

EFFECT OF CONSERVATION TILLAGE ON THE SOIL PHYSICAL AND MECHANICAL PROPERTIES

ABSTRACT

Effect of different tillage methods on soil physical and mechanical properties was evaluated in this research. A split plot experimental design with nine treatments and six replications was used for soil bulk density and penetration resistance. Main plots were tillage methods including conventional tillage, reduced tillage, and zero tillage. Soil depth ranges of 0 to 100, 100 to 200, and 200 to 300 mm were considered as sub plots. Soil bulk density, soil penetration resistance, coefficients of soil internal and external friction, adhesion, and cohesion were measured. Collected data were analyzed (one way ANOVA) using SAS statistics software and Duncan's multiple range tests were used to compare the treatments means. Results showed that tillage methods had a significant effect on the soil bulk density so that the conventional and reduced tillage methods had the lowest soil bulk density, and zero tillage method had the highest one. Soil bulk density was also affected by soil depth in such a way that bulk density increased when soil depth increased from 0 to 200 mm, and then decreased by increasing soil depth from 200 to 300 mm. The maximum soil penetration resistance was obtained from the zero tillage; while, the conventional tillage had the minimum soil penetration resistance. Soil penetration resistance increased with increasing soil depth from 0 to 300 mm. Results also indicated that zero tillage significantly decreased the coefficient of soil internal friction; whereas, the coefficient of soil external friction was not affected by tillage methods.

Keywords: Bulk density; friction coefficient; penetration resistance; tillage methods

24

INTRODUCTION

25

26

27

28

29

30

31

32

33

34

35

36

37

38

39

40

41

42

43

44

45

46

47

Conventional tillage system is being replaced in the world by the conservation tillage method in which at least 30% of soil surface remains covered by crop residues. Transition from the conventional tillage method to the conservation system may affect the soil physical and mechanical properties such as soil bulk density, soil penetration resistance, and soil internal and external coefficients of friction. Soil bulk density and penetration resistance are used as indices of soil compaction so that by increasing these two indices, soil compaction increases and increasing soil compaction may prevent water and crop root penetration in the soil. Soil bulk density and penetration resistance are also used to predict the depth of soil hardpan (Mehari et al., 2005). There are some contradictory results of research work conducted on the effect of conservation tillage on the soil bulk density and penetration resistance. Results of some studies show that conservation tillage methods (no-till and reduced tillage) increase the soil bulk density and penetration resistance compared to the conventional tillage. Liu et al. (2005) reported that zero tillage increased soil bulk density and soil penetration resistance compared to the conventional tillage. Taser and Metinoglu (2005) showed that conservation tillage (reduced and no-till methods) increased the soil bulk density and penetration resistance. Fabrizzi et al. (2005) evaluated the effect of conservation tillage on the soil temperature, compaction, water content, and crop yield and reported that soil had the higher water retention during the critical growth stage of corn in no-till method. Their results also showed that no-till had the higher soil bulk density and penetration resistance, and lower soil temperature and corn yield compared to the minimum tillage method.

There are also some research results showing no significant effect of conservation tillage on the soil bulk density and penetration resistance. Rasouli et al. (2012) studied the effect of conservation tillage on the soil bulk density in saline soils and found that bulk density

48 was not affected by tillage methods. Afzalnia et al. (2011) showed that conservation tillage
49 method did not increase soil bulk density compared to the conventional tillage in cotton field.
50 Logsdon and Karlen (2004) reported that there was no considerable difference between no-till
51 and conventional (ridge-tillage) methods from the soil bulk density and water content point of
52 view in deep-loess soils. They also concluded that soil compaction could not be a serious
53 problem for changing from conventional tillage to the no-till system. Touchton et al. (1984)
54 reported that the winter legumes made no considerable variations in the soil nitrogen and bulk
55 density, but increased the water infiltration rate when cotton was no-till planted into winter
56 legumes compared to the cotton direct seeding in the fallowed soil. Soil bulk density and
57 penetration resistance are also affected by soil depth. Results of a research work in a Rhodic
58 Ferrasol in Parana, Brazil, revealed that soil bulk density had the highest value at the soil
59 depth range of 200 to 300 mm in a no-till system (Cavalieri et al., 2009). According to the
60 results of a study conducted in Argentina, no-till increased soil resistance compared to the
61 conventional tillage and soil resistance increment was greater in the shallow layers compared
62 to the deep layers (Ferrerias et al., 2000). Results of a research performed in Kimberly, Idaho
63 showed that soil bulk density was 16% to 18% greater in disk and no-till treatments compared
64 to paratill in the soil depth range of 150 to 200 mm (Aase et al., 2001). Results of this study
65 also indicated that there was a linear relationship between soil bulk density and soil
66 penetration resistance. On the other hand, coefficients of friction between soil-soil particles
67 and soil-steel surface can directly affect soil engaging tools wear and draft. Soil texture and
68 structure have significant effect on the soil coefficient of friction (Manuwa, 2012). There is a
69 correlation between angle of soil internal friction and soil bulk density in such a way that
70 angle of soil internal friction is a quadratic function of soil bulk density (Ngapgue et al.,
71 2012). Tillage methods may affect soil structure which in turn affects soil coefficients of

72 friction, adhesion, and cohesion; however, no research work regarding the effect of
73 conservation tillage on the soil coefficients of friction, adhesion, and cohesion was found in
74 the previous literature. Objective of this study was to determine the effect of conservation
75 tillage and soil depth on the soil physical and mechanical properties such as bulk density,
76 penetration resistance, and soil coefficients of friction, adhesion, and cohesion.

77 **MATERIALS AND METHODS**

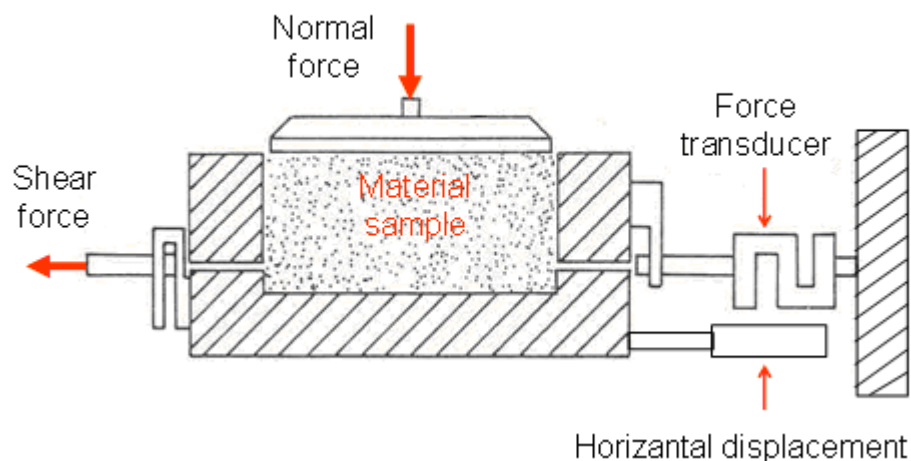
78 This research was conducted in a farm in Fars province, Iran with the soil
79 specifications shown in Table 1. The research was performed in the form of a randomized
80 complete block experimental design with three treatments and six replications for the soil
81 coefficients of friction. For soil bulk density and soil penetration resistance, a split plot
82 experiment with the base of randomized complete block design with two factors (tillage
83 methods and soil depth) and six replications was used. Main plots were tillage methods
84 including; 1) conventional tillage method (CT); 2) reduced tillage (RT); and 3) zero tillage
85 (ZT), and subplots were soil depths of 0 to 100, 100 to 200, and 200 to 300 mm. In the
86 conventional tillage method, primary tillage was performed using a moldboard plow with
87 working depth of 25 cm, and disk harrow and land leveler were used as the secondary tillage
88 implements. A tine and disc cultivator which was able to complete the primary and secondary
89 tillage operations simultaneously, was used to prepare seed bed in the reduced tillage method
90 (with working depth of 15 cm). BERTINI pneumatic direct planter (Rosario, Santa Fe,
91 Argentina) was utilized to plant corn seed directly (planting depth of 5 cm) without any seed
92 bed preparation in the no tillage method. Standing crop residue was kept in the plots for all
93 tillage treatments. Corn (*Zea mays* L., single cross 704) at the seed rate of 25 kg ha⁻¹ and the
94 row space of 750 mm was planted in 20x6 m plots. Sprinkle irrigation system was used to
95 irrigate the experimental plots of all treatments. Tillage treatments were applied for two years

96 (2009-2011) in irrigated corn-wheat rotation. The measurements were carried out in
97 September 2011 at the end of corn growing season. Soil bulk density, soil penetration
98 resistance (PR), soil internal coefficient of friction (coefficient of friction between soil
99 particles), soil external coefficient of friction (coefficient of friction between soil and steel
100 surface), adhesion coefficient, and cohesion coefficient were measured. Collected data were
101 analyzed (one way ANOVA) using SAS statistics software and Duncan's multiple range tests
102 were used to compare the treatments means. Soil bulk density was measured at the soil depths
103 of 0 to 100, 100 to 200, and 200 to 300 mm using core samplers. Samples were taken from
104 three different locations of each plot and dried at 105 degrees centigrade for 24 hours.

105 Soil penetration resistance was measured using a cone soil penetrometer (Eijkelkamp
106 6.15 with cone diameter of 11.28 mm and penetration rate of 2 cm s^{-1}) up to the soil depth of
107 300 mm with 100 mm depth interval at the moisture content of 23% w.b. (field capacity).
108 Average of 10 penetrations at each soil depth range was considered as the soil penetration
109 resistance of each plot. Soil coefficient of internal friction and the coefficient of soil friction
110 on a polished steel surface were measured in the laboratory using a shear box apparatus (Fig.
111 1). This apparatus consisted of a sample box (60x60 mm) for holding the soil samples, a force
112 transducer to record the frictional force, a linkage to apply the normal force to the sample, and
113 an electrical motor to provide a relative motion for the variable half of the sample box with
114 respect to its fixed half. Both coefficients were measured at the average soil moisture content
115 of 18% (wb) and tests were carried out at three levels of normal pressures (100, 200, and 300
116 kPa). For each test, soil sample was put in the sample box and the bottom half of the sample
117 box was subjected to a shear force by the electrical motor at a shear rate of 0.5 mm min^{-1}
118 for each of the aforementioned normal pressures. The frictional forces and horizontal
119 displacements were recorded by the shear box during the test running period.

120 **Table 1.** Soil specifications of the experimental area in the farm.

pH(unit?)	EC (unit?)	Silt (%)	Clay (%)	Sand (%)	Soil texture
8.4	0.79	54.73	40.94	4.33	Silty clay loam



121

122

Fig. 1. Schematic of shear box apparatus.

123

124

125

126

127

128

129

130

131

$$\tau = C_a + \mu\sigma_n, \tag{1}$$

132 where:

133

τ = effective shear stress (kPa),

- 134 C_a = adhesion coefficient (kPa),
 135 μ = coefficient of external friction (decimal) and
 136 σ_n = effective normal stress (kPa).

137 In the coefficient of internal friction measurement, the y-intercept represents the cohesion
 138 coefficient (it is shown by C) and μ is the coefficient of internal friction.

139

140 RESULTS AND DISCUSSION

141 Results showed that tillage method ($p < 0.05$) and soil depth ($p < 0.01$) had a significant
 142 effect on the soil bulk density; while, this parameter was not affected by interaction between
 143 tillage method and soil depth (Table 2). Soil disturbance intensity is different in various tillage
 144 methods; therefore, significant effect of tillage method on the soil bulk density is expected.

145 **Table 2.** Variance analysis of soil bulk density data.

Variation sources	Degree of freedom	Sum squares	Mean squares	F values
Tillage method	2	0.027	0.014	9.08*
Soil depth	2	0.146	0.073	48.51**
Interaction between tillage method and soil depth	4	0.005	0.001	0.86 ^{ns}
Error	30	0.03	0.002	-

146 ^{ns}: not significant; * : significant at $p < 0.05$; ** : significant at $p < 0.01$.

147

148 The maximum soil bulk density was related to the zero tillage method which was
 149 significantly different from those of the reduced and conventional tillage methods (Table 3).

150 The conventional and reduced tillage methods had identical soil bulk density. The higher soil

151 bulk density in zero tillage was associated with the lack of soil disturbance in this tillage
 152 method. Liu et al. (2005), Taser and Metinoglu (2005), Fabrizzi et al. (2005), and Afzalinia et
 153 al. (2010) also reported the higher soil bulk density in zero tillage compared to the
 154 conventional tillage method. Soil bulk density increased with increasing soil depth from 0 to
 155 200 mm and then decreased when the soil depth increased from 200 to 300 mm; therefore, the
 156 maximum soil bulk density was occurred at the soil depth range of 100 to 200 mm. Reason for
 157 occurring the maximum soil bulk density at 100 to 200 mm soil depth range was probably
 158 concentration of the pressure applied to the soil by agricultural machinery traffics at this soil
 159 depth range. Increasing soil bulk density from the soil surface to a certain depth and its
 160 decreasing after that depth, has been also reported by Cavalieri et al. (2009).

161 **Table 3.** Average soil bulk density of different tillage methods and soil depths.

Tillage methods	Bulk density (Mg m ⁻³)	Soil depth (mm)	Bulk density (Mg m ⁻³)
Conventional tillage	1.22 b	0-100	1.24b
Reduced tillage	1.22 b	100-200	1.29 a
Zero tillage	1.26 a	200-300	1.16 c

162 a, b: averages with different letters in each column and group are statistically different at
 163 p<0.05.

164 Results of penetration resistance data analyses indicated that soil penetration resistance
 165 was significantly (p<0.01) affected by tillage methods, soil depth, and interaction between
 166 tillage method and soil depth (Table 4). The reason for the soil penetration resistance being
 167 significantly affected by the tillage methods and soil depth was diversity of soil disturbance
 168 intensity in various tillage methods and soil depths.

169

170 **Table 4.** Variance analysis of soil penetration resistance data.

Variation sources	Degree of freedom	Sum squares	Mean squares	F value
Tillage method	2	2.36	1.18	117.33 ^{**}
Soil depth	2	1.43	0.72	71.11 ^{**}
Interaction between tillage method and soil depth	4	0.36	0.09	8.85 ^{**}
Error	30	0.28	0.009	-

171 ^{**}: significant at $p < 0.01$

172 Soil penetration resistance means comparison revealed that the maximum soil
173 penetration resistance was occurred in the zero tillage because of the minimum soil
174 disturbance in this method and the minimum amount of penetration resistance was related to
175 the conventional method due to the maximum soil disturbance in this tillage treatment (Table
176 5). The higher soil penetration resistance (higher soil compaction) in the zero tillage method
177 can reduce water infiltration and crop root penetration in the soil. Liu et al. (2005), Taser and
178 Metinoglu (2005), and Fabrizzi et al. (2005) also reported a higher soil penetration resistance
179 for the zero tillage compared to the conventional method. Soil penetration resistance increased
180 when the soil depth increased from 0 to 300 mm so that the soil depth range of 200 to 300 mm
181 had the highest soil penetration resistance, and the soil depth range of 0 to 100 mm had the
182 lowest one (Table 5). Results of means comparison for interaction between tillage methods
183 and soil depth on the soil penetration resistance showed that there was a significant difference
184 between tillage methods at all the soil depth ranges tested (Table 6). Conventional tillage
185 method at the soil depth range of 0 to 100 mm had the lowest soil penetration resistance and

186 zero tillage at the soil depth range of 200 to 300 mm had the highest penetration resistance.
 187 The difference between cone indices of tillage methods increased with increasing soil depth so
 188 that the difference was the least at the soil depth range of 0 to 100 mm and was the most at the
 189 soil depth range of 200 to 300 mm. Although zero tillage method had the maximum amount of
 190 soil penetration resistance, the penetration resistance obtained from this tillage method was
 191 lower than the critical soil penetration resistance for agricultural crops (about 2 MPa).

192

193 **Table 5.** Average soil penetration resistance of different tillage methods and soil depths.

Tillage methods	Penetration resistance (MPa)	Soil depth (cm)	Penetration resistance (MPa)
Conventional tillage	0.48 c	0-100	0.55 c
Reduced tillage	0.78 b	100-200	0.76 b
Zero tillage	0.99 a	200-300	0.94 a

194 a, b, c: averages with different letters in each column and group are statistically different at
 195 $p < 0.05$.

196 **Table 6.** Soil penetration resistance affected by interaction between tillage methods and soil
 197 depths.

Tillage method	Soil depth (mm)	Penetration resistance (MPa)
Conventional tillage	0-100	0.40 e
Conventional tillage	100-200	0.46 e
Conventional tillage	200-300	0.57 d
Reduced tillage	0-100	0.46 e
Reduced tillage	100-200	0.78 c

Reduced tillage	200-300	1.10 ab
Zero tillage	0-100	0.77 c
Zero tillage	100-200	1.02 b
Zero tillage	200-300	1.16 a

198 a, b: averages with different letters in each column and group are statistically different at
 199 $p < 0.05$.

200 Data analysis of coefficients of soil internal friction, external friction, cohesion, and
 201 adhesion indicated that coefficient of soil internal friction and adhesion coefficient were
 202 significantly affected ($p < 0.05$) by tillage methods; while, the effect of tillage treatments on the
 203 coefficient of soil external friction and cohesion coefficient was not statistically significant
 204 (Table 7).

205 **Table 7.** Data variance analysis of coefficients of soil internal friction, external friction,
 206 cohesion, and adhesion. Data shown in this table are F values.

Variation sources	Internal friction	External friction	Cohesion	Adhesion
Replication	0.85 ^{ns}	0.68 ^{ns}	1.59 ^{ns}	6.84 [*]
Tillage method	3.23 [*]	0.14 ^{ns}	1.85 ^{ns}	3.45 [*]

207 ^{ns}: not significant

208 ^{*}: significant at $p < 0.05$

209 Coefficients of soil internal friction and cohesion in different tillage methods are
 210 shown in Table 8. Conventional tillage method had the highest coefficient of internal friction;
 211 whereas, the lowest coefficient of internal friction was obtained from the zero tillage.
 212 Reduction of soil coefficient of internal friction in the conservation tillage methods was
 213 probably because of improving soil structure in conservation tillage system. Since soil specific

214 resistance is significantly influenced by the soil coefficient of internal friction, conservation
 215 tillage method can reduce soil specific resistance by reducing the coefficient of internal
 216 friction. The maximum cohesion coefficient was related to the zero tillage method which was
 217 statistically different from those of the conventional and reduced tillage treatments. The
 218 minimum cohesion coefficient was obtained from the reduced tillage method (Table 8).

219

220 **Table 8.** Average coefficients of soil internal friction and cohesion in different tillage
 221 methods.

Tillage methods	Coefficient of internal friction	Cohesion coefficient (kPa)
Conventional tillage	0.44 a	13.2 b
Reduced tillage	0.45 a	10.5 b
Zero tillage	0.35 b	21.0 a

222 a, b, c: averages with different letters in each column and group are statistically different at
 223 $p < 0.05$.

224 There was not a significant difference between tillage treatments for coefficient of soil
 225 external friction (Table 9); however, this coefficient had slightly higher amount in the zero
 226 tillage method compared to the conventional and reduced tillage treatments. Results of this
 227 study also showed that the difference between the tillage methods for adhesion coefficient was
 228 significant in such a way that the largest amount of soil adhesion coefficient was obtained
 229 from the zero tillage and the smallest one was related to the reduced tillage method.

230

231

232 **Table 9.** Average coefficients of soil external friction and adhesion in different tillage
233 methods.

Tillage methods	Coefficient of external friction	Adhesion coefficient (kPa)
Conventional tillage	0.27 a	15.5 b
Reduced tillage	0.30 a	9.6 c
Zero tillage	0.27 a	18.1 a

234 a, b, c: averages with different letters in each column and group are statistically different at
235 $p < 0.05$.

236

CONCLUSIONS

237 Results of this study indicated that soil bulk density and penetration resistance were
238 significantly affected by tillage methods and soil depth. Zero tillage method had the maximum
239 soil bulk density and penetration resistance, and conventional tillage treatment had the
240 minimum soil bulk density and penetration resistance. Penetration resistance increased with
241 increasing soil depth from 0 to 300 mm; whereas, bulk density increased when soil depth
242 increased from 0 to 200 mm and then decreased with increasing soil depth from 200 to 300
243 mm. Results also showed that tillage method had a significant effect on the coefficient of soil
244 internal friction and adhesion coefficient; while, the coefficient of soil external friction and
245 cohesion coefficient were not significantly affected by the tillage treatments. The zero tillage
246 method reduces the coefficient of soil internal friction which may in turn reduce the soil
247 specific resistance and power required to cut the soil.

248

RECOMMENDATION FOR FUTURE WORK

249 According to results and limitations of this study, the following recommendation can be
250 given to make the future studies more effective in this area:

251 Since the coefficients of soil friction were measured at one level of moisture content in the
252 present study, the interactive effect of soil moisture content and tillage methods on the
253 coefficients of soil internal and external friction, adhesion, and cohesion may be evaluated in
254 the future research.

255 REFERENCES

- 256 1. Aase JK, Bjerneberg DL, Sojka RE. 2001 Zone-Subsoiling Relationships to Bulk
257 Density and Cone index on a Furrow-Irrigated Soil. *Trans. ASAE*, 44, 577-583.
- 258 2. Afzalinia S, Karami A, Alavimanesh SM. 2012. Comparing Conservation and
259 Conventional Tillage Methods in Corn-Wheat Rotation. Paper presented at the
260 International Conference of Agricultural Engineering, Valencia, Spain, 8-12 July
261 2012.
- 262 3. Afzalinia S, Behaen MA, Karami A, Dezfuli A, Ghasari A. 2011. Effect of
263 Conservation Tillage on the Soil Properties and Cotton Yield. Paper presented at the
264 11th International Congress on Mechanization and Energy in Agriculture, Istanbul,
265 Turkey, 21-23 September 2011.
- 266 4. Fabrizzi KP, Garc´ FO, Costa JL, Picone LI. 2005. Soil Water Dynamics,
267 Physical Properties and Corn and Wheat Responses to Minimum and No-tillage
268 Systems in the Southern Pampas of Argentina. *Soil Tillage Res.*, 81, 57-69.
- 269 5. Ferreras LA, Costa JL, Garcia FO, Pecorari C. 2000. Effect of No-Tillage on Some
270 Soil Physical Properties of a Structural Degraded Petrocalcic Paleudol of the Southern
271 "Pampa" of Argentina. *Soil Tillage Res.*, 54, 31-39.
- 272 6. Cavalieri KMV, Silva APD, Tormena CA, Leao TP, Dexter AR, Hakansson I. 2009.
273 Long-Term Effects of No-Tillage on Dynamic Soil Physical Properties in a Rhodic
274 Ferrasol in Parana, Brazil. *Soil Tillage Res.*, 103, 158-164.

- 275 7. Lawton PJ, Marchant JA. 1980. Direct Shear Testing of Seeds in Bulk. *Journal of*
276 *Agricultural Engineering Research*, 25, 189-201.
- 277 8. Liu S, Zhang H, Dai Q, Huo H, Xu ZK, Ruan H. 2005. Effects of No-Tillage Plus
278 Inter-Planting and Remaining Straw on the Field on Cropland Eco-environment and
279 Wheat Growth. *Ying Yong Sheng Tai Xue Bao*, 16(2), 393-396.
- 280 9. Logsdon SD, Karlen DL. 2004. Bulk Density as a Soil Quality Indicator during
281 Conversion to No-tillage. *Soil Tillage Res.*, 78, 143–149.
- 282 10. Manuwa SI. 2012. Effect of Moisture Content on Rubber, Steel and
283 Tetrafluoroethylene Materials Sliding on Textured Soils. *Modern Applied Science*, 6,
284 117-121.
- 285 11. Mehari, A, Schultz B, Depeweg H. 2005. Where Indigenous Water Management
286 Practices Overcome Failures of Structures: the Wadi Laba Spate Irrigation System in
287 Eritrea. *Irrigation and Drainage*, 54, 1–14.
- 288 12. Ngagoue F, Madjadoumbaye J, Nouanga P, Amadou T, Tamo TT. 2012. Modeling of
289 Frictional and Cohesive Resistances of Bafoussam (Cameroon) Soils. *EJGE*, 17, 463-
290 472.
- 291 13. Rasouli F, Kiani Pouya A, Afzalinia S. 2012. Effect of Conservation Tillage Methods
292 on Soil Salinity. Paper presented at the 8th International Soil Science Congress, Izmir,
293 Turkey, 15-17 May 2012.
- 294 14. Taser O, Metinoglu F. 2005. Physical and Mechanical Properties of a Clay Soil as
295 Affected by Tillage Systems for Wheat Growth. *Acta Agriculturae Scandinavica*
296 *Section B-soil and Plant*, 55, 186-191.
- 297 15. Touchton JT, Rickerl DH, Walker RH, Snipes CE. 1984. Winter Legumes as a
298 Nitrogen Source for No-tillage Cotton. *Soil Tillage Res.*, 4(4), 391-401.