

Original Research Article

Wave Energy Impact on Benin's Coastline Dynamics, Gulf of Guinea

Abstract

Most of the shorelines around the world are affected by the phenomenon of coastal erosion, especially the Benin's coastline.

We investigated the parameters (significant height, peak period and peak direction) and wave energy potential offshore Benin from ECMWF ERA reanalysis. We adjusted these ERAI data with in situ data coming from the buoy installed off Autonomous Port of Cotonou (Benin) over a period of 14 years. Next, we used statistical analysis to establish the link between wave energy and Benin coast dynamics. Wave energy assessment has been carried using the empirical formula for medium water depths consideration (equation (10)).

The results show that in Benin's coastal area, wave energy potential is moderate and available ($H_s \approx 1.36\text{m}$, $T_p \approx 9.6$ and $P \approx 15.56\text{kW/m}$). At seasonal scale, wave energy density P and coastline displacement are strongly linked ($\sigma^2 = 0.9$).

Wave energy exploitation will contribute to energy self-sufficiency and will play an important role in the coastal protection of the country.

Keywords: Coastal erosion; Benin coastline; Wave energy; Coastal protection.

1. INTRODUCTION

More than 70% of beaches are eroding [1], and beach erosion is a global problem [2]. Intensification of urban development results from expanding coastal use by human populations [3], and almost every beach on every coastline is threatened by human activities [4]. Benin, a coastal country in Gulf of Guinea, has not been spared by the phenomenon of coastal erosion. Erosion observed on Benin's coastline is accentuated by the human installations: port with dykes blocking the coastal drift, urbanization

with fixing of the dune cord, construction of dams upstream of the rivers, thus reducing sediment inputs. Indeed, the sedimentary equilibrium of this coastline is precarious, it depends on the dynamics of coastal drift, one of the largest in the world ($\approx 500\,000\text{ m}^3/\text{year}$, [5], which is put into motion by swells generated in the South Atlantic. As a result, the coastline is experiencing a very significant decline, ranging from 2 to more than 30m per year from Côte d'Ivoire to Nigeria [6-9]. The geographical location of the country, offers the possibility of exploiting wave energy, which could contribute to the mitigation of coastal erosion observed. Indeed, there are currently, several wave energy recovery devices that play an active role in coastal protection. These recovery devices are particularly interesting since they partially absorb waves in producing electricity and may thus reduce the wave energy incident on the littoral [10]. Recent studies [10-13] showed that nearshore currents, which are the main factor in driving the coastline dynamics, are sometimes even more sensitive than the waves to the nearshore energy extraction. This is explained by the fact that the wave farms induce relevant changes; not only to the wave heights, but also to the wave directions [14]. Wave energy in Benin coastal area, if available, will contribute to the country's energy dependence. Although very crucial, the characteristics (minimum, average, maximum, inter-annual and seasonal variability) of the wave energy resource in Benin's coastal zone are poorly known.

In this paper, wave energy has been characterized and analyzed using European Center for Medium-Range Weather Forecasts (ECMWF) reanalysis (ERA-Interim) datasets adjusted with in situ data coming from the buoy installed off Autonomous Port of Cotonou (Benin) over a period of 14 years. Next, the link between wave energy and Benin coastline dynamics has been investigated using statistical analysis.

42

43 **2. MATERIALS AND METHODS**

44 **2.1. Study area**

45 Benin's coastline, 125 km long, is located between the longitudes $E1^\circ5'$ and $2^\circ5'E$ and
 46 the latitudes $5^\circ N$ and $6^\circ N$ and facing South Atlantic Ocean (Fig. 1.a). It is an open
 47 environment exposed to long swell waves. It is an environment dominated by the in-
 48 fluence of waves of moderate energy (mean significant wave height $H_s = 1.36\text{ m}$,

mean peak period $T_p = 9.4$ s) coming from mid-to high latitudes ($45-60^\circ$) in the South Atlantic as well as to locally generated short-waves in the tropical band (6°N to 15°S) with an S-SW incidence (incidence on the coast between 4 and 10°), [5,15]

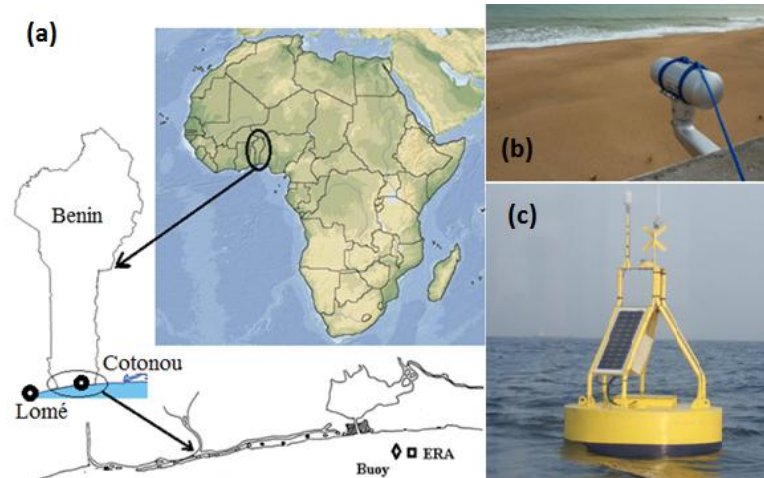


Fig.1. Sketch of study area (Benin, Gulf of Guinea). Location of ERA and Buoy ;
a.) Oceanographic buoy.

2.2. Data sets

2.2.1. Buoy data

Wave parameter data from the buoy deployed offshore about 6Km from the Autonomous port of Cotonou and more than 15m deep at the coordinates ($6^\circ 18' 49\text{N}$, $2^\circ 28' 46\text{E}$) are used (Fig. 1.c). Waves parameters significant wave height (H_s), peak period (T_p) and peak direction (D_p) are recorded every 30 min (48 daily data). The buoy data used here cover the period from december 2015 to october 2016.

2.2.2. ERAI reanalysis

The simulations used were provided by ERA-Interim ($1.5^\circ \times 1.5^\circ$) of the European Center for Medium-Range Weather Forecasting (ECMWF). ERA datasets has always been used and validated in the Gulf of Guinea [5,15]. Wave parameters used are (H_s , T_p and D_p). These parameters are stored four times a day (temporal resolution: 6h). The outputs used are calculated at the point ($6^\circ 0' \text{N}$; $3^\circ 0' \text{E}$). ERAI datasets cover the period 2003-2016.

78 2.2.3. The camera system

79 In February 2013, a low-cost video system was installed on the top of a tower of the
80 Navy Forces of Benin in Grand Popo, about 70 m from the shoreline [16]. The system
81 was composed of a VIVOTEK IP 7361 camera (1600-728 pixels), which collected
82 data continuously at 2 Hz (Fig.1.b). Twenty ground control points were taken with
83 GPS to process image geo-rectification [17], by applying the method of direct linear
84 transformation [18]. See [16,19-21] for more description. Data used here are about,
85 the shoreline position.

86 2.3. Data validation

87 A comparison between the ERA model outputs and the buoy data indicates an over-
88 estimation of the extremes at the reanalysis with respect to the buoy data. Although
89 the mean values are well described, it thus appears that the model reproduces the large
90 swells ($H_s > 1\text{m}$) but misses the small ones ($H_s < 1\text{m}$). The correlation between the buoy
91 data and the model outputs ($R^2 = 0.80$ for H_s , $R^2 = 0.49$ for T_p) made it possible to
92 consider an adjustment between the significant heights H_s , peak period T_p observed
93 (buoy) and estimated (ERA). The linear adjustment is written by:

$$94 \begin{cases} H_{sb} = 1.03 * H_{sm} - 0.10 \\ T_{pb} = 0.55 * T_{pm} + 0.45 \end{cases} \quad (1)$$

95 where H_{sb} , T_{pb} represents respectively the significant height and the peak period of
96 the waves measured by the buoy and H_{sm} , T_{pm} derived from ERAI. This adjustment is
97 used for the characterization of wave parameters and consequently average energy
98 density in Benin coastline area.

99 2.4. THEORY

100 2.4.1. Wave energy density estimation

101 Recently, Wave power density is the most important analytical model, which has been
102 typically uses to calculate wave energy resources by integrating model spectra, based
103 on numerical wave models [22]. In shallow or medium water depths, the nearshore
104 effects must be considered when calculating the wave power density, including refrac-
105 tion, shoaling, bottom dissipation and sheltering by the coastline or adjacent islands

[23]. Hence, in shallow water, the wave power can be obtained using the following expression [24]:

$$P = \frac{1}{T} \int_0^T \int_{-h}^0 (p + \rho g z) u dt dz \quad (2)$$

where t : the time (s); T : wave period (s) and z : water depth (m).

The integral of Eq. (2) over the wave period and the water depth conducted to P . Therefore, P can be calculated using [25]:

$$P = \bar{E} C_g \quad (3)$$

Where C_g denotes wave group velocity and $\bar{E}$ (J/m^2), the wave energy density which ones can respectively be express as follows;

$$C_g = \frac{1}{2} \left[1 + \frac{2kh}{\sinh(2kh)} \right] * C \quad (4)$$

$$\bar{E} = \frac{1}{16} \rho g H_s^2 \quad (5)$$

The wave number k (m^{-1}) as a function of λ (wavelength) (m) is giving by:

$$k = \frac{2\pi}{\lambda} \quad (6)$$

The phase velocity C can be expressed as follows;

$$C = \frac{\lambda}{T} = \left(\frac{g}{k} \tanh(kh) \right)^{\frac{1}{2}} \quad (7)$$

In the deep water ($\frac{h}{\lambda} \geq \frac{1}{2}$; $\left[1 + \frac{2kh}{\sinh(2kh)} \right] = 1$ and $\tanh kh \simeq 1$) were included in Eq. (3) and rearranged conducted to [22]:

$$P = \frac{\rho g^2}{64\pi} H_s^2 T_e \quad (8)$$

In shallow or medium water depths, the nearshore effects must be taken account when calculating the wave power density, including refraction, shoaling, bottom dissipation and sheltering by the coastline or adjacent islands [23]. Indeed, in the shallow water,

$$\left(\frac{h}{\lambda} < 1/20; \left[1 + \frac{2kh}{\sinh(2kh)} \right]_* = 2 \text{ and } \tanh(kh) \simeq \frac{2\pi h}{\lambda} \right)$$

Equation (3) can then be rewritten:

$$P = \frac{1}{16} \rho g H_s^2 \sqrt{gh} \quad (9)$$

For medium water depths, ($1/20 < h/\lambda < 1/2$), shallow water correction must be considered and P can be calculated as:

$$P = \bar{E} \left(\frac{gT_e}{2\pi} (\tanh(kh))^{\frac{1}{2}} \right) * \left[\frac{1}{2} * \left(1 + \frac{2kh}{\sinh(2kh)} \right) \right] \quad (10)$$

with

$$\lambda = \frac{g}{2\pi} T_e^2 \quad (11)$$

In the equations above, P is the wave power per unit of crest length (kW.m^{-1}), H_s is the significant wave height, T_e is the energy period, ρ is the density of seawater (assumed to be 1025 kg.m^3) and g is the gravitational acceleration (assumed to be 9.81 N.kg^{-1}). T_e is computed as a function of spectral moments [26-27]:

$$T_e = \frac{m_{-1}}{m_0} \quad (12)$$

Another approach when T_p is known, the energy period can be assumed as [26-28]:

$$T_e \simeq \alpha T_p \quad (13)$$

where α is a coefficient whose value depends on the shape of the wave spectrum (e.g. 0.86 for a Pierson-Moskowitz spectrum). [27] adopted more conservative assumption of $\alpha \simeq 0.90$ or $T_e \simeq 0.9T_p$. This assumption introduces uncertainty in the resulting wave power. However, the errors in period are less significant than errors in wave height since P is proportional to T_e and to the square of the H_s [29].

The buoy ALIZE, is deployed offshore off Benin's coastline about 6Km at 15m deep corresponding to medium water. Then, we use in this work, the equation (10) for wave power calculation and we assumed that $T_e = T_p$.

2.4.2. Longshore sediment transport rate (LST)

Several empirical formulas are used for LST's calculating. In this work formula proposed by [30] has been used. [31] showed that this formula predicts the longshore sediment transport rates much more accurately. Longshore sediment transport formulae require as input the breaking wave parameters, but global wave hindcasts only provide deepwater characteristics [5].

$$I = 2.33 \cdot H_{sb}^2 T_p^{1.5} \delta^{0.75} d^{-0.25} \sin^{0.6}(2\alpha_b) \quad (14)$$

where I denotes the longshore transport rate in (underwater) kilograms per second (kg/s), H_{sb} the breaking wave height, α_b the local breaking wave angle, T_p is the peak period, δ the beach slope inducing the breaking (i.e. one wave length before

breaking) and $d = d_{50}$ the mean sediment grain size; d is here equal to 0.60 mm based on [32]. The value 2.33 is the dimensional coefficient related to the SI system assuming salt water (1025 kg/m³). Although using a nested numerical model (e.g. SWAN or WW3) to propagate waves from deep water to the break point would have been an ideal option for a short-term study, because of the difficulties presented by the spatio-temporal scales of this study, we have used here the empirical breaking wave predictor proposed by [33] and tested by [5].

[33], proposed an empirical breaking wave predictor formula to estimate H_{sb} which directly provides breaking wave height H_{sb} and angle α_b , given deepwater wave height h_0 , period T and direction α_0 :

$$H_{sb} = \lambda \frac{c^2}{g} \quad (15)$$

$$\alpha_b = a \sin(\sin(\alpha_0) \sqrt{\lambda}) \quad (16)$$

where λ denotes a correction factor defined as :

$$\lambda = \Delta \lambda_\alpha \quad (17)$$

where $\Delta = 1 + 0.1649\zeta + 0.5948\zeta^2 - 1.6787\zeta^3 + 2.8573\zeta^4$

$$\zeta = \lambda_\alpha \sin \theta^2$$

$$\lambda_\alpha = [\cos(\alpha_0)/\theta]^{\frac{2}{5}} \text{ and}$$

$$\theta = \left(\frac{c}{\sqrt{gH}}\right)^4 \left(\frac{c}{C_g}\right) \gamma^2$$

and γ is the constant breaker index defined as [34] :

$$\gamma = \frac{H_{sb}}{d_b} = 0.78 \quad (18)$$

3. RESULTATS AND DISCUSSION

3.1. Sea-wave instantaneous characterization

Fig. 2.a shows average scatter sea-wave regime in terms of H_s and T_p and Fig. 2.b in-

182 dicates the compass rose of wave directions Dir-(Hs) for the 10 months and half peri-
 183 od of buoy dataset. Fig. 2 shows that in Benin coastal area, the significant wave
 184 height can reach more than 2,5 m. The wave periods range from 4 to 14 s and mean
 185 wave directions from 180° to 227° and 165° to 180° (S-SW clockwise). In general, the
 186 waves have significant heights between 0.5 and 2.53m from the south-west quadrant,
 187 i.e., 190° to 235° . The most frequent wave periods are between 5.2 to 10 s. The inter-
 188 val 6–9 s has the most occurrences. It should be noted that several wave trains are
 189 concomitant in the Gulf of Guinea even but the peak energy is dominated by long
 190 swells of the south-west. This is due to the fact that the coast is quite far from the
 191 swelling generation zone to be affected by local and remote waves, which facilitates
 192 the coexistence of multiple wave generation zones [5]

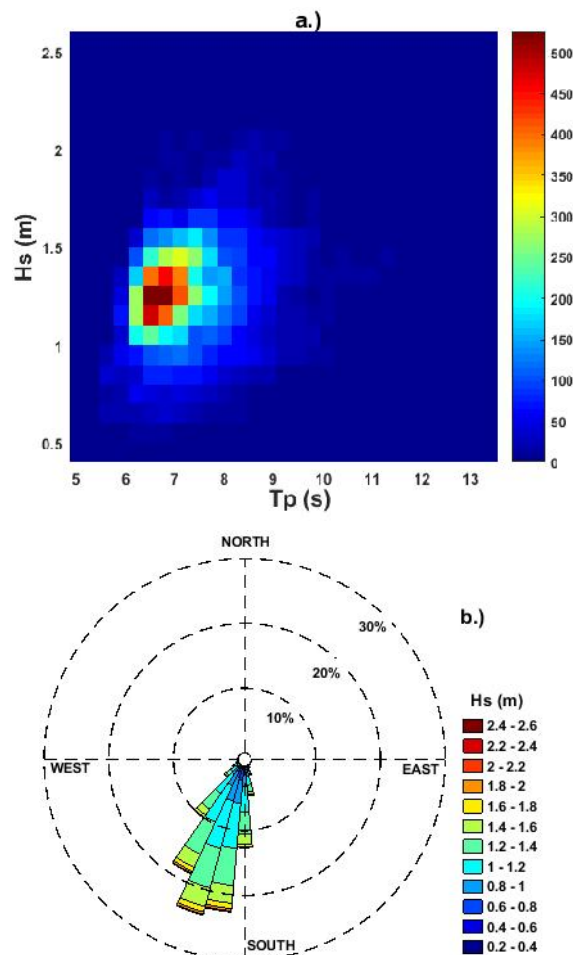


Fig. 2 : Wave scatter diagram (a) and compass rose of wave directions (b) for the period 2015–2016 in Benin coastal area from buoy data sets.

3.2. Sea-wave long term characterization (Non)

3.2.1. Wave parameters instantaneous variability

The equations (1) are used to estimate wave parameters for long term wave consideration and then for wave energy assessment. Fig. 3a average scatter sea-wave regime in terms of H_s and T_p and Fig. 3.b the compass rose of wave directions Dir- H_s for the 14-years period of ERAI reanalysis dataset. H_s averaged occurrences are found between 0.5 and 2.1m (with the most frequent values from 1 to 2 m), associated with mean wave directions from the South/South-West (182° – 210°). The most frequent for wave periods (T_p) are between 6.5 to 13.5 s and 1 to 2.5m for wave height. The interval 7–12 s has the most occurrences for wave period. A statistical study shows that 85.47 percent of T_p was greater than 8s indicating the predominance of the swell.

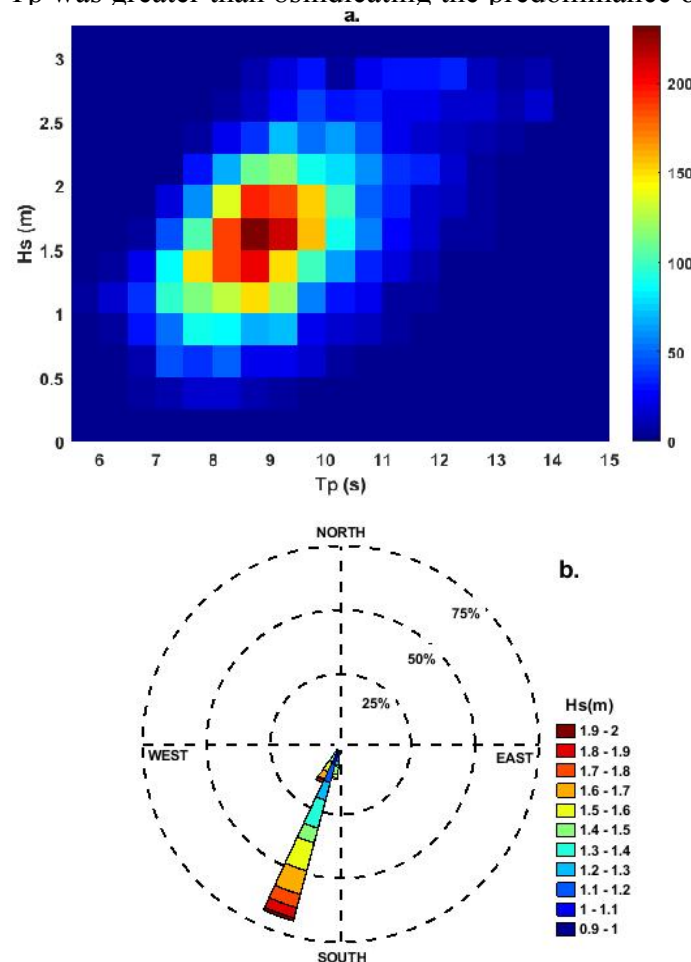


Fig. 3. Wave scatter diagram (a) and compass rose of wave directions (b) for the period 2003–2016 in Benin coastal area from ERAI data sets adjusted by buoy data.

3.2.2. Wave parameters seasonal variability

Figure 6 shows the averaged sea-wave regime in terms of H_s and T_p . At seasonal scale the maximum values of H_s are observed from May to September ranging from 1.19 to 1.68 m averaged of 1.44m with peak values in June, July and August. The figure indicates an increasing tendency of H_s from January to July and decreasing tendency until December. Wave peak period ranging from 8.54s to 9.55s averaged of 9.17s. The seasonality observed is related to wind variability in the Atlantic Ocean. In fact, the winds generated in the South Atlantic maximum in July, increase from January to July and then decrease until December. The seasonality observed is related to wind variability in the Atlantic Ocean. In fact, the winds generated in the South Atlantic maximum in July, increase from January to July and then decrease until December [35-36]

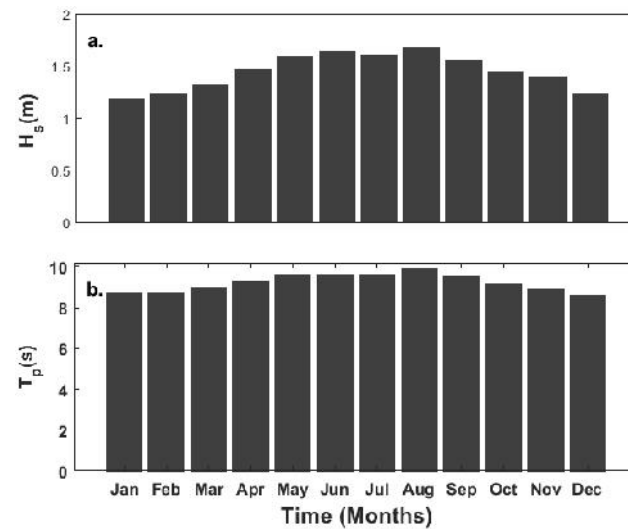


Fig. 4. Averaged H_s (a) and T_p (b) wave regime in Benin's coastal area

3.3. Wave energy potential analysis in Benin coastal area

3.3.1. Wave energy inter-annual variability

Figure 6 indicates wave annual power variability P , from 2002 to 2016 using equation (9) when all types of waves have been taken into account. The figure shows an increasing tendency of wave power ranging from 13.78 to 16.78 kW.m^{-1} averaged of 15.56 kW.m^{-1} with ($\text{std}=0.72$). The majority of wave power averaged (P_{av}) occur-

rences are found in the interval of 14.5 and 17 kW.m⁻¹ (with the most frequent values from 15 to 16.5 kW.m⁻¹). This trend is related to this of the significant height in the Gulf of Guinea. Indeed, [21,36] observed increasing tendency of significant wave height respectively in Ghana and Benin coastal areas. In the sub-region, there is no knowledge of work in this area. But further south, along the South African coast, the average annual wave power available varied from 33 to 41kW.m⁻¹, [37], higher than that found in this work. Referring to the global average wave energy map [38], our results seem to overestimate the values contained therein. Indeed, according to this map, energy available to Beninese coastal area is between 5 and 12kw.m⁻¹. It is important to note that this map was carried out with deep water consideration which is not the case of this study where the energy is assessed with medium water consideration.

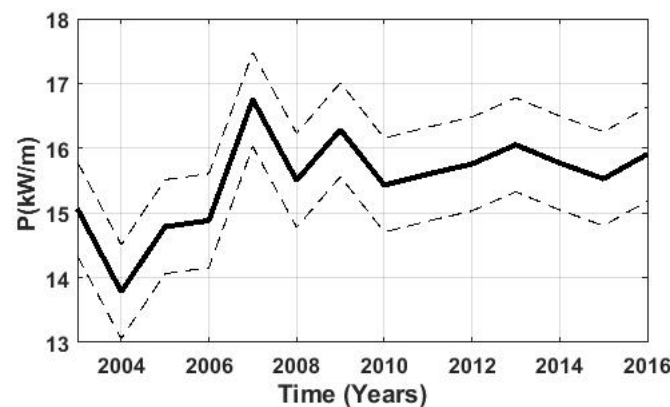


Fig. 5. Annual averaged wave power (14 years). The dashed lines indicate the standard deviation of annual wave power.

3.3.2. Inter-annual statistic of wave energy density

Inter-annual characteristics of annual wave energy deduced from Fig. 5 have been mentioned in Table 1.

Table 1. Inter-annual characteristics of wave energy off Cotonou from 2003 to 2016 and its standard deviation (σ)

Min (kW.m ⁻¹)	Mean(kW.m ⁻¹)	Max(kW.m ⁻¹)	σ
13.78	15.57	16.78	0.72

3.3.3. Wave Seasonal variability

The energy in Benin marine area is strongly influenced by seasonal fluctuations. Figure 6.a indicates wave power's seasonal variability (P) from 2003 to 2016 using equation (9) when all types of waves have been taken into account. The figure shows an increasing tendency of wave power with (std=2.9) from January to august and decreasing tendency until december with values rangind from 9.64 to 21.82 kW.m⁻¹ averaged of 15.76 kW.m⁻¹. The result can be attributed to wave significant height in Gulf of Guinea (Fig. 5.a) [15]. The low values were observed from December to February where the power is less than 15kW.m⁻¹ and the maximum values from March to November where the power is between 15-21.82 kW.m⁻¹. Pronounced seasonal variations in the wave energy are present in this area (Fig. 6.b). Figure 6.b, indicates the assessment of wave energy for the different seasons of year. The wave energy is larger in summer and autumn (20-21.85 kW.m⁻¹) than at in spring and winter (12.75-14.95 kW.m⁻¹); so the wave energy exploitation is mainly in autumn and winter. This variability is similar to the global seasonal distribution of average wave power [29]. Indeed, wave energy average estimated by the global distribution is less than 11kW.m⁻¹ in January and between 11-22 kW.m⁻¹ in July.

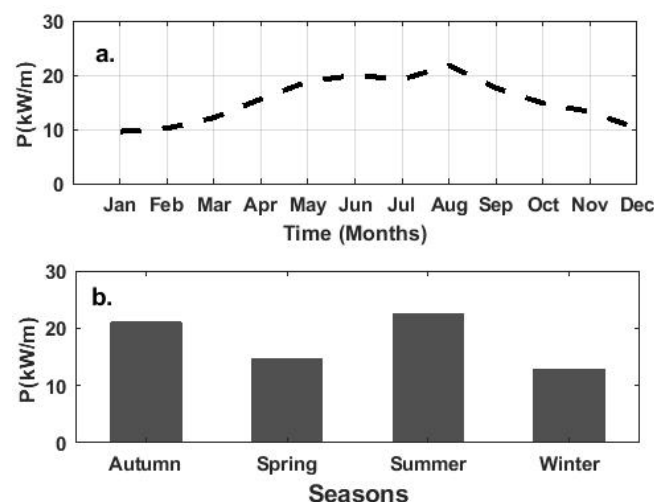


Fig. 6. Average wave energy density, (a) monthly and (b) for each season of the year in Benin marine area.

3.3.4. Seasonal statistic of wave energy density

Seasonal characteristics of annual wave energy deduced from Fig. 6 have been mentioned in Table 2.

Table 2. Inter-annual characteristics of wave energy off Cotonou from 2003 to 2016 and its Standard deviation (σ).

Min (kW.m ⁻¹)	Mean(kW.m ⁻¹)	Max(kW.m ⁻¹)	σ
9.64	15.76	21.85	2.67

3.4. Interannual variability of longshore sediment transport (LST)

Wave parameters characteristics on Benin's coastline (incidence $\approx 9.4^\circ$) induce a longshore current that generates a littoral drift. This drift observed along the coasts of the Gulf of Guinea countries, one of the largest in the world has been estimated in this work using formula proposed by [30], the breaking parameters coming from the empirical breaking wave predictor proposed by [33]. Fig. 7 indicates the inter-annual variability of the longshore sediment flux (LST) estimated from formula 14. This figure shows a significant upward trend of LST with values ranging from 4.56×10^5 to 5.71×10^5 with an average of 5.15×10^5 m³/year (std = 3.12×10^4) directly related to the observed increase in significant wave height in the study area (Gulf of Guinea). Our results are in agreement with those found by [5]. Indeed, using the model developed by [39], the authors found a longshore sediment flux averaged of $\approx 5 \times 10^5$ m³/year on Beninese coast. A little further west, on Ghanaian's coast for example, the longshore sediment flux was estimated at 7.65×10^5 m³/year as a result of the large waves on these exposed open ocean coasts [40]. Further north, [41] using the same theory as [5], found results overestimating those found in our study ($\approx 7 \times 10^5$ m³/year) on Senegalese coast.

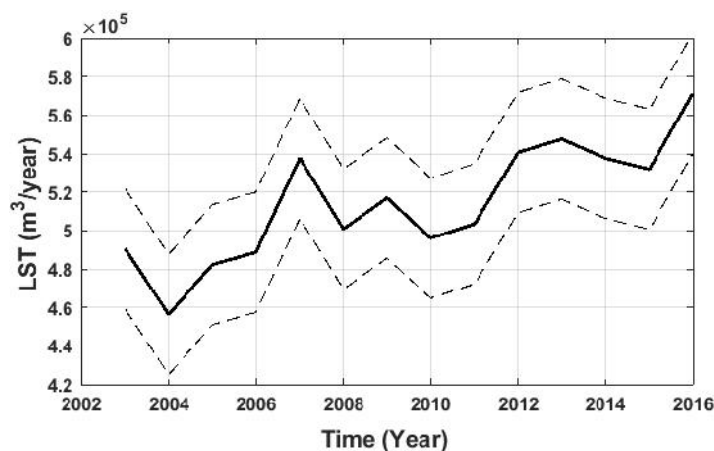


Fig. 7. Inter-annual variability of longshore sediment transport using offshore wave characteristics. The dashed lines indicate the standard deviation of LST

3.5. Shoreline position and offshore wave variability

Wave parameters characteristics on Benin's coastline (wave incidence $\approx 10^\circ$ on average) show the involvement of the swell in the phenomenon of coastal erosion. Wave impact on shoreline evolution was investigated using seasonal variability analysis of shoreline position and the one of wave energy. Fig. 8 shows seasonal wave energy and shoreline position time series. Seasonal cycle of the shoreline position (red curve) presented two main different phases, the erosive phase (January-July) and accretive phase (July to December). The figure indicates that for the first phase, wave energy increases from 10 to 20kW/m but the shoreline has moved from the position 66.70 to 60m, which shows an average sea advance of 6m on the coast. For the second phase, wave energy decreases from 22 to 10.3kW/m but shoreline position increase from 60 to 65m showing an accretion during this phase. This shows that at the seasonal scale, the dynamics of Benin's coastline is strongly influenced by wave energy. Statistical analysis shows that wave energy density and shoreline position are negatively correlated (Correlation coefficient = -0.95).

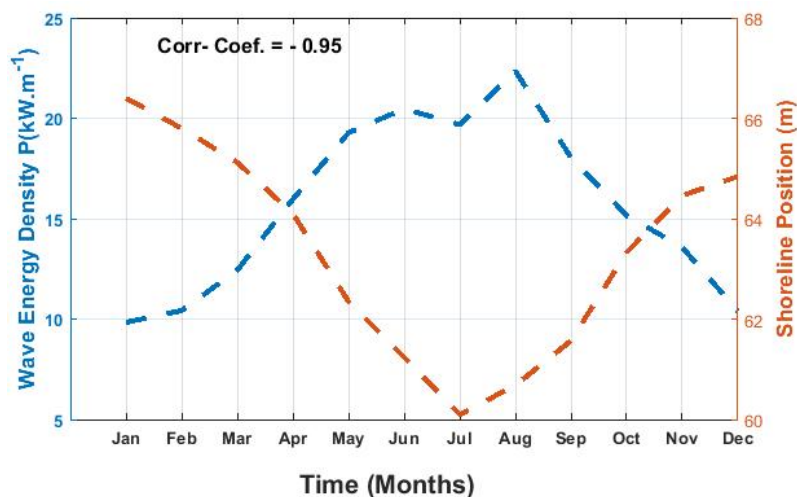


Fig. 8. Seasonal cycle comparison between shoreline position (red) and offshore wave energy (blue).

CONCLUSION

Wave energy potential in Benin coastal area has been characterized and analyzed using fourteen years ERA reanalysis of European Center for Medium-Range Weather Forecasts (ECMWF) wave data sets adjusted with buoy data deployed offshore about 6Km from the Autonomous port of Cotonou (Benin) and more than 15m deep at the coordinates (2°28'46E, 6°18'49N). After, the link between wave energy and coastline has been investigated.

The results indicate that wave energy in Benin coastal area is moderate and available ($H_s \approx 1.36\text{m}$, $T_p \approx 9.6$ and $P \approx 16.62\text{kW/m}$ per wave front). Wave energy is influenced by seasonal variability related to wave parameters (H_s and T_p) in the study area. At seasonal scale, wave energy density and shoreline position are strongly linked ($\sigma^2 = 0.9$).

Given the link between wave energy variability and coastline evolution, wave energy exploitation will help Benin country to improve its energy autonomy and consequently contribute to the mitigation of coastal erosion phenomenon observed this coast.

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