Original Research Article

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ABSTRACT

The engine oil industry is faced with complex chemical reactions and difficult chemical engineering involved in the formulation of synthetic based engine oils, and therefore, the need to source for alternative base oils for engine oil formulation from vegetable oils has become urgent and inevitable. This research is aimed at formulation of lubricant using calabash seed oil (CSO). An experiment designed (Mixture Design Method using Minitab 17) was used to obtain the blend of CSO (28.75%), SN 500 (68.75%), and additive (2.50%) with improved physicochemical parameters. The lubricant obtained had kinematic viscosities 9.30 ± 2.11 cSt (at 100° C) and 53.11 ± 1.03 cSt (at 40° C), a viscosity index of 167 ± 0.51 , flash point of $240\pm2.01^{\circ}$ C, and pour point of $-28\pm1.31^{\circ}$ C. The lubricant obtained in this research had quality parameters that are comparable to those of synthesised environmentally acceptable engine oils, and are within the standard for engine oils.

Formulation of lubricant from calabash seed oil

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18 1. INTRODUCTION

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The engine oil industry is faced with numerous challenge such as renewability of the base oils [1-3], availability and accessibility of the products [1,4,5], compatibility of the products with modern machines and equipment [6], and environmental acceptability of the products [1,2,7].

Keywords: Formulation, Environment, Lubricant, Calabash Seed Oil

Leaders in the engine oil industry have accepted the challenges and are formulating specialised products in conformity with the aformentioned challenge but the formulation processes are associated with costs because of the complex chemical reactions and difficult chemical engineering involved in the production of synthetic based engine oils [6].

The use of vegetable oils for the formulation of engine oil is associated with numerous advantages. Vegetable oils have high lubricity [2,4] owing to the polar group (esters) with long carbon chains [8,9], high viscosity indexes making them useful over a wide range of temperatures [2,10], they produce fewer emissions (due to higher boiling temperature range of esters) and have high valitilities and high flash points (because of their high molecular weight) [4,10] which makes them safe for transport and storage, and they are renewable, non-toxic, and ecofriendly [1,2,11].

The challenges inherent in the use of vegetable oils include poor low temperature stability [12] because of their high pour points (making them less applicable for any application at extreme cold temperatures), poor thermo-oxidative stability [2,4] owing to the degree of unsaturation of their molecular structures [7], relatively higher initial cost of production or processing [2,5] compared to mineral oils. The use of vegetable oils for the production of environmetally acceptable engine oils is a promising development in addresing the drawbacks associated with the use of conventional mineral oils, the complex methods employed in the formulation of synthetic engine oils, and additionally, economic relevance in the local communities where vegetable oil crops are grown and processed [3-5,13-15].

This study is aimed at using calabash seed oil (CSO) for the formulation of lubricating engine oil.

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48 **2. METHODS**

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50 **2.1 Sample Collection and Treatment**

Calabash seeds (Appendix I) were obtained from Sokoto Metropolis, Sokoto State, Northwestern Nigeria, and authenticated by Botany Unit, Department of Biological Science,
Faculty of Sciences, Usmanu Danfodiyo University, Sokoto. The seeds were dehulled, dried,
ground into powder, and sieved to obtain a homogeneous powder. The powdered calabash
seed (300.00 g) was weighed and preserved for oil extraction [7,16].

57 58 **2.2 Oil Extraction**

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Soxhlet extractor (Figure 1) was employed in the extraction of calabash seed oil (CSO) with 60 61 n-hexane (6:1 w/w% of solvent/sample) as the extracting solvent (in 500 cm³ round-62 bottomed flask). The sample (50.00 g per each extraction) was placed in a thimble, while the n-hexane was heated gently (using a heating mantle). A reflux condenser was fitted (to cool 63 64 the heated n-hexane), and the mixture was heated at 60°C for 5 hours, while the condensed 65 hot-solvent soaked the timble. The solvent siphoned into the flask when it reached the top of the siphon tube of the Soxhlet apparatus [5,7]. The oil was separated from the solvent with 66 67 the aid of a rotory evaporator. The percentage yield of the CSO was calculated using 68 equation 1:

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% Yield = Weight of $Oil(g) \times 100$ / Weight of the Sample(g)

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2.3 Lubricant Formulation

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In order to achieve a better thermal and oxidative stability for the CSO [4,17], the CSO was blended with SN 500 mineral based oil and additive (poly alkylmethacrylate). A design of experiment (Mixture Design method of Minitab 17) was used to obtain the best blend with improved quality parameters from the raw CSO extract. The blend of CSO, SN 500, and additive was done in a conical flask at a temperature of 45°C, and stirred at 600 rpm for 15 minutes, while a heating mantle equipped with a magnetic stirrer was used to achieve a homogeneous mixture [4,7].

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84 **2.4 Physicochemical Parameters of CSO and the Lubricant**

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86 The CSO extract and the formulated engine oil were analysed for their physicochemical
87 properties as below (Appendix II):

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2.4.1 Determination of Kinematic Viscosity

The oils were each poured into a viscometer tube and mounted upright in the viscometric bath which was maintained at 40 or 100° C. The oil in the tube was allowed to gain equilibrium for 15 minutes. When the equilibrium temperature was achieved, the oil level in the viscometer tube was adjusted using a suction pump to 7 mm above the upper mark of the viscometer tube. The time (*f*) taken for the oil to move from the upper mark to the lower mark of the viscometer tube was recorded [7]. The kinematic viscosity (KV) was obtained via equation 2:

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105 Where, **KV** is the kinematic viscosity; **C** is the calibration constant of the viscometer; *t* is the time.

107 2.4.2. Determination of Viscosity Index

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109 Viscosity index (VI) of the oils were each obtained using values of kinematic viscosity
 110 obtained at 40 and 100°C with standard measurement table as determined by ASTM D-2270
 111 method.

112 2.4.3. Determination of Pour Point

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114 Pour point tester of accuracy of ±3°C was used to determine the pour points of the CSO and lubricating oil. The tester used methanol as the cooling solvent and has a minimun 115 temperature of -68°C. The oil (45 cm³) was poured into a test jar to the levelled mark. Then 116 the tester was cooled to -37°C. While cooling the tester, the oil jar was heated to 45°C with 117 the aid of a water bath. The oil iar was cooled with another water bath to a temperature of 118 27°C. When the pour point tester had reached -36°C, the oil jar was placed in a horizontal 119 120 position in the hole at the top of the tester and the pour point temperature was taken after 5 seconds when the oil showed no movement [4]. 121

122 **2.4.4. Determination of Flash Point**

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The flash point of the CSO and lubricating oil were each determined by heating a cup holding the oil and moving a flame over the oil at regular temperature, starting with a temperature of 28°C below the expected flash point of the oil. The bulb of the thermoneter was immersed in the sample in order to allow monitoring and reading of the temperature at flash point. The flash occured in the cup containing the CSO when the temperature of the oil had reached its flash point [7].

130 2.4.5 Determination of Free Fatty Acid

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The oil (2.00 g each of CSO and lubricating oil) was placed in a dry 250 cm³ -conical flask. 50 cm³ of ethanol and few drops (2-3) of phenolphthalein indicator were added. The mixture was heated at 60°C in a water bath for 10 minutes and then cooled. The mixture was titrated with 0.1 M KOH to the endpoint (with consistent shaking). A dark pink colour was observed and the volume of KOH used for the titration was recorded as the titre value [4]. The acid value and the free fatty acid value were calculated using equation 3 and 4:

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142 143 Acid value $\left(\frac{\text{mgKOH}}{\text{g sample}}\right) = \frac{\text{Volume KOH}(\text{cm}^3) \times \text{N KOH}(\text{mmol/cm}^3) \times 56.1 \text{ (mg/mmol)}}{\text{sample weight (g)}}$ 3

Where, **KOH** is potassium hydroxide; **N** is the molar concentration of KOH; and **56.10** is the molecular weight of KOH

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3. RESULTS AND DISCUSSION 149

150 The formulated CSO lubricant with optimum physicochemical properties was obtained from the proportion with details as CSO (28.75% wt), SN 500 (68.75% wt), and additive (2.50% 151 152 wt) (Table 1).

153 An index for evaluating the internal resistance in the motion of engine oil is kinematic 154 viscosity [18]. The higher the fluid's viscosity, the thicker it will be and more energy will be 155 needed to move an object through it [19]. Kinematic viscosities of the lubricant were found to 156 be 53.11±1.03 cSt at 40°C and 9.30±2.11 cSt at 100°C (Table 2) which are lower compared to the values for synthesised oil (Appendix III) but are within the standard for engine oils [7]. 157 158 Thus, the lubricant is useful for engine oil application.

159 The effect of changing temperatures on the kinematic viscosity of lubricating fluid is called 160 viscosity index (VI) and it is inversely proportional to temperature: a higher change in 161 viscosity in response to temperature variation indicates small viscosity index [18,20]. The 162 viscosity index of the lubricant was found to be 167±0.51 (Table 2) which is comparable to 163 the available commercial lubricating oil. This shows that the lubricant will experience less 164 change in its viscosities as a result of variations in temperatures during applications.

165 The value of flash point of the lubricant was found to be 240±2.0 °C (Table 2). Flash point is 166 a useful lubricating oil property which suggests the minimum temperature at which the oil generates ignitable vapour [21], it determines lubricant's volatility and fire resistance [22]. The 167 168 high flash point of the produced lubricant suggests a higher and complex nature of its 169 molecular structure, and hence, has low risk associated with vapourisation during transport 170 and storage.

171 However, the pour point of the lubricant was found to be -28±1.31°C (Table 2). According to 172 Gobinda et al. [23], vegetable oil base stocks solidify at low temperatures making them less 173 useful for some applications. Though the pour point of the lubricant is within the standard for 174 engine oil [7], the produced lubricant would require a calculated amount of pour point depressant (PPD) for it to be applicable in extreme low temperature conditions as compared 175 to synthesised engine oils. The PPDs will minimise the negative effects of precipitation at 176 177 low temperatures during usage.

Free fatty acid component of crude vegetable oil is an important factor used to determine the 178 179 food or oleochemical application of the vegetable oil; percentage free fatty acid greater than 180 5% suggests that the oil could be useful for the production of biodiesel, biolubricant, and 181 bioplastics [24]. The free fatty acid value of the crude extract (1.06±12) decreases to 182 0.85±12 in the formulated lubricating oil (Table 2), this is due to the effect of additive in the 183 formulated oil.

184 The result of the gas chromatography mass spectrum (GC-MS) of the extracted oil revealed 185 the degree of unsaturation of the ester carbon atoms such as $C_{20}H_{36}O_4$, $C_{21}H_{38}O_4$, and 186 $C_{23}H_{42}O_4$. The unsaturated nature of the oil extract is a factor that influence both the physical and chemical properties of the formulated lubricating oil [9,25,26]. Esters have been known 187 188 for their lubricity and are good starting materials for the production of engine oils [26]. The

presence of ester functionality was also confirmed by fourier transformed infra-red spectroscopy (FTIR) assay of the oil extract using sodium chloride plate [4] (Figure 2). Alkene stretching vibration, =CH, for the oil extract was observed at 3011 cm⁻¹, which suggests that the oil extract has methylene interrupted double bond in its molecule [27,28]. Similarly, the carbonyl functional group was observed at 1744 cm⁻¹, which suggests the presence of ester in the oil extract since there is no visible O-H absorption band (Figure 2).





Figure 1. A Set Up for the Extraction of CSO

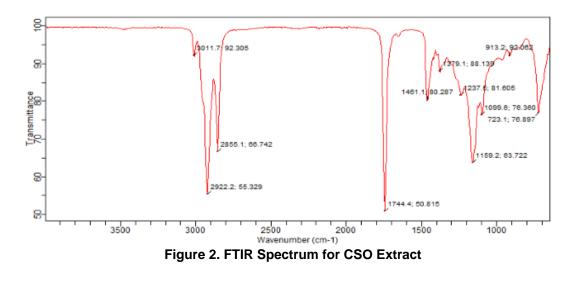


Table 1. Optimised Blends for the Lubricant Formulation

Run Order	CSO	SN 500	Additive	KV @ 100⁰C (cSt)	KV @ 40 ⁰ C (cSt)	VI	FP (°C)	PP (°C)
1	0.00	90.00	10.00	9.00	89.20	75	233	-10
2	68.75	23.75	7.50	8.02	34.43	219	146	-13
3	23.75	68.75	7.50	10.50	50.18	207	241	-19
4	90.00	0.00	10.00	8.11	20.44	270	153	-24
5	28.75	68.75	2.50	9.31	53.00	166	238	-28
6	68.75	28.75	2.50	7.70	41.30	163	144	-16
7	10.00	90.00	0.00	10.70	65.20	157	236	-14
8	28.75	68.75	2.50	9.30	53.11	167	240	-28
9	90.00	0.00	10.00	8.11	20.62	268	153	-23
10	23.75	68.75	7.50	10.51	50.13	208	241	-18
11	90.00	10.00	0.00	8.60	44.90	172	166	-28
12	68.75	28.75	2.50	7.60	41.90	155	145	-15
13	68.75	23.75	7.50	8.02	34.47	217	145	-13
14	47.50	47.50	5.00	9.59	49.32	183	232	-29
15	0.00	90.00	10.00	9.50	89.17	85	231	-11
16	90.00	10.00	0.00	8.60	44.90	174	164	-27
17	47.50	47.50	5.00	9.50	49.32	182	233	-28
18	10.00	90.00	0.00	10.70	65.20	156	236	-14

Key: **CSO** = Calabash Seed Oil; **KV** = Kinematic Viscosity; **VI** = Viscosity Index; **FP** = Flash Point; **PP** = Pour Point

Parameters	Units	CSO	Lubricant	Engine oil range*
Kinematic Viscosity @ 40°C	cSt	21.78±1.22	53.11±1.03	> 28.80
Kinematic Viscosity @ 100°C	cSt	6.55±1.01	9.30±2.11	> 4.10
Viscosity Index		266±2.11	167±0.51	> 90.00
Flash Point	°C	145±1.01	240±2.01	> 150.00
Pour Point	°C	-11±0.01	-28±1.31	< -5.00
Free Fatty Acid	mg KOH g ⁻¹	1.06±12	0.85±12	-

Key: **CSO** = Calabash Seed Oil; (\pm) = Mean Value Plus or Minus Standard Deviation (n = 3); (*) = Owuna et al., 2018

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224 4. CONCLUSION

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226 This research was undertaken in order to formulate engine oil from calabash seed oil. The 227 results obtained showed that a blend of CSO with mineral based oil and additive gave a 228 formulation of lubricant that has parameters that are within the standard for engine oils and 229 are comparable to commercially available engine oils. The chemical assay of the calabash 230 seed extract revealed ester functionality which makes the oil good base oil for the formulation or synthesis of lubricating oil. The lubricant can be used as substitute for any 231 232 applications where synthesised engine oils are applicable if thermo-oxidative stability of the oil can be validated, and requisite (tailor-made) additive is incorporated in the formulation. 233

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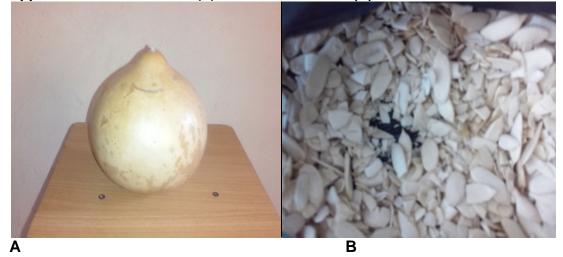
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321 **DEFINITIONS**

- 322 **ASTM** = American Society for Testing and Materials
- 323 CSO = Calabash Seed Oil
- 324 **FTIR** = Fourier Transform Infra-Red Spectroscopy
- 325 **GC-MS** = Gas Chromatograpy Mass Spectroscopy
- 326 **HTHS** = High Temperature High Shear
- 327 **mg/l** = Milligram per Litre
- 328 **mPa** = Millipascal
- 329 **SEA** = Society of Automotive Engineers
- 330 Wt% = Weight Percent

331332 APPENDIX

Appendix I: Calabash Fruit (A) and Dehulled Seeds (B)



Appendix II: Analyses of Oils in Progress OVH Energies & Marketing, Kaduna,
 Nigeria



350 Appendix III: Fully Synthesised Mobil 1 5W-30 Oil (Mobil) Technical Data

Sheet

Typical Properties

Mobil 1 5W-30			
SAE Grade	5W-30		
Viscosity @ 100°C, cSt (ASTM D445)	11.0		
Viscosity, @ 40°C, cSt (ASTM D445)	61.7		
Viscosity Index	172		
Sulfated Ash, wt% (ASTM D874)	0.8		
HTHS Viscosity, mPa•s @ 150°C (ASTM D4683)	3.1		
Pour Point, °C (ASTM D97)	-42		
Flash Point, °C (ASTM D92)	230		
Density @15.6 °C, mg/l (ASTM D4052)	0.855		

Source: http://mobil.moovelub.com/sites/default/files/mobil_1_5w-30.pdf