Original Research Article

High Microwave Absorption of Multi-Walled Carbon Nanotubes (Outer Diameter 10 – 20 nm)-Epoxy Composites in R–Band

Abstract

We studied the microwave absorption of multi-walled carbon nanotubes (MWCNTs)-epoxy composites over a continuous frequency range in R-band (26.5 – 40 GHz). The outer diameters (OD) of the MWCNTs were in the 10 – 20 nm range. We measured and analyzed the microstructures, dielectric and the microwave absorption properties of the composite samples. High attenuation factor which correlates significant absorption of microwave was observed in the 32 – 40 GHz frequency band. Microwave absorption was due to high dielectric losses, interfacial charge polarization, and the free electron mobility in the composite material. Our results also show the dependence of microwave absorption on the loading fractions of MWCNTs and on the thickness of the absorbing material. Significant microwave absorption capabilities of the composite samples were achieved at 7 to 10 wt.% of MWCNT loadings for frequencies above 32 GHz.

Keywords: Composites; Nanotubes; Dielectric properties; Conducting polymers; Microwave absorption.

1. Introduction

The combination of structure, topology, and dimensions creates an unparalleled host of physical properties in carbon nanotubes (CNTs) for explorations[1]. These tiny, quasi one-dimensional materials show great promise for a variety of application areas, such as molecular reinforcements in composites, displays, sensors, energy-storage media and molecular electronic devices[2-4].

Multi-walled carbon nanotubes (MWCNTs) are made by rolling a stacking of multiple layers of graphene sheets so as to obtain concentric nanotubes. Like polymer chains in epoxy used as a composite matrix, MWCNTs have practically one-dimension and are flexible. Many exciting and unique properties have been demonstrated for polymers filled with C-based materials, including improved strength and durability, electrical conductivity, flame resistance, UV absorption, and reduced permeability [5-9]. In addition to these properties, the rapid progress in the fabrication of CNTs and large area (≈1 cm^2) graphene flakes[10] make these C structures promising for microwave absorption (MA) applications, e.g., as shielding materials for the protection of electronic devices, reduction in electromagnetic exposure, and others[11]. It has been reported that nanoparticles could provide better absorption properties in the polymer matrix than micro-sized ones; hence, nanocomposite materials could be used successfully as microwave absorbers[12].

Recent studies show that carbon filled polymer matrices can be used for electromagnetic (EM) absorption and interference shielding applications [13-18]. These include reducing electromagnetic interference among electronic components. Other areas of applications include consumer electronics, wireless LAN devices, radar absorbers, wireless antenna system, cellular phones, and others.

Ghasemi et al. [19] reported that the reflection loss of nanocomposites from MWCNTS at the frequency range of 2–18 GHz were better when compared to that of strontium ferrite nanoparticles. They showed that reflection loss improved significantly with an increase in volume percentage of MWCNTs thus indicating their potential as wide-band electromagnetic wave absorbers. Sutradhar et al. [20] demonstrated from their studies that microwave absorption of nanoparticles of Cu^{2+} doped with Li–Zn ferrite in a frequency of 8 – 18 GHz was drastically enhanced after encapsulation with a non-magnetic matrix of multi-walled carbon nanotubes (MWCNT). The microwave absorption properties of polymer composites can be tailored through changes in geometry, composition, morphology, and fractions of the filler particles[11]. In this work, we fabricated MWCNTs-epoxy composites by varying the loading fractions of MWCNTs in epoxy matrix in the range of 1 – 10 wt.%. We studied the dielectric and microwave absorption properties of the fabricated CNT-epoxy composites over a continuous frequency range in R-band (26.5-40 GHz). Our motivation for this work is to investigate microwave absorption properties of MWCNT-epoxy composites in R-band when the loading fraction of MWCNTs increases in the matrix, given that relatively lower frequencies (< 20 GHz) have been well studied.

The matrix used in fabricating these nanocomposites is the epoxy resin. Epoxy resin or polyepoxide is a thermosetting polymer that cures when mixed with a catalyzing agent or hardener. It is known for its excellent adhesion as well as chemical and heat resistance. It also has excellent mechanical strength and good electrical insulating properties, thereby making it a good candidate as a polymer matrix material when MWCNTs are dispersed in it.

2. Experiments

2.1 Materials

The MWCNTs were obtained from Cheap Tubes Inc. USA. Epoxy Resin #300 and Hardener #11 were purchased from Aeromarine Products Inc. USA. The outer diameters (OD) of the MWCNTs are in the range of 10-20nm; their length distribution is within the range of 10 - 30µm. The purity content of MWCNTs in the powder form is greater than 95 wt.%, while the ash content is less than 1.5 wt.%.

2.2 Sample Fabrication

A mechanical mixture method was employed in the fabrication of the MWCNTs–epoxy composites[21]. The MWCNTs with loading fractions of 1-10 wt.% were mixed in epoxy using a hot plate magnetic stirring machine for 1 hour at 120 rpm and 90^{o}C. The procedure is to ensure proper dispersion of MWCNTs in the epoxy resin by reducing its viscosity and eliminating the formation of air bubbles in the mixture during stirring.

Aeromarine hardener was then added with the same mass ratio as the epoxy resin and stirred carefully for about 10 minutes for pre-curing. Release Agent (PTFE: Miller Stephenson, MS-122AD) was sprayed onto the sample molds and allowed to dry for 10mins. This action is to aid the removal of sample from the molds after curing. The mixture was then infused into waveguide molds of varying dimensions and placed in the oven for post-curing at 80^{o}C for 1 hour. The waveguide molds produce two composite sample sizes of 2mm and 3mm thickness (length 7.1 mm and width 3.5 mm) after post-curing. Both samples were used for the measurements.

2.3 Instruments and Measurements

An Agilent N5230C PNA-L Microwave Network Analyzer (Agilent Company, USA) was used to measure the scattering parameters (s – parameters). Measurements were taken at room temperature. The relative complex dielectric permittivity $\varepsilon = \varepsilon' - j\varepsilon''$ was also measured by the PNA-L Network Analyzer using the Agilent Technology 85071E Material measurement software for the R-band frequency range of 26.5 – 40GHz for all the samples.

The scanning electron microscopy (SEM) images of some selected samples were obtained using Hitachi S–4500 II (Japan) with an accelerated voltage of 10 KV. Gold sputtering was first performed on all the samples for improved conductivity before taking the SEM images. X-Ray Diffraction (XRD) technique was used to characterize the microstructures of the samples using MiniFlex 600 (Rigaku, Japan), with 2θ scanning range from 10° to 80°.

3. Results and Discussion

3.1 Morphological Characterization using SEM

The dispersion of MWCNTs in epoxy enhances the microwave absorption properties of the composite. The porosity (i.e. defects) in the MWCNT-epoxy composites influences the reflection loss and absorption properties of the samples. In particular, defects could affect the morphology and functionality of the MWCNTs. Porous structures could contribute to microwave absorption properties [22-25]. Multiple reflections and scattering occur when microwave is incident on a porous structure, causing loss of electromagnetic energy [26]. Defects such as stacking faults, grain boundaries and interfaces, which can cause charge polarization and relaxation, are reported to improve microwave absorption [27-29]. It is difficult to identify accurately and quantitatively the type of defects contained in composite materials, and there is no known standards to distinguish them systematically[30].

The structural morphology of selected MWCNTs-epoxy composites with different MWCNT loadings were examined using SEM, as shown in Fig. 1. Due to the weak Van der Waals interaction force between the individual carbon tubes, the MWCNTs in the samples formed MWCNT bundles. The MWCNT bundles are sparsely dispersed in the epoxy resin at 2 wt.% MWCNT loading [Fig. 1(a)]. The MWCNT bundles become more visible in the composite as the MWCNT loading fraction increases to 9 wt.% in epoxy, as can be seen in Fig. 1(b). The SEM image of the composite sample with 9 wt.% MWCNT loading showed the cross section of dense and well dispersed MWCNTs (tiny white bundles) in the composite.

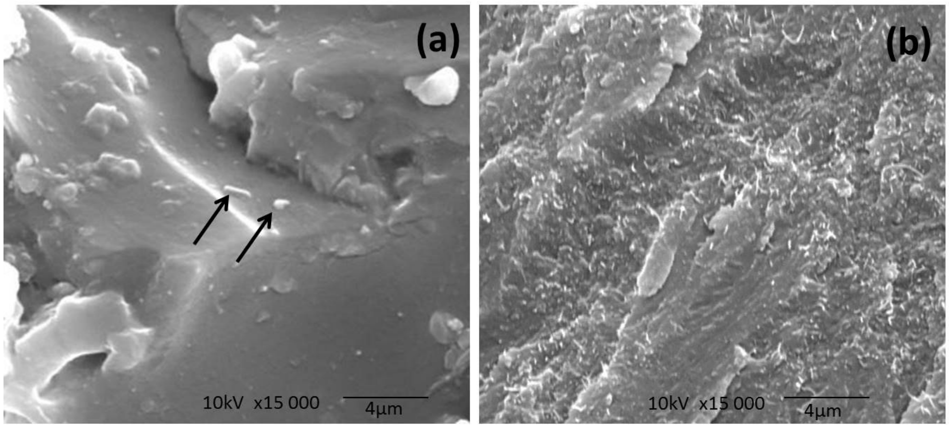

Figure 1. SEM images of MWCNT-epoxy composite samples with the MWCNT loading of (a) 2 wt.% and (b) 9 wt.%. The black arrows in (a) points to dispersed MWCNTs in the epoxy matrix. MWCNTs are much more numerous and visible (everywhere) in the 9 wt.% sample as compared to the 2 wt.% one.

3.2 X-Ray Diffraction Measurement

Fig. 2 shows the X-ray diffraction (XRD) patterns of the pure epoxy and MWCNTs-epoxy composites. The sharp narrow reflection peak at $2\theta = 26.2°$ of the MWCNTs conforms to the interlayer distance in *(002)* in the multi-walled carbon nanotubes, approximately at 3.40 Å and close to the distance between graphene layers in graphite. The weak reflection peak *(100)* of the pure MWCNTs at $2\theta = 43.6°$ implies a characteristic of turbostratic graphite lacking interlayer stacking correlation[31].

The reflection peak at $2\theta = 18.9°$ was observed for the pure epoxy sample; the peak positions slightly increase to higher diffraction angles as the loading fraction of MWCNTs increases in epoxy, indicating an interaction between the epoxy resin and MWCNTs.

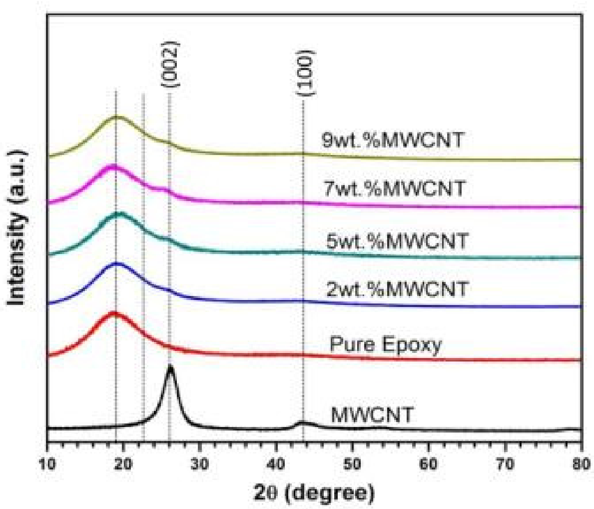

Figure 2. XRD patterns of MWCNTs, pure Epoxy, and different MWCNTs loadings in the MWCNTs-epoxy composites.

The major reflection peak positions for 2, 5, 7 and 9 wt.% of MWCNTs in the epoxy composites were observed to align with that of pure epoxy at $2\theta = 18.9°$, signifying the preservation of the microstructures of the epoxy and MWCNTs.

3.3 Complex Dielectric Permittivity.

According to the transmission line theory[32], when an electromagnetic wave is transmitted through a material, the reflectivity and absorption are affected by factors such as permittivity, permeability, frequency, and the thickness of the material or absorber. These factors may cause either dielectric or magnetic loss in the material. In this work, we measured the dielectric permittivity (real and imaginary part) of the pure epoxy and MWCNTs-epoxy composites in the frequency range 26.5 – 40 GHz. The measurement data show that real part of *the relative magnetic permeability* μ *is about 1.0 and the imaginary* part of *the relative permeability is nearly 0.0*, within the measurement *uncertainty of about ±5%, because our samples are non-magnetic.*

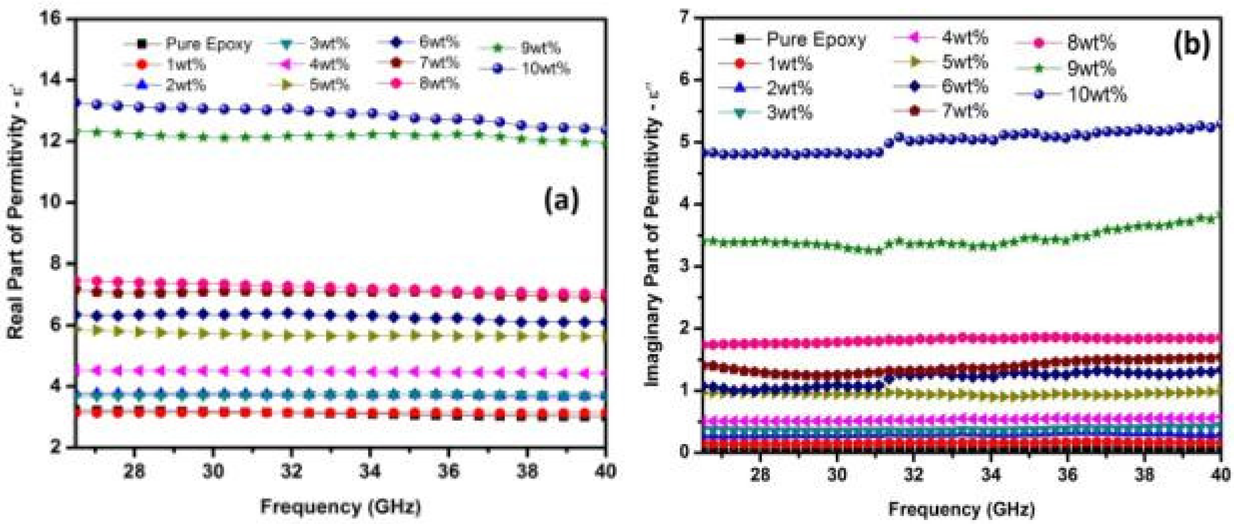

Figure 3. Real part (ε') and Imaginary part (ε'') of relative dielectric permittivity of pure epoxy and MWCNTs-epoxy composites with MWCNT loading fractions from 1 – 10 wt.%.

The measurement results showed the dependence of real part ε' and imaginary part ε'' of permittivity on the loading fractions of MWCNTs in the composites as shown in Fig. 3 [21, 33-36]. The values of ε' and ε'' increase as the loading fraction of MWCNTs increases. Substantial increases in ε' and ε'' were observed for composite samples (sample thickness is 3mm) with 9 and 10 wt.% MWCNT loading fractions [Fig 3 (a) and (b)]. The real part of the permittivity, ε', is related to a measure of the energy storage capability in the material from electromagnetic field [11]. As the loading fraction increases, free electrons gain mobility and the MWCNTs form larger aggregates that act as polarization centers. These aggregates attenuate the microwave thereby enhancing the absorption of the material [35].

Figure 3 (b) shows the dependence of imaginary part of permittivity, ε'' on the frequency. The imaginary part of the permittivity, ε'' indicates the dissipative tendency of a material to electromagnetic fields and it is related to its microwave absorption capabilities. We noticed a substantial increase in the values of ε'' for the samples with 9 and 10 wt.% MWCNT loadings [Fig 3 (b)]. The high values of ε'' in the 9 and 10 wt.% MWCNTs in the composites signify high dielectric absorption of external EM wave by the material, resulting from increased loadings of MWCNTs. The real part of the permittivity, ε' for the same samples decreases [Fig 3(a)] as the frequency increases. These phenomena of decreasing values of ε' versus increasing ε'' as the frequency increases, are understood in terms of the correlation between ε' and ε'' for the fact that the displacement current significantly lags behind the built-up potential across the sample as the electromagnetic wave frequency increases[35].

Our results showed that increasing the loading fractions of MWCNTs in the composites influences the values of ε' and ε'' which as we have seen, enhances the microwave absorption of the composite sample.

3.4 Dielectric Loss Tangent

The dielectric loss tangent of a material is a ratio of the imaginary part ε'' to the real part ε' of the permittivity. This quantity is a measure of loss in a material for a given sample thickness at a specified wavelength. It determines the attenuating factor of the material [36]. Increasing loss tangent shows improved attenuating properties in the material. Our results show that increasing the loading fraction of MWCNTs in the matrices enhances the loss tangents of the composite samples [Fig 4]. The MWCNTs-epoxy composite with 10 wt.% MWCNT loading has high loss performance: the loss tangent for the sample is 0.37 for frequencies less than 31GHz, but gradually increases up to 0.42 for frequencies in 32-40GHz range. The significant increase in the loss tangent of the composite with 10 wt.% MWCNT loading contributes to higher EM attenuation factor in the 32-40GHz range.

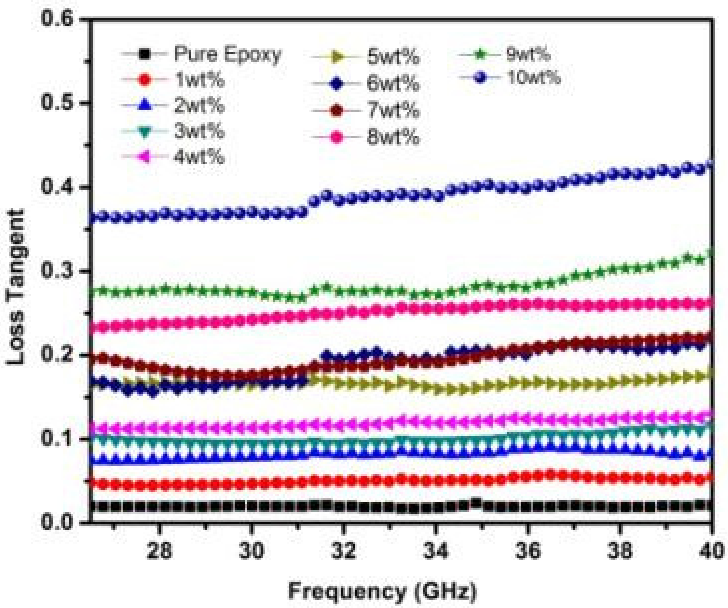

Figure 4. Dielectric loss tangents of pure epoxy and MWCNTs-epoxy samples with MWCNT loading fractions from 1 – 10 wt.%.

3.5. Microwave Absorption in the MWCNT-Epoxy Composites

When a microwave beam is incident on a material, some of its energy is reflected, absorbed, or transmitted. The transmission and reflection losses of microwave in absorbing material play an important role in applications. The transmission and reflection loss are obtained from the scattering parameters (s-parameters). We used the Agilent N5230C PNA-L Microwave Network Analyzer to measure the scattering parameters. The transmittance (*T*), reflectance (*R*), and absorbance (*A*) through the composite material can be described as below [37]:

$$T = |S_{21}|^2 \ (= |S_{12}|^2) \qquad (1)$$

$$R = |S_{11}|^2 \ (= |S_{22}|^2) \qquad (2)$$

$$A = 1 - R - T \qquad (3)$$

where S11 (or S22) and S21 (or S12) are the reflection and transmission coefficients, respectively. The absorbance A, also referred to as the absorption ratio, is a measure of the microwave absorption capability of the material under test. The transmission and reflection loss of the fabricated MWCNTs-epoxy composite samples were measured over a continuous frequency range in R-band (26.5-40 GHz).

The frequency dependence of reflection loss (RL) can also be evaluated from the complex permittivity

$(\varepsilon_r = \varepsilon_r' - j\varepsilon_r'')$ and permeability $(\mu_r = \mu_r' - j\mu_r'')$ according to the following equations[32]

$$Z_{in} = Z_0 \left(\frac{\mu_r}{\varepsilon_r}\right)^{1/2} \tanh\left[j\left(\frac{2\pi f d}{c}\right)\mu_r \varepsilon_r{}^{1/2}\right] \qquad (4)$$

$$RL = 20log\left|\frac{Z_{in} - Z_0}{Z_{in} + Z_0}\right| \qquad (5)$$

where f is the microwave frequency; d is the thickness of the absorber (in this case the CNT-epoxy composite samples); Z_0 is the impedance of air; Z_{in} is the input impedance of the absorber; and *c* is the speed of light in the vacuum.

The absorption ratio (in %) versus microwave frequency (GHz) for the 2mm and 3mm composite samples is shown in Fig. 5 (a) and (b). Clearly, the pure epoxy samples (both 2 and 3mm thickness) have very low microwave absorption capability.

Our results show that the microwave absorption in composite materials strongly depends on the loading fraction of MWCNTs in epoxy. Increase in the loading fraction of MWCNTs in epoxy substantially increases the microwave absorption. The effect of the sample thickness on the microwave absorption of the composites was observed in lower loadings of MWCNTs for frequencies lower than 34GHz.The 3mm composite samples (with 1 – 5 wt.% MWCNTs) have higher absorption ratios in the lower frequencies (below 34 GHz) than that of the 2mm sample, as showed in Fig. 5. For higher MWCNT loading fractions (6 – 10 wt.%), the microwave absorption ratio of the composite samples becomes quite complex as showed in Fig. 5 (a) and (b). This complexity is attributed to the high dielectric loss and free electron mobility in MWCNTs-epoxy composites. The formation of MWCNT aggregates [38] and the active electrons [39] in the composites with higher MWCNT loading have been suggested as the possible mechanism for this complexity. As we increase the concentration of MWCNTs in the matrix, it reaches and eventually surpasses the percolation threshold of the composite samples, thus impacting significantly on its effective dielectric and microwave absorption characteristics [11]. Once the percolation threshold is exceeded, a phase transition from an insulating to a conducting state occurs in the composite sample which also influences microwave absorption [40].

The 2mm composite sample with 7 wt.% MWCNTs has a steady absorption performance over a broad frequency band as shown in Fig. 5(a). Especially, the 2 mm composite sample with 7 wt.% MWCNTs shows quite high (45 to 60 %) microwave absorption in a wide frequency band (from 26.5 to 40 GHz). From these results, optimum loading fractions of the MWCNTs was achieved at 7 wt.%. Further increases in the loading fractions of the MWCNTs in epoxy did not significantly affect the microwave absorption capabilities of the composite samples as shown in Fig. 5 (a). Specifically, the 2mm samples with 7, 8 and 9 wt.% MWCNTs can be used as microwave absorbers in applications where a steady absorption performance is required.

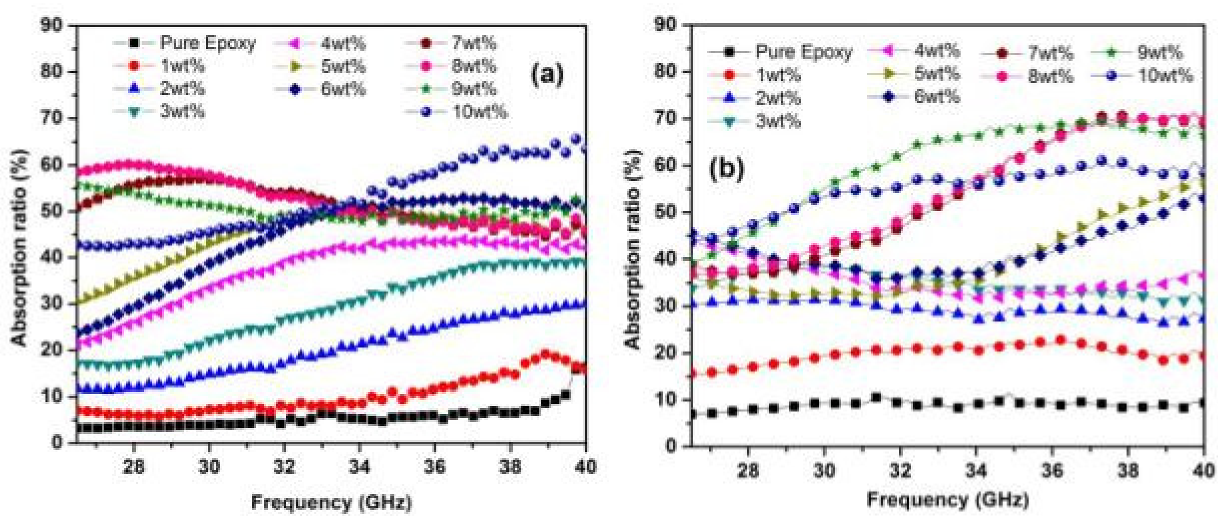

Figure 5. Absorption ratio (in %) of (a) 2mm and (b) 3mm pure epoxy and MWCNTs-epoxy samples with MWCNT loading fractions from 1 – 10 wt.%.

The microwave absorption ratio of the 3mm MWCNTs-epoxy samples with higher MWCNT loadings (7, 8, 9, and 10 wt.%) increases as the microwave frequency increases as shown in Fig. 5(b). The 3mm MWCNTs-epoxy samples with 7 and 8 wt.% MWCNTs produce high absorption ratio (about 70%) in a narrow frequency range 37 – 40GHz. The 3mm composite sample with 9 wt.% MWCNTs shows a steady microwave absorption ratio (45 to 67%) over a wider frequency range (29 – 40GHz). Increasing the MWCNT loading to 10 wt.%, for the 3mm composite sample, a lower microwave absorption was observed.

For both (2 and 3 mm) composite samples, the maximum steady absorption ratio of the microwave radiation was around 60 - 67%, showing weak dependence on the thickness of the absorber, especially at higher loading fractions of MWCNTs in the composites.

Since MWCNTs are nonmagnetic materials, their microwave absorption mainly originates either from polarization, ohmic losses, or multiple scattering. For the MWCNTs-epoxy composites, the presence of large amount of interfaces between the high aspect ratio of MWCNTs and epoxy matrix benefit the improvement of interfacial charge polarization. External electromagnetic radiation can be attenuated due to the interaction of microwave energy with charge multipoles at polarized interfaces. This will contribute to the absorption of electromagnetic energy. Interface scattering due to the difference in the effective permittivity between conductive MWCNTs and insulating epoxy host can also contributes to the microwave absorption in the composites. In addition, the free electric charges from the electrically conductive MWCNTs with relatively high MWCNT loadings in the epoxy composite will interact with electromagnetic wave, dissipate the radiation energy to heat, and contribute to the absorption of electromagnetic energy.

4. Conclusion

In this work, MWCNTs-epoxy composites were fabricated using MWCNTs (outer diameter of 10 – 20nm) with loading fraction ranging from 1 to 10 wt.%. We studied the microstructure, dielectric permittivity, and microwave absorption properties of the composites within the frequency range of R-band (26.5 – 40GHz). The 3mm MWCNTs-epoxy samples with 7 and 8 wt.% MWCNTs show high absorption ratio (about 70%) in a narrow frequency range of 37 – 40GHz. The 3mm composite sample with 9 wt.% MWCNTs shows steady microwave absorption ratio (45 to 67%) over a wider frequency range (29 – 40GHz), an indication of potential applications for steady microwave absorption. The microwave absorption of the samples is due to high dielectric loss, interfacial charge polarization, and free electron mobility of MWCNTs, by increasing the loading fractions of MWCNTs in epoxy matrix. Our result (high microwave absorption ratio up to 70%) suggest that this group of MWCNTs (OD: 10 -20nm) has potentials for high as well as for broad bandwidth microwave absorption applications.

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