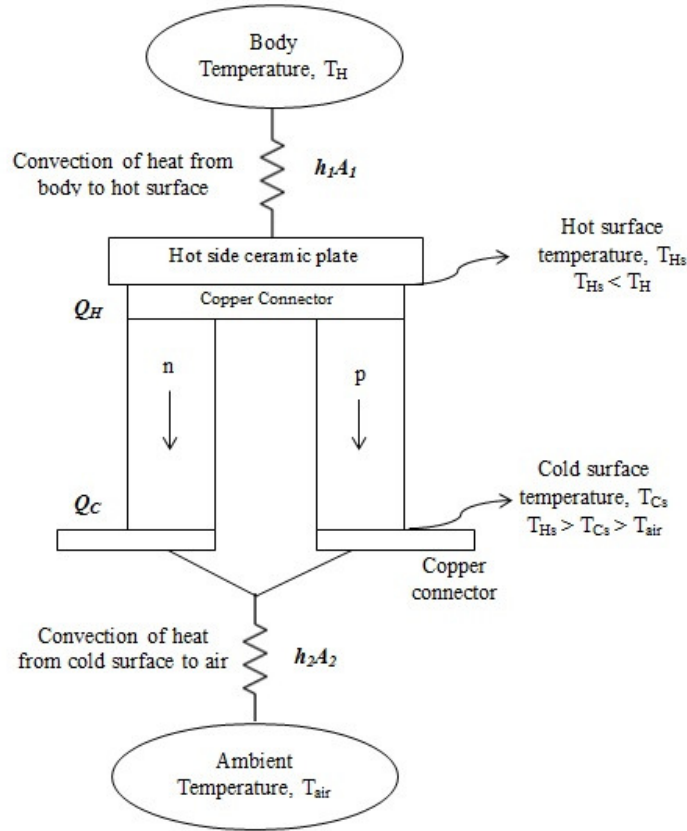
According to Eqs. (4) and (5), the rate of heat flow going in and out from the TEG surface is given by:

$$\dot{Q}_H = n[\alpha T_{Hs} + K(T_{Hs} - T_{Cs}) - 0.5I^2 R_{in}] \quad (4)$$

$$\dot{Q}_C = n[\alpha T_{Cs} + K(T_{Hs} - T_{Cs}) + 0.5I^2 R_{in}] \quad (5)$$

In these equations, almost all parameters are known except T_{Hs} and T_{Cs} temperatures. Actually, T_{Hs} is not equal to the hot side temperature of T_H and similarly T_{Cs} is not equal to T_{air} , which is cold side. Theoretically, the amount of rate of heat flow at hot side must be equal to the amount of rate of heat flow at the hot surface of the element and similarly for the cold surface. But practically there is some heat loss as heat convection, which also must be equal to the rate of flow of heat from the hot surface

303 to cold surface of the element. Figure 13 illustrates the schematic diagram of a practical scenario of
304 heat flow from hot side to cold side of a TEG.



305 **Fig. 13. Schematic diagram of heat flow in and out from a TE element.**

306 For the simplicity of numerical analysis of the module, following assumptions are made:

- 307 (i) The whole system is in steady state;
308 (ii) The properties of the TE materials are independent of temperature changes;
309 (iii) The size and dimensions of all n-type and p-type elements are identical;
310 (iv) The TE elements are connected in series and heat flows parallel from hot to cold side;
311 (v) The surroundings of the n-type and p-type materials (left, right and the gap between them) are
312 adiabatic.
313
314

315 Now considering the heat convection process, the rate of heat flow from hot side to hot surface of the
316 element and cold surface to ambient temperature are given by:
317
318

$$\dot{Q}_H = h_1 A_1 (T_H - T_{Hs}) \quad (9)$$

$$\dot{Q}_C = h_2 A_2 (T_{Cs} - T_{air}) \quad (10)$$

319 According to Eqs. (4), (5) and Eqs. (9), (10), the rate of heat flow is rewritten as:
320
321

$$\dot{Q}_H = n[\alpha T_{Hs} + K(T_{Hs} - T_{Cs}) - 0.5I^2 R_{in}] = h_1 A_1 (T_H - T_{Hs}) \quad (11)$$

$$\dot{Q}_C = n[\alpha T_{Cs} + K(T_{Hs} - T_{Cs}) + 0.5I^2 R_{in}] = h_2 A_2 (T_{Cs} - T_{air}) \quad (12)$$

322 where, h_1 (assumed for numerical analysis $0.5 \text{ W/m}^2\text{K}$) and A_1 (0.054 mm^2) are the heat transfer
323 coefficient and surface area of the upper copper plate, respectively. Similarly, h_2 (assumed 0.035
324 $\text{W/m}^2\text{K}$) and A_2 (0.0392 mm^2) are the heat transfer coefficient and surface area of the lower copper
325

plate, respectively. When $h_1 A_1 = h_2 A_2 = \text{infinity}$ only that case $T_H = T_{Hs}$ and $T_{Cs} = T_{air}$ which is not practically possible. Solving the Eqs. (11) and (12), unknown parameters T_{Hs} and T_{Cs} can be found as:

$$T_{Hs} = \frac{(nK - n\alpha I + h_2 A_2)(0.5nI^2 R_{in} + h_1 A_1 T_H) + (0.5nI^2 R_{in} + h_2 A_2 T_{air})nK}{(h_1 A_1 + nK + n\alpha I)(nK - n\alpha I + h_2 A_2) - (nk)^2} \quad (13)$$

$$T_{Cs} = -\frac{nK(-0.5nI^2 R_{in} - h_1 A_1 T_H) + (-h_1 A_1 - nK - n\alpha I)(0.5nI^2 R_{in} + h_2 A_2 T_{air})}{(h_1 A_1 + nK + n\alpha I)(nK - n\alpha I + h_2 A_2) - (nk)^2} \quad (14)$$

Substitute Eqs. (13) and (14) into Eqs. (4) and (5) to calculate the heat flow rates and then output power can be easily calculated from Eq. (3). For numerical analysis, material properties were taken from Table 2, and the size and dimensions are taken from Table 1 where, $T_H = 310$ K, $T_{air} = 298$ K. The whole numerical analysis was carried out in Maple software to get the power. Figure 14 illustrates the output results in the output power with respect to the load current. The temperature difference between T_{Hs} and T_{Cs} (i.e., the difference was around 3 K calculated from theoretical analysis) was very low which was one of the main reasons of low power output (μW level). The output power increases with increasing electrical current. However reaching the peak value, the power output decreases with further increasing of current. The theoretical maximum power is calculated to be 6.5 μW at 0.015 A with ΔT of 3 K.

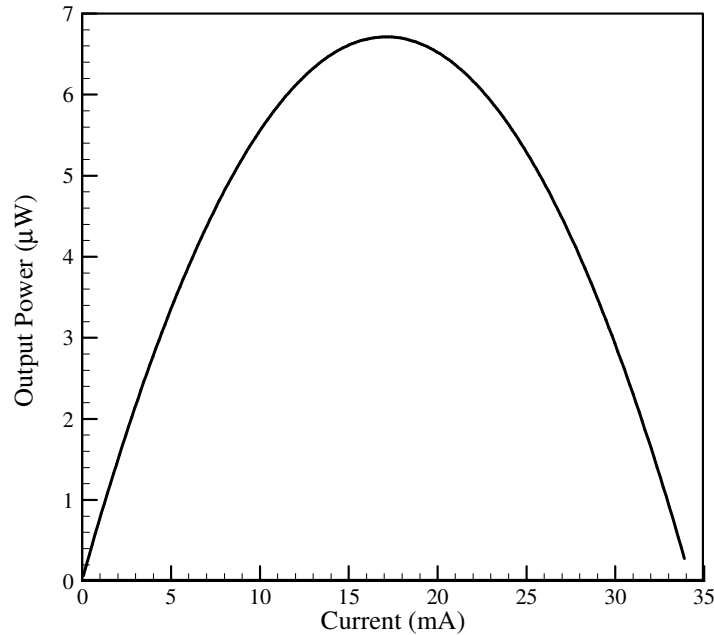


Fig. 14. Theoretical result of the power output with respect to current.

4.3 Finite Element Analysis (FEA)

Finite element analysis was done in FlexPDE software using the materials properties and geometry. Figure 15 shows the mesh analysis of TE element. In this analysis, an external load was added at the bottom to complete the cycle. The electrical resistance of the load was equal to the internal resistance of the thermoelectric material.

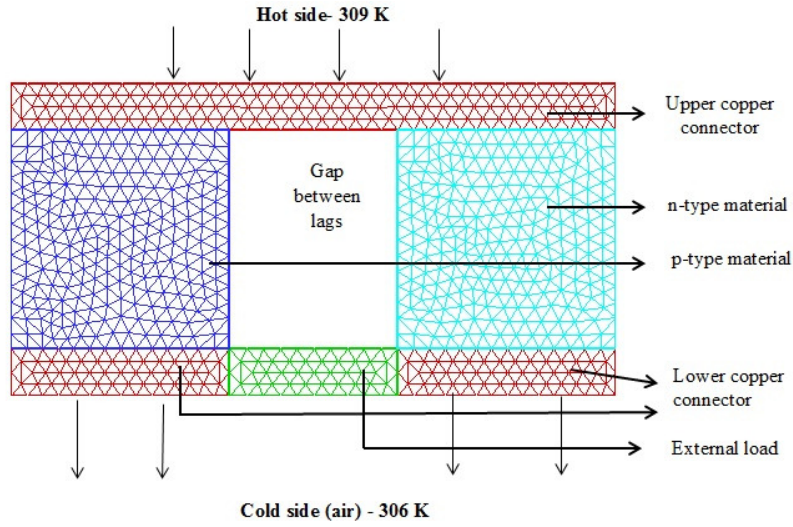


Fig. 15. Mesh analysis of TE element.

4.3.1 Governing Equation for FEA

The governing equations for electric field ($\vec{E}$) produced in the thermoelectric element due to the temperature difference (ΔT) and heat flow ($\vec{q}$) through the elements due to the Peltier effect, are given by:

$$\vec{J} = \sigma(\vec{E} - \alpha \Delta T) \quad (15)$$

$$\vec{q} = \alpha T \vec{J} - k \Delta T \quad (16)$$

here, $\vec{J}$, σ , α , k are current density, electrical conductivity, Seebeck coefficient, and thermal conductivity, respectively. According to the conservation principal of energy and current-

$$\nabla \cdot \vec{q} = \vec{J} \cdot \vec{E} = \dot{q} \quad (17)$$

$$\nabla \cdot \vec{J} = 0 \quad (18)$$

According to the definition of electric potential, electric field is given by:

$$\vec{E} = -\nabla V \quad (19)$$

Figure 16 represents heat flow, current density profiles of designed TE pair. Figure 16 (a) shows that the heat flows from hot surface ($T_{Hs}=310$ K) to cold surface ($T_{Cs}=306$ K) but not flowing through the gap between legs, sidewalls, and not also through the load, as it is not the part of the TEG.

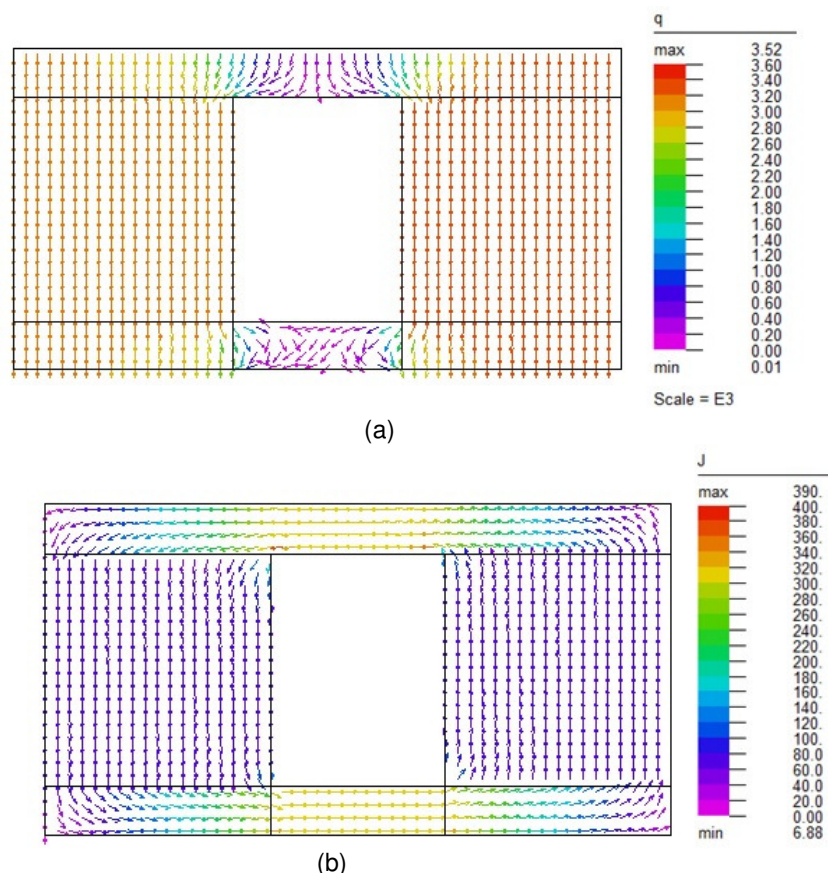


Fig. 16. (a) heat flow profile and (b) current density profile of a single TE module.

5. CHALLENGES OF GENERATING OPTIMUM POWER

Most of the wearable TEGs generate power of micro (μ) watt range even less than this. It becomes a challenge to generate optimum energy to power up the mobile electronic devices from this green technology. Some existing challenges are discussed below:

- (i) Low Thermal Resistance [23]
- (ii) Low figure of merit of TE materials [2]
- (iii) The flexibility of Module: Flexibility of the module is another big problem. The TEG modules that are available in the market have a rigid body at top and bottom side. However, the human body is not a plain surface. The body has different shapes and curves. Figure 17 shows an overview of the human curved body with a rigid TEG. Therefore, TEGs are not attached to the body very tightly which causes to reduce heat flow from the body to the hot surface of the module. Figure 18 presents a flexible TEG module designed in SolidWorks.

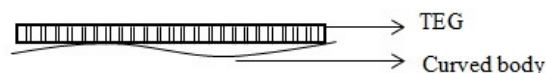


Fig. 17. Typical TEG module attached on body

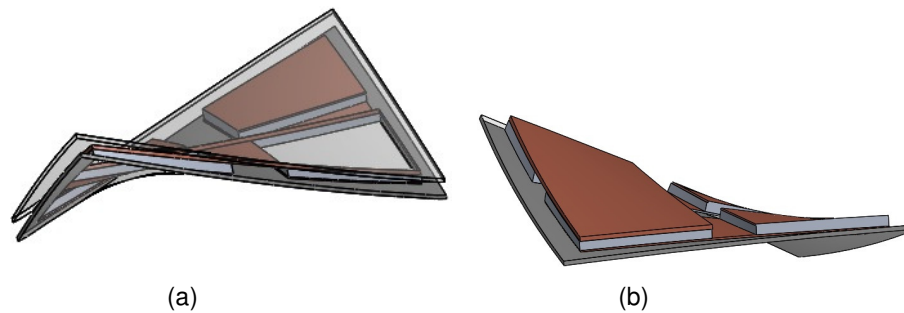


Fig. 18. Flexibility of wearable TEG.

5. CONCLUSION

In this paper, both theoretical and experimental analyses have been described. Experimental work was carried out using existing TEG module. A maximum output power of $0.35 \mu\text{W}$ was measured for the single module at matched load. Double and single modules with fin were also tried for the experiment. Therefore, it is found that the among these three configurations, single TEG with a fin has a high power output of around $2.5 \mu\text{W}$, which is nearly 7 times greater than a single module. In theoretical analysis, *n*-type 75% Bi_2Te_3 , 25% Bi_2Se_3 and *p*-type 25% Bi_2Te_3 0.75% Sb_2Te_3 (1.75%Se) were used. The theoretical result shows that TEG with these TE materials generates approximately $6.5 \mu\text{W}$ when ΔT is 3 K. Finite element analysis of *n*-type and *p*-type materials shows their heat flow and current density profile when the hot surface and cold surface temperature are 310 K and 306 K, respectively.

Now flexibility and high power output are two main concerns for the further developments of WTEG for researchers. To optimize the output power and make the WTEG module more flexible and thin, the existing challenges might be considered to overcome the problems as a future work.

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