

# EFFECT OF CONSERVATION TILLAGE ON THE SOIL PHYSICAL AND MECHANICAL PROPERTIES

## ABSTRACT

Effect of different tillage methods on soil physical and mechanical properties was evaluated in this research. A split plot experimental design with nine treatments and six replications was used for soil bulk density and penetration resistance. Main plots were tillage methods including conventional tillage, reduced tillage, and zero tillage. Soil depth ranges of 0 to 100, 100 to 200, and 200 to 300 mm were considered as sub plots. Soil bulk density, soil penetration resistance, coefficients of soil internal and external friction, adhesion, and cohesion were measured. Collected data were analyzed (one way ANOVA) using SAS statistics software and Duncan's multiple range tests were used to compare the treatments means. Results showed that tillage methods had a significant effect on the soil bulk density so that the conventional and reduced tillage methods had the lowest soil bulk density, and zero tillage method had the highest one. Soil bulk density was also affected by soil depth in such a way that bulk density increased when soil depth increased from 0 to 200 mm, and then decreased by increasing soil depth from 200 to 300 mm. The maximum soil penetration resistance was obtained from the zero tillage; while, the conventional tillage had the minimum soil penetration resistance. Soil penetration resistance increased with increasing soil depth from 0 to 300 mm. Results also indicated that zero tillage significantly decreased the coefficient of soil internal friction; whereas, the coefficient of soil external friction was not affected by tillage methods.

**Keywords:** Bulk density; friction coefficient; penetration resistance; Soil depths; tillage methods

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## INTRODUCTION

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Conventional tillage system is being replaced in the world by the conservation tillage method in which at least 30% of soil surface remains covered by crop residues. Transition from the conventional tillage method to the conservation system may affect the soil physical and mechanical properties such as soil bulk density, soil penetration resistance, and soil internal and external coefficients of friction. Soil bulk density and penetration resistance are used as indices of soil compaction so that by increasing these two indices, soil compaction increases and increasing soil compaction may prevent water and crop root penetration in the soil. Soil bulk density and penetration resistance are also used to predict the depth of soil hardpan (Mehari et al., 2005). There are some contradictory results of research work conducted on the effect of conservation tillage on the soil bulk density and penetration resistance. Results of some studies show that conservation tillage methods (no-till and reduced tillage) increase the soil bulk density and penetration resistance compared to the conventional tillage. Liu et al.(2005) reported that zero tillage increased soil bulk density and soil penetration resistance compared to the conventional tillage. Taser and Metinoglu (2005) showed that conservation tillage (reduced and no-till methods) increased the soil bulk density and penetration resistance. Fabrizzi et al. (2005) evaluated the effect of conservation tillage on the soil temperature, compaction, water content, and crop yield and reported that soil had the higher water retention during the critical growth stage of corn in no-till method. Their results also showed that no-till had the higher soil bulk density and penetration resistance, and lower soil temperature and corn yield compared to the minimum tillage method.

There are also some research results showing no significant effect of conservation tillage on the soil bulk density and penetration resistance. Rasouli et al. (2012) studied the

48 effect of conservation tillage on the soil bulk density in saline soils and found that bulk density  
49 was not affected by tillage methods. Afzalnia et al. (2011) showed that conservation tillage  
50 method did not increase soil bulk density compared to the conventional tillage in cotton field.  
51 Logsdon and Karlen (2004) reported that there was no considerable difference between no-till  
52 and conventional (ridge-tillage) methods from the soil bulk density and water content point of  
53 view in deep-loess soils. They also concluded that soil compaction could not be a serious  
54 problem for changing from conventional tillage to the no-till system. Touchton et al. (1984)  
55 reported that the winter legumes made no considerable variations in the soil nitrogen and bulk  
56 density, but increased the water infiltration rate when cotton was no-till planted into winter  
57 legumes compared to the cotton direct seeding in the fallowed soil. Soil bulk density and  
58 penetration resistance are also affected by soil depth. Results of a research work in a Rhodic  
59 Ferrasol in Parana, Brazil, revealed that soil bulk density had the highest value at the soil  
60 depth range of 200 to 300 mm in a no-till system (Cavaliere et al., 2009). According to the  
61 results of a study conducted in Argentina, no-till increased soil resistance compared to the  
62 conventional tillage and soil resistance increment was greater in the shallow layers compared  
63 to the deep layers (Ferrerias et al., 2000). Results of a research performed in Kimberly, Idaho  
64 showed that soil bulk density was 16% to 18% greater in disk and no-till treatments compared  
65 to paratill in the soil depth range of 150 to 200 mm (Aase et al., 2001). Results of this study  
66 also indicated that there was a linear relationship between soil bulk density and soil  
67 penetration resistance. On the other hand, coefficients of friction between soil-soil particles  
68 and soil-steel surface can directly affect soil engaging tools wear and draft. Soil texture and  
69 structure have significant effect on the soil coefficient of friction (Manuwa, 2012). There is a  
70 correlation between angle of soil internal friction and soil bulk density in such a way that  
71 angle of soil internal friction is a quadratic function of soil bulk density (Ngapgue et al.,

72 2012). Tillage methods may affect soil structure which in turn affects soil coefficients of  
73 friction, adhesion, and cohesion; however, no research work regarding the effect of  
74 conservation tillage on the soil coefficients of friction, adhesion, and cohesion was found in  
75 the previous literature. Objective of this study was to determine the effect of conservation  
76 tillage and soil depth on the soil physical and mechanical properties such as bulk density,  
77 penetration resistance, and soil coefficients of friction, adhesion, and cohesion.

## 78 MATERIALS AND METHODS

79 This research was conducted in a farm in Fars province, Iran with the soil  
80 specifications shown in Table 1. The research was performed in the form of a randomized  
81 complete block experimental design with three treatments and six replications for the soil  
82 coefficients of friction. For soil bulk density and soil penetration resistance, a split plot  
83 experiment with the base of randomized complete block design with two factors (tillage  
84 methods and soil depth) and six replications was used. Main plots were tillage methods  
85 including; 1) conventional tillage method (CT); 2) reduced tillage (RT); and 3) zero tillage  
86 (ZT), and subplots were soil depths of 0 to 100, 100 to 200, and 200 to 300 mm. In the  
87 conventional tillage method, primary tillage was performed using a moldboard plow with  
88 working depth of 25 cm, and disk harrow and land leveler were used as the secondary tillage  
89 implements. A tine and disc cultivator which was able to complete the primary and secondary  
90 tillage operations simultaneously, was used to prepare seed bed in the reduced tillage method  
91 (with working depth of 15 cm). BERTINI pneumatic direct planter (Rosario, Santa Fe,  
92 Argentina) was utilized to plant corn seed directly (planting depth of 5 cm) without any seed  
93 bed preparation in the no tillage method. Standing crop residue was kept in the plots for all  
94 tillage treatments. Corn (*Zea mays* L., single cross 704) at the seed rate of 25 kg ha<sup>-1</sup> and the  
95 row space of 750 mm was planted in 20x6 m plots. Sprinkle irrigation system was used to

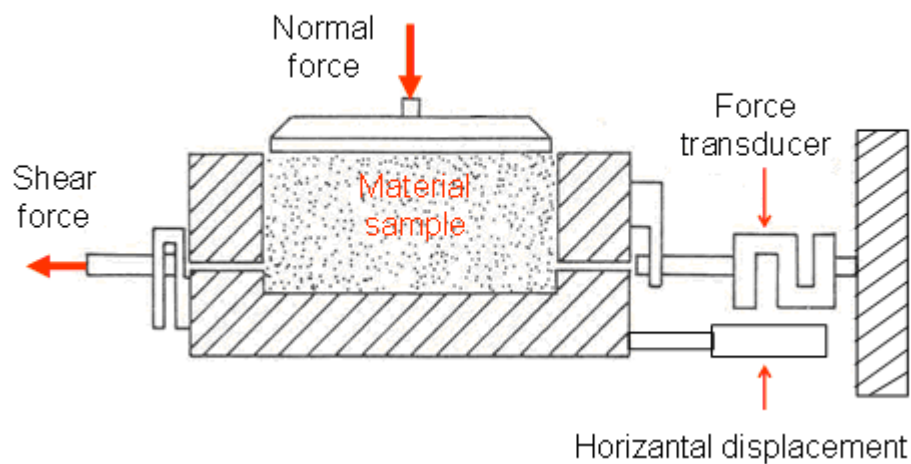
96 irrigate the experimental plots of all treatments. Tillage treatments were applied for two years  
97 (2009-2011) in irrigated corn-wheat rotation. The measurements were carried out in  
98 September 2011 at the end of corn growing season. Soil bulk density, soil penetration  
99 resistance (PR), soil internal coefficient of friction (coefficient of friction between soil  
100 particles), soil external coefficient of friction (coefficient of friction between soil and steel  
101 surface), adhesion coefficient, and cohesion coefficient were measured. Collected data were  
102 analyzed (one way ANOVA) using SAS statistics software and Duncan's multiple range tests  
103 were used to compare the treatments means. Soil bulk density was measured at the soil depths  
104 of 0 to 100, 100 to 200, and 200 to 300 mm using core samplers. Samples were taken from  
105 three different locations of each plot and dried at 105 degrees centigrade for 24 hours.

106 Soil penetration resistance was measured using a cone soil penetrometer (Eijkelkamp  
107 6.15 with cone diameter of 11.28 mm and penetration rate of  $2 \text{ cm s}^{-1}$ ) up to the soil depth of  
108 300 mm with 100 mm depth interval at the moisture content of 23% w.b. (field capacity).  
109 Average of 10 penetrations at each soil depth range was considered as the soil penetration  
110 resistance of each plot. Soil coefficient of internal friction and the coefficient of soil friction  
111 on a polished steel surface were measured in the laboratory using a shear box apparatus (Fig.  
112 1). This apparatus consisted of a sample box (60x60 mm) for holding the soil samples, a force  
113 transducer to record the frictional force, a linkage to apply the normal force to the sample, and  
114 an electrical motor to provide a relative motion for the variable half of the sample box with  
115 respect to its fixed half. Both coefficients were measured at the average soil moisture content  
116 of 18% (wb) and tests were carried out at three levels of normal pressures (100, 200, and 300  
117 kPa). For each test, soil sample was put in the sample box and the bottom half of the sample  
118 box was subjected to a shear force by the electrical motor at a shear rate of  $0.5 \text{ mm min}^{-1}$

119 <sup>1</sup> for each of the aforementioned normal pressures. The frictional forces and horizontal  
 120 displacements were recorded by the shear box during the test running period.

121 **Table 1.** Soil specifications of the experimental area in the farm.

pH	EC	Silt (%)	Clay (%)	Sand (%)	Soil texture
8.4	0.79	54.73	40.94	4.33	Silty clay loam



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123 Fig. 1. Schematic of shear box apparatus.

124 Each test was repeated six times, and a new sample was used for each test. In the case  
 125 of surface friction measurements, the steel surface was cleaned after running each test to  
 126 remove the residue deposited on the surface. The maximum shear stresses were plotted versus  
 127 the normal pressures for each replication. The slope of the best fit line to the plotted data was  
 128 considered as the coefficient of friction of the sample at that replication based on Mohr-  
 129 Coulomb's model. Mohr-Coulomb's model expresses shear stress as a function of normal  
 130 stress, coefficient of friction, and adhesion or cohesion coefficients as follows (Lawton and  
 131 Marchant, 1980):

132 
$$\tau = C_a + \mu\sigma_n, \tag{1}$$

133 where:

134  $\tau$  = effective shear stress (kPa),

135  $C_a$  = adhesion coefficient (kPa),

136  $\mu$  = coefficient of external friction (decimal) and

137  $\sigma_n$  = effective normal stress (kPa).

138 In the coefficient of internal friction measurement, the y-intercept represents the cohesion  
139 coefficient (it is shown by C) and  $\mu$  is the coefficient of internal friction.

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## 141 RESULTS AND DISCUSSION

142 Results showed that tillage method ( $p < 0.05$ ) and soil depth ( $p < 0.01$ ) had a significant  
143 effect on the soil bulk density; while, this parameter was not affected by interaction between  
144 tillage method and soil depth (Table 2). Soil disturbance intensity is different in various tillage  
145 methods; therefore, significant effect of tillage method on the soil bulk density is expected.

146 **Table 2.** Variance analysis of soil bulk density data.

Variation sources	Degree of freedom	Sum squares	Mean squares	F values
Tillage method	2	0.027	0.014	9.08*
Soil depth	2	0.146	0.073	48.51**
Interaction between tillage method and soil depth	4	0.005	0.001	0.86 <sup>ns</sup>
Error	30	0.03	0.002	-

147 <sup>ns</sup>: not significant; \* : significant at  $p < 0.05$ ; \*\* : significant at  $p < 0.01$ .

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149 The maximum soil bulk density was related to the zero tillage method which was  
 150 significantly different from those of the reduced and conventional tillage methods (Table 3).  
 151 The conventional and reduced tillage methods had identical soil bulk density. The higher soil  
 152 bulk density in zero tillage was associated with the lack of soil disturbance in this tillage  
 153 method. Liu et al. (2005), Taser and Metinoglu (2005), Fabrizzi et al. (2005), and Afzalnia et  
 154 al. (2010). also reported the higher soil bulk density in zero tillage compared to the  
 155 conventional tillage method. Soil bulk density increased with increasing soil depth from 0 to  
 156 200 mm and then decreased when the soil depth increased from 200 to 300 mm; therefore, the  
 157 maximum soil bulk density was occurred at the soil depth range of 100 to 200 mm. Reason for  
 158 occurring the maximum soil bulk density at 100 to 200 mm soil depth range was probably  
 159 concentration of the pressure applied to the soil by agricultural machinery traffics at this soil  
 160 depth range. Increasing soil bulk density from the soil surface to a certain depth and its  
 161 decreasing after that depth, has been also reported by Cavalieri et al. (2009).

162 **Table 3.** Average soil bulk density of different tillage methods and soil depths.

Tillage methods	Bulk density (Mg m <sup>-3</sup> )	Soil depth (mm)	Bulk density (Mg m <sup>-3</sup> )
Conventional tillage	1.22 b	0-100	1.24b
Reduced tillage	1.22 b	100-200	1.29 a
Zero tillage	1.26 a	200-300	1.16 c

163 a, b: averages with different letters in each column and group are statistically different at  
 164 p<0.05.

165 Results of penetration resistance data analyses indicated that soil penetration resistance  
 166 was significantly (p<0.01) affected by tillage methods, soil depth, and interaction between  
 167 tillage method and soil depth (Table 4). The reason for the soil penetration resistance being



168 significantly affected by the tillage methods and soil depth was diversity of soil disturbance  
 169 intensity in various tillage methods and soil depths.

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171 **Table 4.** Variance analysis of soil penetration resistance data.

Variation sources	Degree of freedom	Sum squares	Mean squares	F value
Tillage method	2	2.36	1.18	117.33**
Soil depth	2	1.43	0.72	71.11**
Interaction between tillage method and soil depth	4	0.36	0.09	8.85**
Error	30	0.28	0.009	-

172 \*\*: significant at  $p < 0.01$

173 Soil penetration resistance means comparison revealed that the maximum soil  
 174 penetration resistance was occurred in the zero tillage because of the minimum soil  
 175 disturbance in this method and the minimum amount of penetration resistance was related to  
 176 the conventional method due to the maximum soil disturbance in this tillage treatment (Table  
 177 5). The higher soil penetration resistance (higher soil compaction) in the zero tillage method  
 178 can reduce water infiltration and crop root penetration in the soil. Liu et al. (2005), Taser and  
 179 Metinoglu (2005), and Fabrizzi et al. (2005) also reported a higher soil penetration resistance  
 180 for the zero tillage compared to the conventional method. Soil penetration resistance increased  
 181 when the soil depth increased from 0 to 300 mm so that the soil depth range of 200 to 300 mm  
 182 had the highest soil penetration resistance, and the soil depth range of 0 to 100 mm had the  
 183 lowest one (Table 5). Results of means comparison for interaction between tillage methods

184 and soil depth on the soil penetration resistance showed that there was a significant difference  
 185 between tillage methods at all the soil depth ranges tested (Table 6). Conventional tillage  
 186 method at the soil depth range of 0 to 100 mm had the lowest soil penetration resistance and  
 187 zero tillage at the soil depth range of 200 to 300 mm had the highest penetration resistance.  
 188 The difference between cone indices of tillage methods increased with increasing soil depth so  
 189 that the difference was the least at the soil depth range of 0 to 100 mm and was the most at the  
 190 soil depth range of 200 to 300 mm. Although zero tillage method had the maximum amount of  
 191 soil penetration resistance, the penetration resistance obtained from this tillage method was  
 192 lower than the critical soil penetration resistance for agricultural crops (about 2 MPa).

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194 **Table 5.** Average soil penetration resistance of different tillage methods and soil depths.

Tillage methods	Penetration resistance (MPa)	Soil depth (cm)	Penetration resistance (MPa)
Conventional tillage	0.48 c	0-100	0.55 c
Reduced tillage	0.78 b	100-200	0.76 b
Zero tillage	0.99 a	200-300	0.94 a

195 a, b, c: averages with different letters in each column and group are statistically different at  
 196  $p < 0.05$ .

197 **Table 6.** Soil penetration resistance affected by interaction between tillage methods and soil  
 198 depths.

Tillage method	Soil depth (mm)	Penetration resistance (MPa)
Conventional tillage	0-100	0.40 e
Conventional tillage	100-200	0.46 e

Conventional tillage	200-300	0.57 d
Reduced tillage	0-100	0.46 e
Reduced tillage	100-200	0.78 c
Reduced tillage	200-300	1.10 ab
Zero tillage	0-100	0.77 c
Zero tillage	100-200	1.02 b
Zero tillage	200-300	1.16 a

199 a, b: averages with different letters in each column and group are statistically different at  
200  $p < 0.05$ .

201 Data analysis of coefficients of soil internal friction, external friction, cohesion, and  
202 adhesion indicated that coefficient of soil internal friction and adhesion coefficient were  
203 significantly affected ( $p < 0.05$ ) by tillage methods; while, the effect of tillage treatments on the  
204 coefficient of soil external friction and cohesion coefficient was not statistically significant  
205 (Table 7).

206 **Table 7.** Data variance analysis of coefficients of soil internal friction, external friction,  
207 cohesion, and adhesion. Data shown in this table are F values.

Variation sources	Internal friction	External friction	Cohesion	Adhesion
Replication	0.85 <sup>ns</sup>	0.68 <sup>ns</sup>	1.59 <sup>ns</sup>	6.84 <sup>*</sup>
Tillage method	3.23 <sup>*</sup>	0.14 <sup>ns</sup>	1.85 <sup>ns</sup>	3.45 <sup>*</sup>

208 <sup>ns</sup>: not significant

209 <sup>\*</sup>: significant at  $p < 0.05$

210 Coefficients of soil internal friction and cohesion in different tillage methods are  
211 shown in Table 8. Conventional tillage method had the highest coefficient of internal friction;

212 whereas, the lowest coefficient of internal friction was obtained from the zero tillage.  
 213 Reduction of soil coefficient of internal friction in the conservation tillage methods was  
 214 probably because of improving soil structure in conservation tillage system. Since soil specific  
 215 resistance is significantly influenced by the soil coefficient of internal friction, conservation  
 216 tillage method can reduce soil specific resistance by reducing the coefficient of internal  
 217 friction. The maximum cohesion coefficient was related to the zero tillage method which was  
 218 statistically different from those of the conventional and reduced tillage treatments. The  
 219 minimum cohesion coefficient was obtained from the reduced tillage method (Table 8).

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221 **Table 8.** Average coefficients of soil internal friction and cohesion in different tillage  
 222 methods.

Tillage methods	Coefficient of internal friction	Cohesion coefficient (kPa)
Conventional tillage	0.44 a	13.2 b
Reduced tillage	0.45 a	10.5 b
Zero tillage	0.35 b	21.0 a

223 a, b, c: averages with different letters in each column and group are statistically different at  
 224  $p < 0.05$ .

225 There was not a significant difference between tillage treatments for coefficient of soil  
 226 external friction (Table 9); however, this coefficient had slightly higher amount in the zero  
 227 tillage method compared to the conventional and reduced tillage treatments. Results of this  
 228 study also showed that the difference between the tillage methods for adhesion coefficient was  
 229 significant in such a way that the largest amount of soil adhesion coefficient was obtained  
 230 from the zero tillage and the smallest one was related to the reduced tillage method.

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233 **Table 9.** Average coefficients of soil external friction and adhesion in different tillage  
234 methods.

Tillage methods	Coefficient of external friction	Adhesion coefficient (kPa)
Conventional tillage	0.27 a	15.5 b
Reduced tillage	0.30 a	9.6 c
Zero tillage	0.27 a	18.1 a

235 a, b, c: averages with different letters in each column and group are statistically different at  
236  $p < 0.05$ .

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### CONCLUSIONS

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Results of this study indicated that soil bulk density and penetration resistance were significantly affected by tillage methods and soil depth. Zero tillage method had the maximum soil bulk density and penetration resistance, and conventional tillage treatment had the minimum soil bulk density and penetration resistance. Penetration resistance increased with increasing soil depth from 0 to 300 mm; whereas, bulk density increased when soil depth increased from 0 to 200 mm and then decreased with increasing soil depth from 200 to 300 mm. Results also showed that tillage method had a significant effect on the coefficient of soil internal friction and adhesion coefficient; while, the coefficient of soil external friction and cohesion coefficient were not significantly affected by the tillage treatments. The zero tillage method reduces the coefficient of soil internal friction which may in turn reduce the soil specific resistance and power required to cut the soil.

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### RECOMMENDATION FOR FUTURE WORK

250 According to results and limitations of this study, the following recommendation can be  
251 given to make the future studies more effective in this area: Since the coefficients of soil  
252 friction were measured at one level of moisture content in the present study, the interactive  
253 effect of soil moisture content and tillage methods on the coefficients of soil internal and  
254 external friction, adhesion, and cohesion may be evaluated in the future research.

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