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8**Original Research Article****Geophysical and Geotechnical Studies of a Proposed
Structure at Akure, Southwestern Nigeria.****Abstract**

Geophysical and geotechnical studies were carried out at a proposed location for the construction of a multi-storey structure in Akure, Southwestern, Nigeria. The aim was to ascertain the suitability of this location for both Founding and Engineering structures. The geophysical investigation involved the Vertical Electrical Sounding (VES) technique using the Schlumberger configuration, Dipole-Dipole Horizontal Profiling and a geotechnical investigation. A total of twenty one (21) VES and five (5) Cone Penetration Test (CPT) locations were occupied within the study site. Dipole-Dipole Horizontal Profiling was occupied along traverses 1 and 2 within the investigated area. The electrode separation varies from 1 to 75 m. The investigation delineated three major layers which are topsoil, which is excavated before any foundation is laid. The second layer delineated was lateritic and the last was weathered layer. From the result obtained, depth to lateritic layer ranges from 1.1 to 9.0 m while resistivity defining the lateritic layer ranges from 150 Ω m to 792 Ω m. Some of the sounding curves generated over the VES stations and Dipole-Dipole Horizontal Profiling fairly correlated with those of the CPT profile. The high cone penetration resistance recorded at CPT point 4 and 5 is manifested as high geoelectric resistivity values recorded at VES 13. This shows that the soil has fairly low clay content. It also seen from the study that the geophysical studies has a greater depth penetration, and it also provide better layer characterization compared to geotechnical studies. The choice of foundation material, clay content and topography elevation should be taken into cognizance, since the load bearing capacity of the lateritic layer was appreciably high.

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Key Words: Vertical electrical sounding, cone penetration test, dipole-dipole, foundation integrity.

Introduction

The Earth is complex in nature and very inhomogeneous in fracture distribution. The complexity of the earth materials is more pronounced in the basement complex regions while in the sedimentary terrain the soil properties may be fairly uniform over long distance. While some areas are underlain by shallow bedrock or materials of higher load bearing capacity, others may have significant superficial soil cover [2]. The near surface bedrock is a very good foundation support material as the load bearing is infinity high. In areas of thick overburden cover, the materials could have variety of engineering

38 properties. While some may be very weak especially where the clay content is high others may be of
39 high load bearing capacity especially if the aggregates are *gravelly*. The rate of failed structures in
40 Nigeria has increased in recent times [8]. These structural failures are in most cases associated with
41 the problem of poor quality of building materials, old age of buildings and improper foundation. In
42 recent times, the land expanses in Akure have been opened to rapid development [7]. Despite this
43 rapid growth and development, the impact of subsurface geologic structures in the area on the
44 durability and easy maintenance of the erected structures have been seldom discussed. Vertical and
45 near vertical cracks or discontinuities have been noticed in the walls of both old and recent buildings
46 [4]. This assertion can be attributed to the minimal attention paid towards the use of geophysics in
47 foundation studies. In Engineering Geophysics and site investigation, structural information and
48 physical properties of a site are sought [10]. This is so because the durability and safety of the
49 engineering structural setting depend on the competence of the material, nature of the subsurface
50 lithology and the mechanical properties of the overburden materials [1]. Foundations are affected not
51 only by design errors but also by foundation inadequacies such as sitting them on incompetent earth
52 layers. For CPT, a cone at the end of a series of rods is pushed into the ground at a constant rate, and
53 measurements are made of the resistance to the penetration of the cone. This is known as “cone
54 resistance” or q_c , which is the total force (Q_c) acting on the cone divided by the projected area (A_c) of
55 the cone. The cone resistance q_c is a direct indicator of the strength of the soil at a given depth. Cost,
56 efficiency, speed, simplicity, reliability, and the ability to provide near continuous information on the
57 soil properties with depth are the important reasons for the increasing popularity of CPT [3]. The
58 primary significance of CPT comes from the fact that it represents a miniature driven pile or
59 foundation in soil; hence, the pile bearing capacity (pressure between a foundation and the soil which
60 will produce shear failure in the soil) can be directly estimated from q_c . Thus, CPT provides valuable
61 constraints for all settlement and stability calculations. CPT q_c responds to soil changes within five to
62 ten times the cone diameter (standard = 35.6 mm) above and below the cone. It should be noted that
63 valuable information that is provided by CPT is limited to its location [6]. CPTs are commonly
64 performed tens or hundreds of meters apart. Soil models based on lateral interpolation of CPT data
65 collected at a few locations at a given site obviously contain large uncertainties, increasing the risk in
66 engineering design.

67 This target of this work is to reveal the use of Geophysical and Geotechnical approaches as a reliable
68 means of undertaking studies of construction sites as related to the Geologic nature of the
69 environment thereby saving a lot of time and cost. Also, with the art of these methods, the basic
70 problems of structures that have emerged problematic can be investigated and remediation actions can
71 be taken.

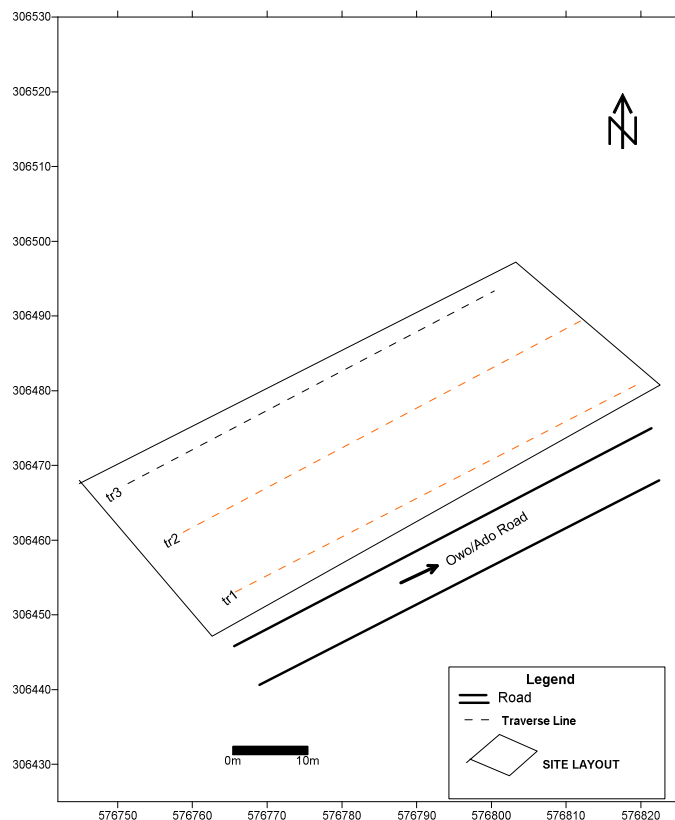
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73 **Description of the Study Area**

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75 The studied area is located within the Akure metropolis along Alagbaka, the capital city of Ondo State
 76 (Figure 1). It is situated between the UTM coordinates of Eastings 576759 - 576820 m and Northings
 77 306455 - 306498 m. The study area is located within the sub-equatorial climatic belt of the tropical
 78 rain-forest with evergreen and broad-leaved trees with luxuriant growth layer arrangement. The area
 79 is characterized by uniformly high temperature and heavy well distributed rainfall throughout the
 80 year. The average annual temperature ranges between 24⁰C and 27⁰C, while the rainfall is mostly
 81 conventional, peaks twice in July and September and varies between 1500mm and 2000mm per
 82 annum.

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87 Figure 1. Base Map of the Study Area

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91 **Geology of the study area**

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Akure is located within the crystalline basement complex terrain of the southwestern Nigeria.

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The area is generally underlain by basement rocks categorized by [9] as migmatite gneiss, quartzite, polytic schist, biotite granite, charnockite, granite gneiss and porphyritic granites.

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The main outcrops in the area are migmatite gneiss, porphyritic granite and charnockite,

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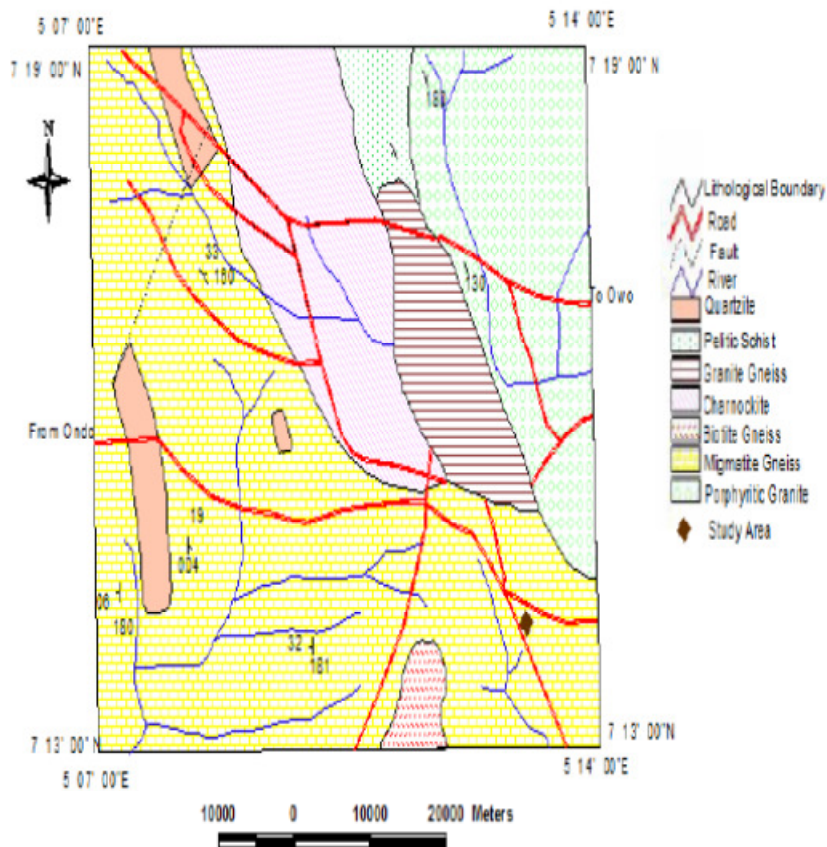
while biotite occurs as a discrete body at the southern part of the area as shown in the Figure

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2. The study area is underlain by migmatite gneiss which is a coarsely grained crystalline

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metamorphic rock having quartz, feldspar and mica as its constituent. Biotite granite.



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101 Figure 2. Geological Map of Akure Showing the Study area

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103 **Methodology**

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105 **Geophysical Survey**

106 Three traverses of about 70 m were established in an approximate E - W direction (Figure 3). The
 107 electrical resistivity method utilized the dipole-dipole profiling and the vertical electrical sounding
 108 (VES) techniques. The dipole-dipole survey was used to determine the lateral and vertical variation in
 109 apparent resistivity of the subsurface beneath the three established traverses. The VES involved the
 110 use of Schlumberger array. Twenty one (21) sounding stations were occupied along the three
 111 established traverses and the current electrode spacing (AB/2) was varied from 1 to 65 m. In order to
 112 process the electrical resistivity data, the apparent resistivity values were plotted against the
 113 electrode spread (AB/2). This was subsequently interpreted quantitatively using the partial curve
 114 matching method and computer assisted 1-D forward modeling with WinResist 1.0 version software
 115 [11]. The dipole-dipole data were inverted into 2-D subsurface images using the DIPPRO™ 4.0
 116 inversion software [5]. 2-D electrical imaging of the subsurface was obtained using dipole-
 117 dipole configuration. The inter-electrode spacing of 5 m was adopted while inter-dipole

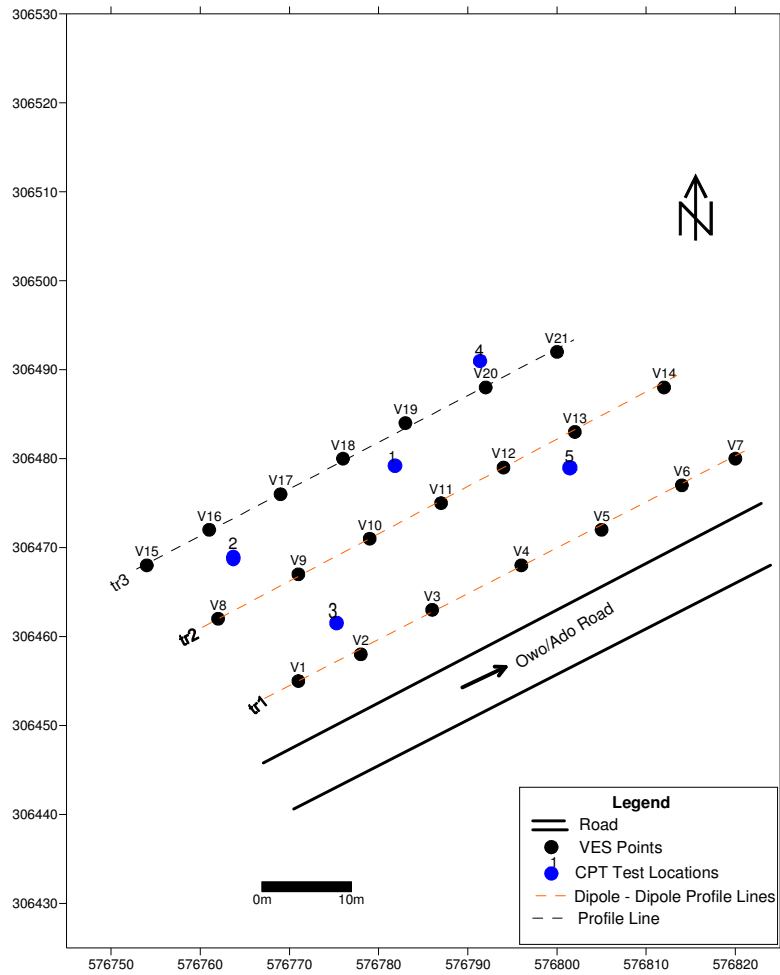
118 expansion factor (n) was varied from 1 to 5. Resistivity values were obtained by taking
119 readings using the ohmega resistivity meter.

120 **Geotechnical Survey**

121 Cone Penetration tests were performed at a total of five (5) locations within the study area (Figure 3).
122 The tests were carried out to a depth of 4.5 m. The Dutch static penetration measures the resistance of
123 penetration into soils using apex angle of 60° and a base of 10 sq cm. The cone Penetrometer test is a
124 means of ascertaining the resistance of the soil. The layer sequences are interpreted from the variation
125 of the values of the cone resistance with depth. The test was carried out by securing the winch frame
126 to the ground by means of anchors. These anchors provided the necessary power to push the cone into
127 the ground. The cone and the tube were pushed together into the ground for 20 to 25 cm; the cone was
128 pushed ahead of the tube for 3.5 cm at a uniform rate of about 2 cm/sec. The resistance to the
129 penetration of the cone registered on the pressure gauge connected to the pressure capsule was
130 recorded. The tube was thereafter pushed down and the procedure enumerated above was repeated.
131 Cone resistance and sleeve friction are plotted against depth using the series of recorded gauge
132 readings obtained. The resistance profile was then obtained by plotting corresponding cone and
133 successive cone and sleeve resistances readings against depths. The profiles were correlated with
134 geophysical data to provide information on the variation of strata and material strength across the site.

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139 Figure 3: Data acquisition Map of the Study Area.

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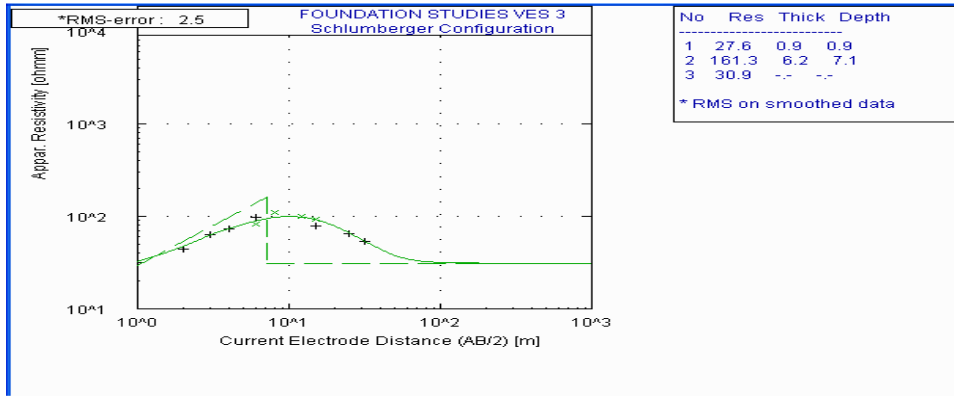
141 **Results and Discussion**

142 The results of the study were presented as Sounding curves geo-electric sections, pseudo sections and
143 graphs

144 **Characteristic of the VES curves**

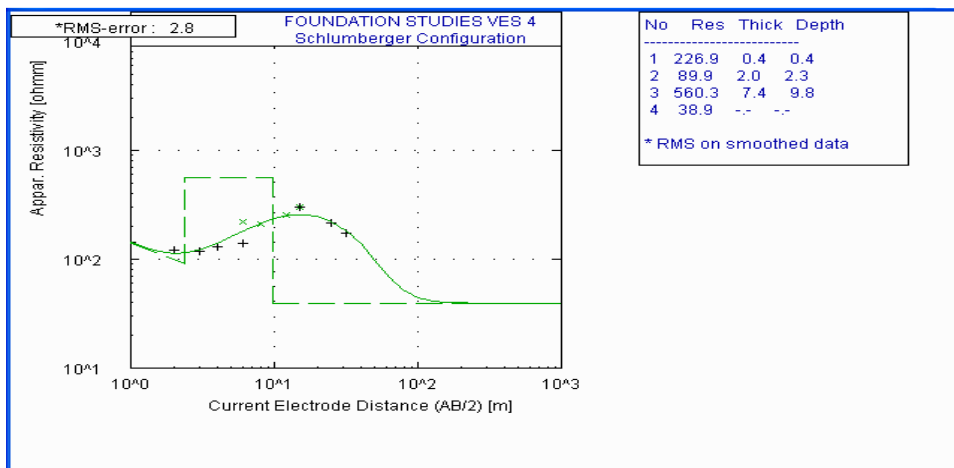
145 Curves types identified ranges from K, Q, KH, HK and KHK varying between three to five geo-
146 electric layers. The KH curve type predominating. Typical curve types in the area are as shown in
147 Figure 4(a-e)

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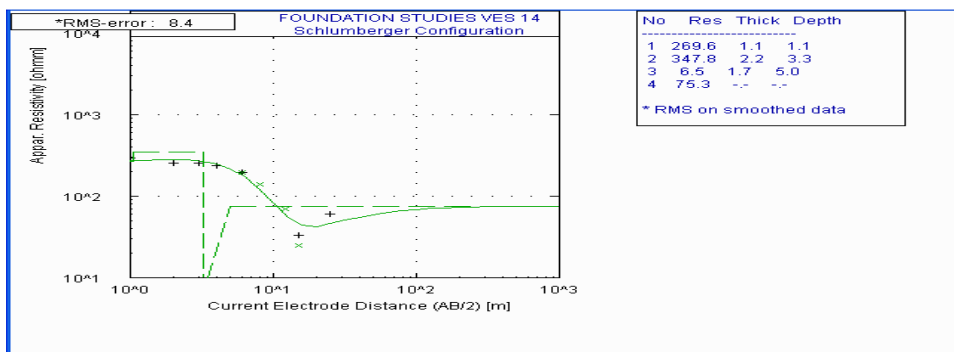
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Figure 4a. Typical 'K' Sounding Curve



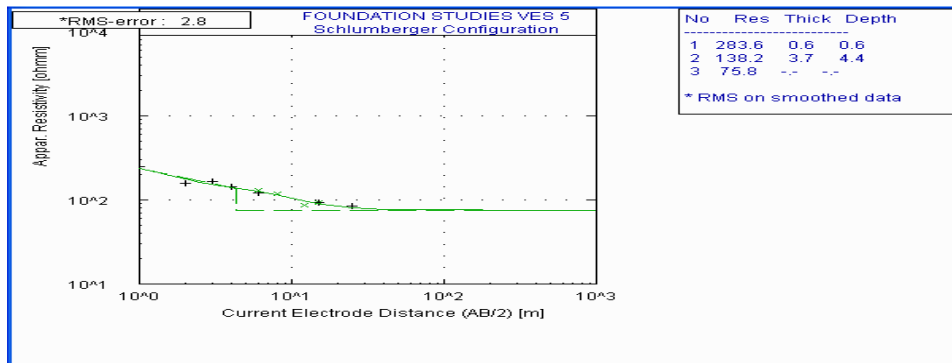
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Figure 4b. Typical 'HK' Sounding Curve



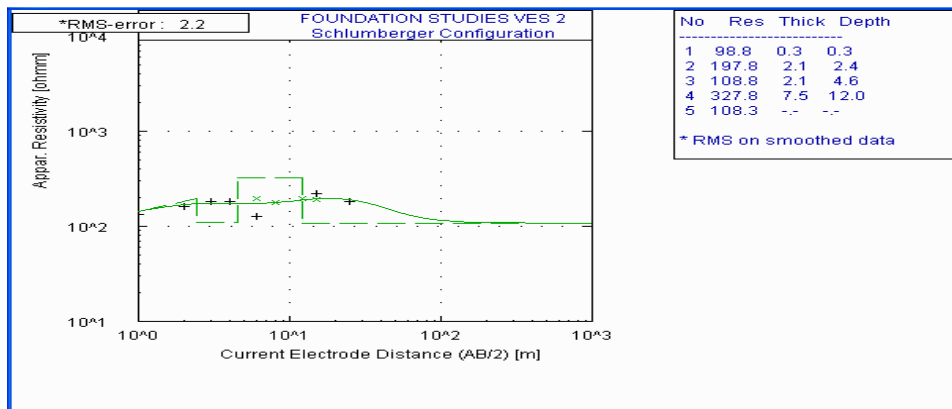
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Figure 4c. Typical 'KH' Sounding Curve



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Figure 4d. Typical 'Q' Sounding Curve



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Figure 4e. Typical 'KHK' sounding curve

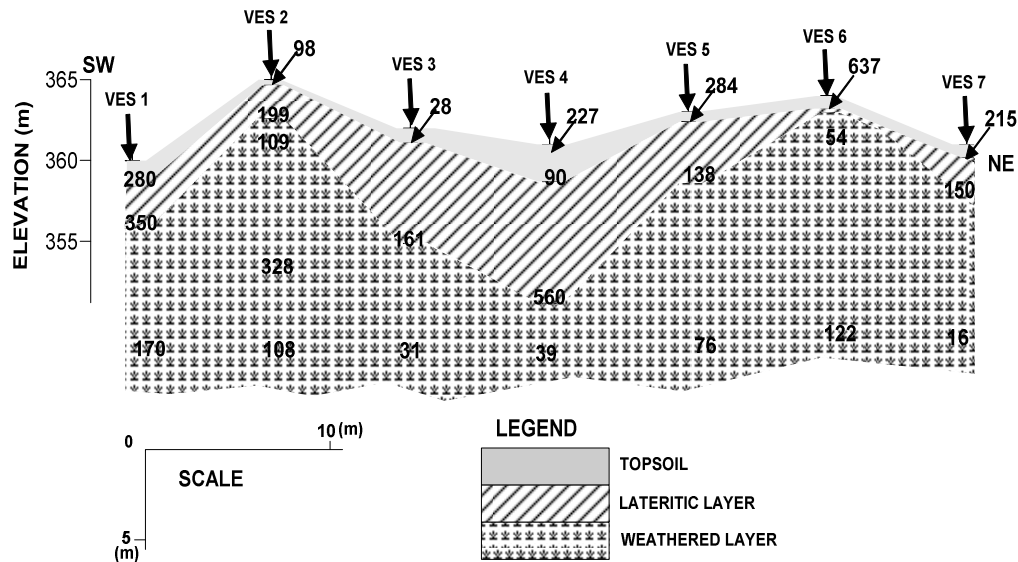
Goelectric and Lithological characteristic along the three Traverses

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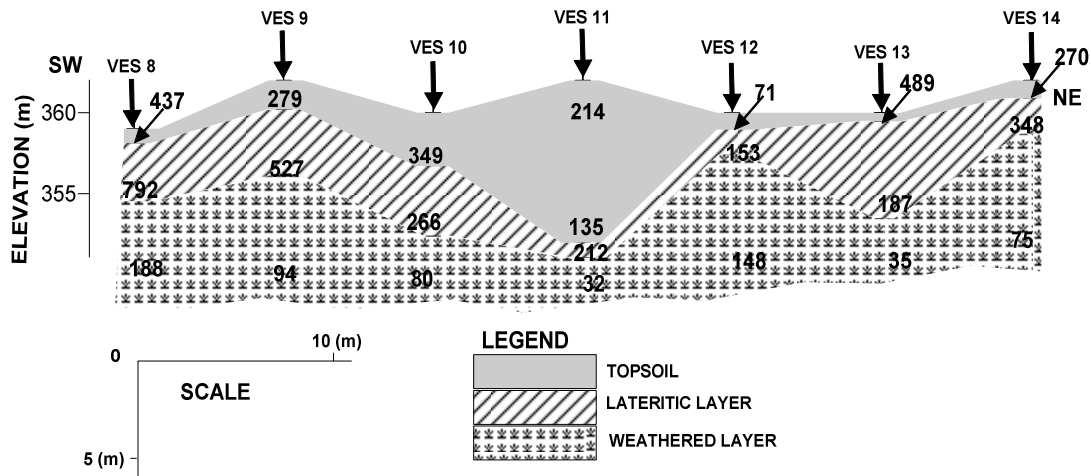
The geo- electric sections were represented by the 2-D view of the geo-electric parameters (depth and resistivity) derived from the inversion of the electrical resistivity sounding data. The goelectric section along Traverse 1 (Figure 5a) attempted to correlate the goelectric sequence across the study area. The goelectric sections identified three goelectric/geologic subsurface layers. The topsoil comprising of clay, clayey sand and sandy clay with the resistivity values ranges from 28 to 637 Ω-m with its thickness varies from 0.3 to 1.6 m, the clayey coarse sand/laterite resistivity values range from 138 to 560 Ω-m and thickness ranges from 2.1 to 7.4 m while the weathered layer resistivity varies from 16 to 122 Ω-m. the resistivity values of the topsoil are indicative of clay, sandy clay and clayey sand. This layer may not be of any special interest since topsoil is normally excavated. Hence, foundation of the proposed structures cannot be found on this layer.

On Traverse 2 (Figure 5b), three subsurface geologic layers were also delineated along this traverse. From the goelectric section, the top soil, lateritic layer and weathered layer were determined. The topsoil comprising of clay, clayey sand and sandy clay with the resistivity values ranges from 71 to 489 Ω-m with its thickness varies from 0.5 to 7.0 m, the clayey coarse sand/laterite resistivity values range from 153 to 792 Ω-m and thickness ranges from 1.1 to 9.0 m while the weathered layer

188 resistivity varies from 32 to 188 Ω -m. the resistivity values of the topsoil are indicative of clay, sandy
 189 clay and clayey sand. This layer may not be of any special interest since topsoil is normally
 190 excavated. Hence, foundation of the proposed structures cannot be found on this layer.
 191 On Traverse 3 (Figure 5c), three subsurface geologic layers were also delineated along this traverse.
 192 From the geo-electric section, the top soil, lateritic layer and weathered layer were determined. The
 193 topsoil comprising of clay, clayey sand and sandy clay with the resistivity values ranges from 58 to
 194 493 Ω -m with its thickness varies from 0.7 to 1.0 m, the clayey coarse sand/laterite resistivity values
 195 range from 175 to 523 Ω -m and thickness ranges from 1.9 to 6.8 m while the weathered layer
 196 resistivity varies from 31 to 168 Ω -m. the resistivity values of the topsoil are indicative of clay, sandy
 197 clay and clayey sand. This layer may not be of any special interest since topsoil is normally
 198 excavated. Hence, foundation of the proposed structures cannot be found on this layer.
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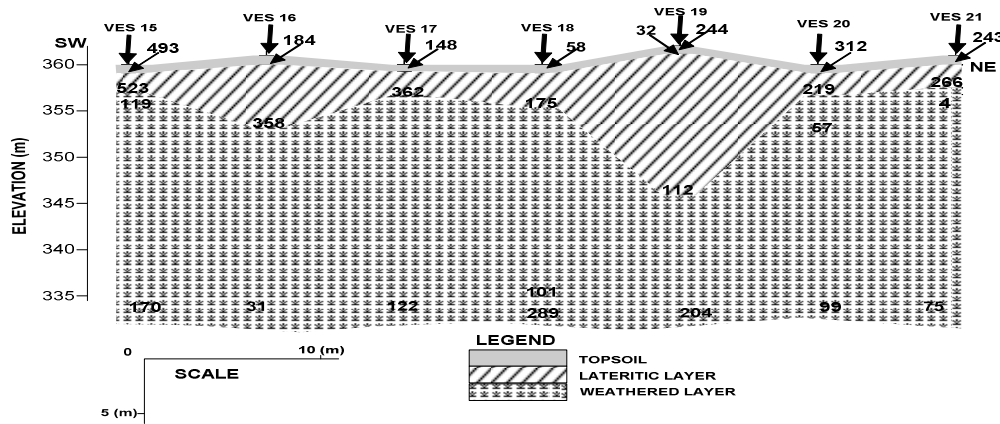


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 204 Figure 5a. Geoelectric Section along Traverse one
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Figure 5b. Geoelectric Section along Traverse two



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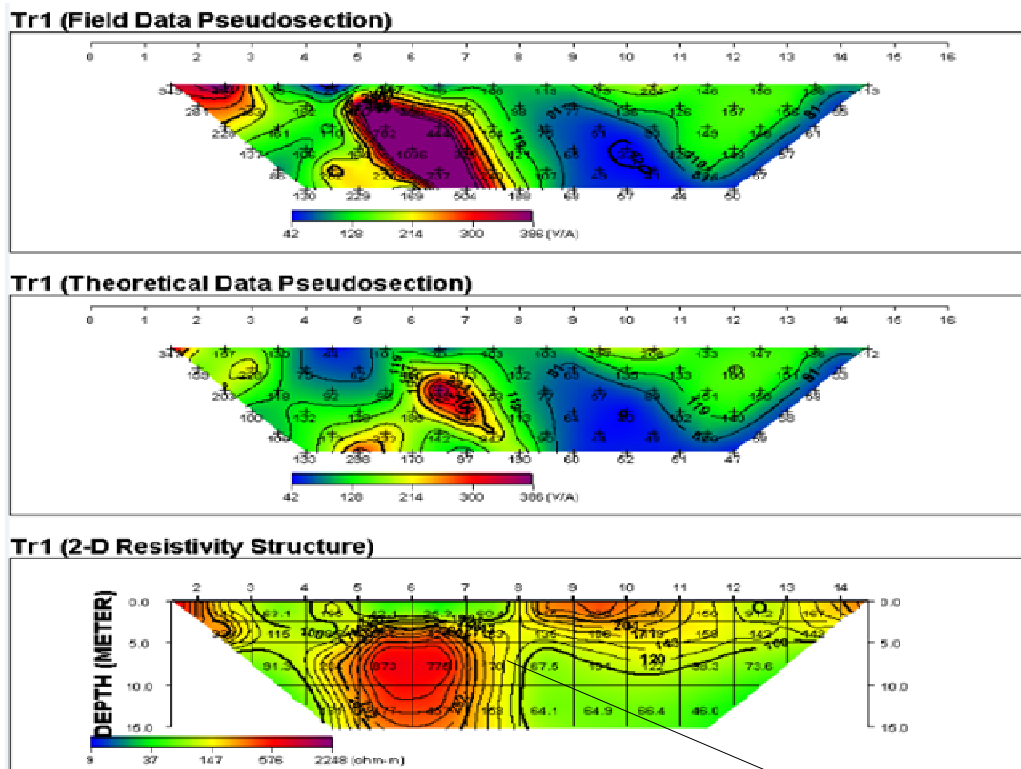
Figure 5c. Geoelectric Section along Traverse three

222 Dipole-dipole Pseudosections

223 The 2-D Pseudosection was produced from the dipole-dipole data taken along the two traverses
 224 (Figure 6a, b). It was set up to have a 2-Dimensional clear view of the subsurface because it shows an
 225 interpretation of unilateral data and its contours. These also have information as the geoelectric
 226 section. It delineated topsoil, weathered/fractured layer (thickness 5 to 12 m) and the fresh bedrock.
 227 The resistive parts are seen at the lower part of the section which is the fresh bedrock while the green
 228 and blue coloured parts are the fractured part of the section. A suspected linear feature was delineated
 229 at distance 40 to 65 m (Figure 6a).

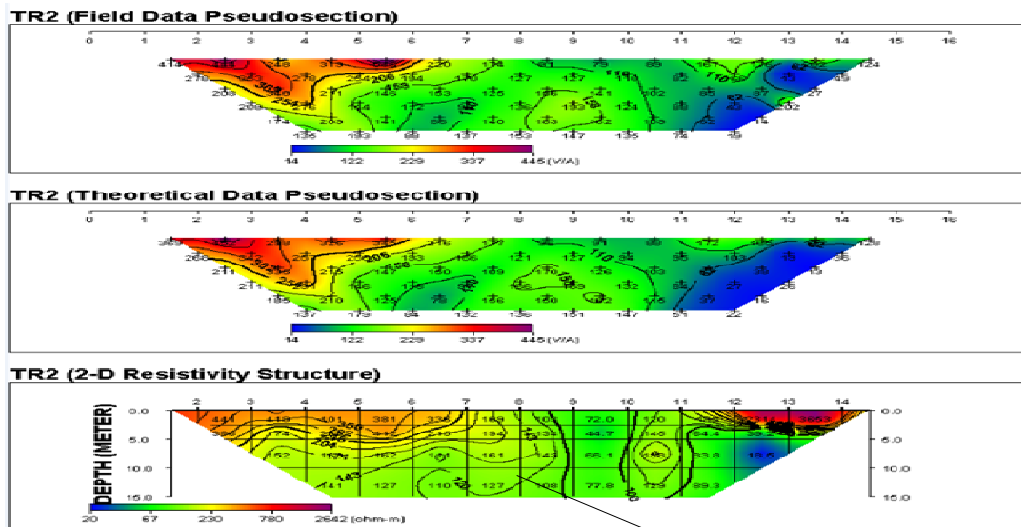
230 The 2-D pseudo-section was also produced from the dipole-dipole data taken along Traverse 2 (Figure
 231 6b). These also have information as the geoelectric section. It delineated topsoil, weathered/fractured
 232 layer and the fresh bedrock. The highly resistive parts are seen at the upper part of the section which

233 is the fresh bedrock while the green and blue coloured parts are the weathered/fractured part of the
 234 section. A suspected linear feature was delineated at distance 35 to 60 m along Traverse 2
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Figure 6a. Dipole – Dipole Horizontal Profiling along traverses 1

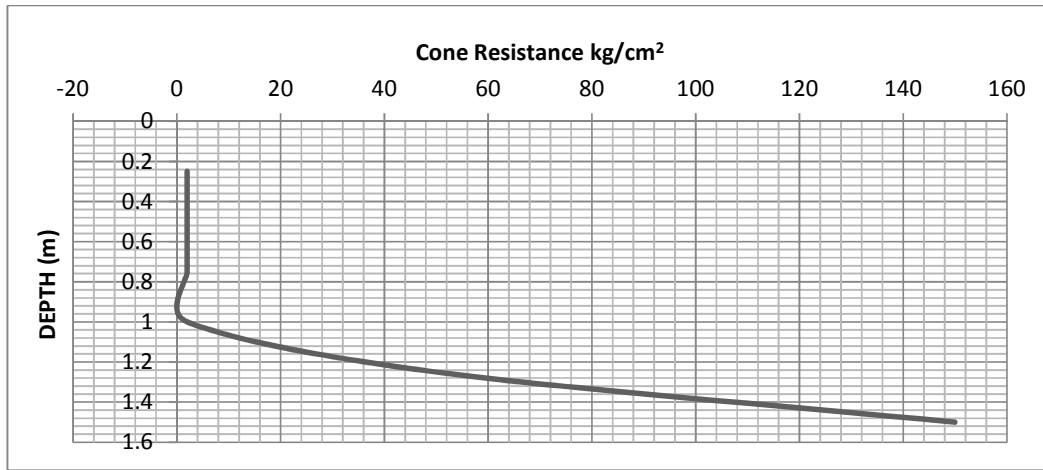


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Figure 6b. Dipole – Dipole Horizontal Profiling along traverses 2

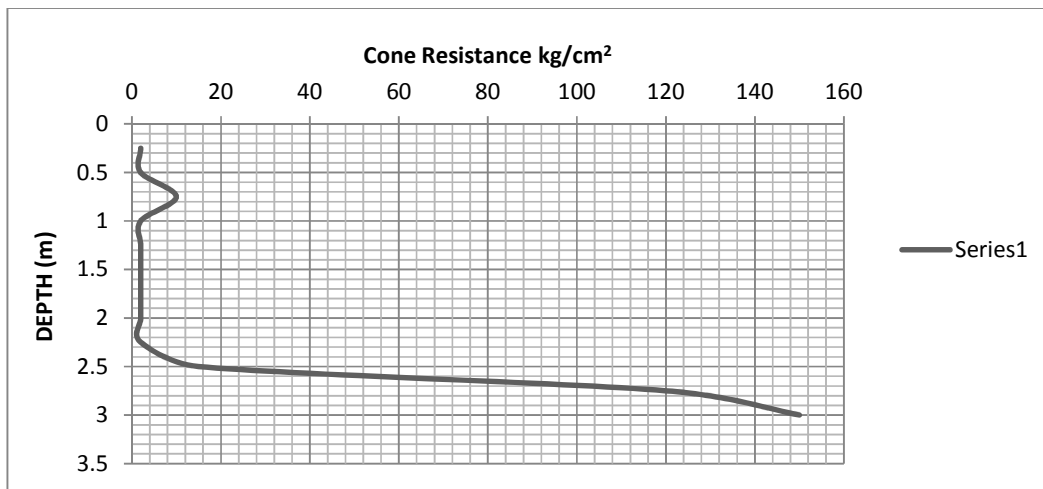
243 **Geotechnical Results**

244 The Cone penetration test plots Figure 7(a-e), varies from 2bar to 150bar with a maximum depth of
 245 4.25 m. The layer sequences were interpreted from variation of the values of the cone resistance
 246 plotted against depth. The CPT points have very low cone resistance values. This illustrates that the
 247 soil consists of conductive clayey materials.



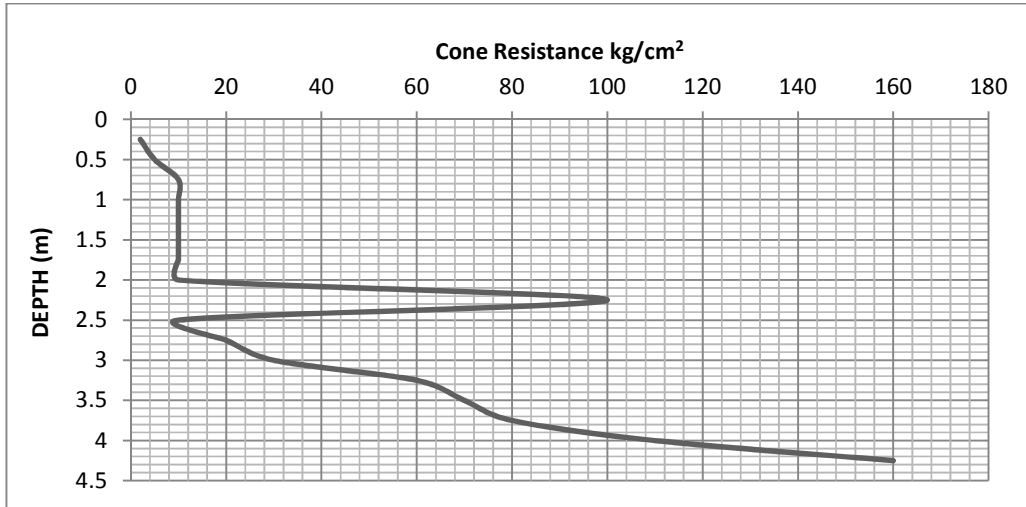
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Figure 7a. CPT Test carried out in point 1



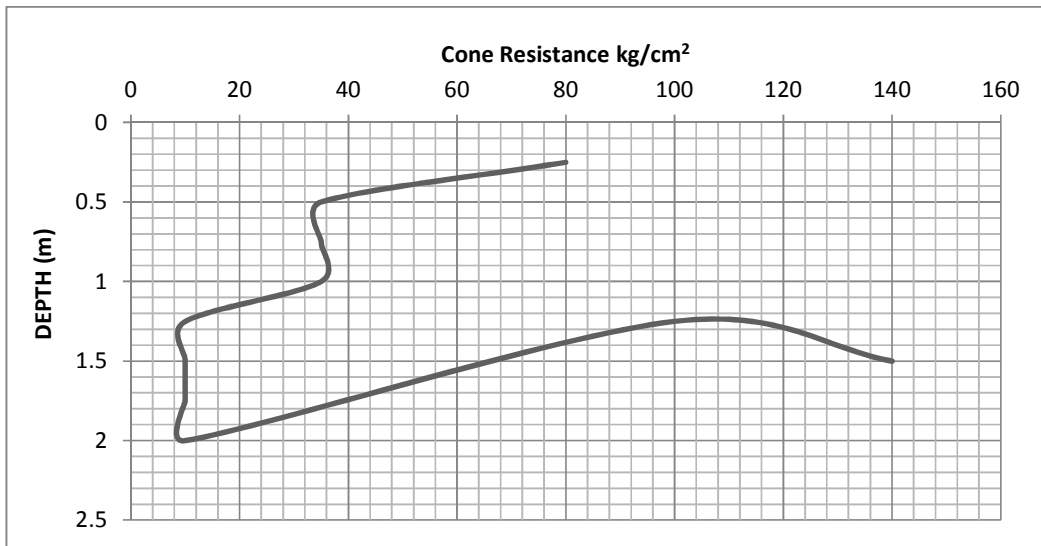
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Figure 7b. CPT Test carried out in point 2



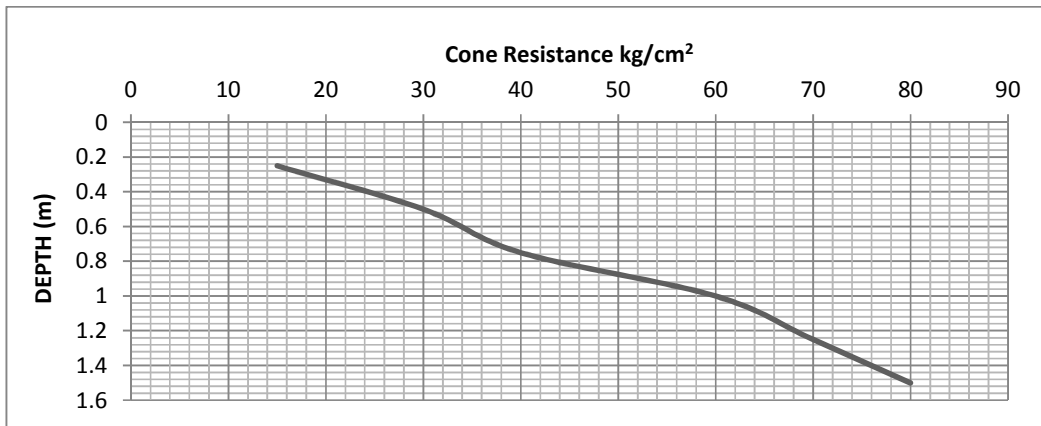
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Figure 7c. CPT Test carried out in point 3



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Figure 7d. CPT Test carried out in point 4



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Figure 7e. CPT Test carried out in point 5

270 **Comparison of Geophysical and Geotechnical Results**

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272 The result obtained from geophysical and geotechnical studies displays similar trend. The geoelectric
273 section, dipole-dipole pseudosections and cone penetration charts illustrates that where there is an
274 increase in apparent resistivity increase in resistance was also recorded. The high cone penetration
275 resistance recorded at CPT points 4 and 5 was manifested as high geoelectric resistivity values
276 recorded at VES 13. This shows that the soil has fairly low clay content. The difference between both
277 methods is that the depth of penetration is higher for electrical resistivity method. Increases in
278 resistivity value were observed at point where the penetration of the cone becomes impossible.
279 Therefore, both methods can serve as a tool in imaging the nature of the subsurface.

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282 **Conclusion**

283 The study has shown the relevance of geophysical site study for foundation design consideration. It
284 can effectively complement the routine geotechnical studies. Geophysics therefore remains a very
285 vital tool which can be applied in civil engineering work. The investigation delineated three major
286 layers which are topsoil, which will be excavated before any foundation can be laid. The second layer
287 delineated was lateritic and the last was weathered layer. From the result obtained, depth to lateritic
288 layer ranges from 1.1 to 9.0 m while resistivity defining the lateritic layer ranges from 150 Ω m to 792
289 Ω m. Some of the sounding curves generated over the VES stations and Dipole-Dipole Horizontal
290 Profiling were fairly correlated with those of the CPT profile. The high cone penetration resistance
291 recorded at CPT point 4 and 5 was manifested as high geoelectric resistivity values recorded at VES
292 13. This shows that the soil has fairly low clay content. it can also be seen from the study that the
293 geophysical studies has a greater depth penetration, and it also provide better layer characterization
294 compared to geotechnical studies. The choice of foundation material, clay content and topography
295 elevation should be put into consideration, since the load bearing capacity of the lateritic layer is
296 appreciably high.

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