Short Research Article

The Effect of Gravity Loads on Seismic Lateral Displacements of R.C. Frames Using Different Damping Ratios

ABSTRACT:

This paper includes an analytical study for an investigation of the gravity load on the seismic lateral displacements of a R/C building located in Khartoum city, Sudan. The R.C. building used in this study is a 6-storey residential building with 3-bays in each in each direction. Two selected frames of the building were analyzed using STAAD-III program, a linear static and dynamic analysis program, one in N-S direction and the other in E-W direction. The analysis was performed for two types of restraints: fixed and pinned, for both frames under the same loading using for cases of damping ratios (0%, 5%, 10% and 20%) taken as percentages of the critical damping. The program used the Dynamic Response Spectrum method (DRS) to solve the dynamic equilibrium equations of motion. Ground motions, i.e., accelerations versus time periods, used were selected from the 1979 Elcentro earthquake as an input data to calculate the seismic lateral displacements. From this study and regardless of values of damping ratios and types of restraints used, it was found that the gravity load contributed in reducing the lateral displacements by an average amount of 25% (the lateral displacements caused by the combination of (gravity +seismic) loads are less than those caused by the seismic load only.

KEYWORDS: Gravity Load, Seismic Response, Lateral Displacements, Damping ratios.

1. INTRODUCTION:

There is growing responsiveness of multi-storey reinforced concrete structures, to accommodate growing population. The primary purpose of all kinds of structural systems used in the building type of structures is to transfer gravity loads effectively. The most common loads resulting from the effect of gravity are dead load, live load and snow load. Besides these vertical loads, buildings are also subjected to lateral loads caused by wind, blasting or earthquake. Lateral loads can develop high stresses, produce sway movement or cause vibration. Therefore, it is very important for the structure to have sufficient strength against vertical loads together with adequate stiffness to resist lateral forces. Many researchers have investigated the contribution of gravity load on seismic response of structures, such as Kulkarni J. G. et al., [1] (2013) who presented an analysis of Multi-storey Building Frames Subjected to Gravity and Seismic Loads with Varying Inertia.

This paper also highlighted on response of reinforced concrete frames for variation of axial force for spread of haunch and storey drift.

A. E. Hassaballa et.al.,[2] (2013) presented a paper on Seismic Analysis of a Reinforced Concrete Building by Response Spectrum Method, using SAP2000 program as a tool of analysis. The study found that the calculated drifts resulting from the nodal displacements due to the combination of static and seismic loads were about 2 to 3 times the allowable drifts and the compressive stresses in ground floor columns were about 1.2 to 2 times the tensile stresses. Mario Galli [3] (2006), evaluated the Seismic Response of Existing R.C. Frame Buildings with Masonry Infills. From his results obtained it can be noted that the presence of masonry infills has a dual effect on the overall structural response. also when the infill panels are regularly distributed in the frame (uniformly infilled frame), the seismic response of the structure was characterized by a soft storey mechanism developing as a consequence of the brittle failure of masonry panels at a particular level, that produces a sudden reduction of strength and stiffness and an increase in the storey deformation demand.

Recent extensive analytical-numerical studies on the response of gravity load designed concrete frame buildings (with and without infills) underlined the peculiar vulnerability of the joint panel zone region. Focus has been given to the damage mechanisms occurring in the joint as well as to their interaction with the global frame response (Guido [4], ANGELO MASI [5], Pampanin [6], Calvi [7]).

The objective of this paper is to investigate the effect of gravity load on the lateral displacements of reinforced concrete frames, located in Khartoum city, subjected to seismic loads.

2. Method of Analysis

The most commonly used methods of analysis are based on the approximation that the effects of yielding can be accounted for by linear analysis of the building, using the design spectrum for inelastic system. Forces and displacements due to each horizontal component of ground motion are separately determined by analysis of an idealized building having one lateral degree of freedom per floor in the direction of the ground motion component being considered. Such analysis may be carried out by the seismic coefficient method (static method) or response spectrum analysis procedure (dynamic method).

2.1. Response Spectrum Analysis

A response spectrum is simply a plot of the peak or steady-state response (displacement, velocity or acceleration) of a series of oscillators of varying natural frequency, that are forced into motion by the same base vibration or shock. In the response spectrum method, the response of a structure during an earthquake is obtained directly from the earthquake response (or design) spectrum. This procedure [8] gives an approximate peak response, but this is quite accurate for structural design applications. In this approach, the multiple modes of response of a building to an earthquake are taken into account. For each mode, a response is read from the design spectrum, based on the modal frequency and the modal mass. The responses of different modes are combined to provide an estimate of total response of the structure using modal combination methods such as complete quadratic combination (CQC), square root of sum of squares (SRSS), or absolute sum (ABS)

method. Response spectrum method of analysis should be performed using the design spectrum specified or by a site – specific design spectrum, which is specifically prepared for a structure at a particular project site. The same may be used for the design at the discretion of the project authorities.

3. FRAME DETAILS AND STUDY CASES:

A residential six-storey three-bay R. C. frame building in Khartoum City with 15 m X 12.5 m plan as shown in Fig.1was considered for the analysis. Two selected frames of this building were analyzed and checked using STAAD III program, one in North- South (N-S) direction and the other in East–West (E-W) direction as shown in Fig. 2. The sections of columns and beams are shown in Table 1.

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Floor Level	Ground Floor	1 st Floor	2 nd Floor	3 rd Floor	4 th Floor	Roof
Columns	500*250	500*250	400*250	400*250	300*250	300*250
Beams	500*250	500*250	500*250	500*250	500*250	400*250

Table 1: Sections of columns and beams of the studied frame

Typical slab thickness is 125 mm.

The three designed loads used in the analysis were the actual dead load, live load and seismic load. Three combinations of load cases were applied as follows:

- Load Case 1 (LC1) is gravity load (dead and live).
- Load Case 2 (LC2) is seismic load only.
- Load Case 3 (LC3) is (gravity + seismic) loads.

A uniformly distributed gravity load of 20 kN/m was applied including the own weights of members. The program uses the Dynamic Response Spectrum method (DRS) to solve the dynamic equilibrium equations of motion. The ground accelerations versus time period were used as an input data to calculate the seismic response spectrum parameters, i. e., displacements in this research. The ground excitations used were selected from the 1979 Elcentro earthquake and a total time of vibration of 8 seconds was considered.. The analysis was performed for two types of restraints; fixed and pinned for the same frames under the same loadings using four values of damping ratios (0%, 5%, 10% and 20%) as representative values of damping for the range of construction. The damping ratios were taken as percentages of the critical damping.

The selected nodes are shown in Fig. 2.

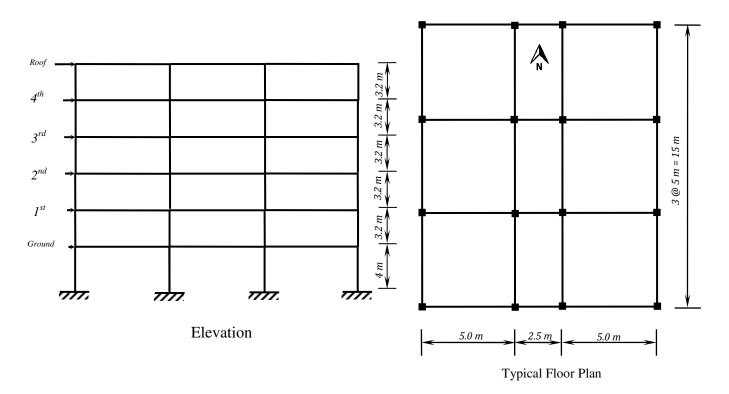


Fig. 1: Dimensions of the Studied Frame Building

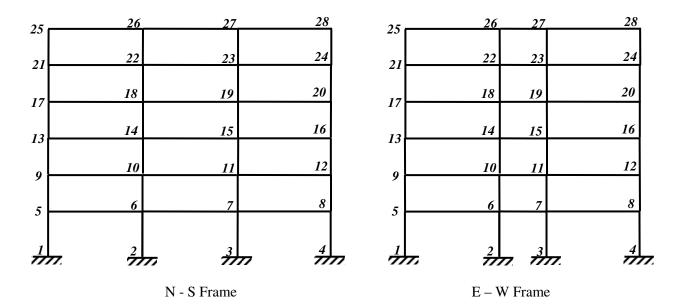


Fig. 2: Selected Nodes of the Studied Frames

3.1. Lateral displacement

It is displacement caused by the Lateral Force on the each storey level of structure. Lateral displacement will be more on top storey. Hence after analyzing the Building the results obtained for these models in both longitudinal and transverse direction and the comparisons between them are presented in tabular form.

3.2. Damping ratios

The damping ratio is a parameter, usually denoted by ζ (zeta) [9] that reflects capacity of dissipating energy and has significant influence on the vibrations of buildings, is regarded as a constant in the seismic design at present. The damping ratio is dimensionless, because it is the result of dividing the units of the damping constant ($N \cdot s/m$) by the critical damping constant ($N \cdot s/m$); the units cancel out.

8.3 Results of the Analysis

The analysis was performed for static and seismic loads. The seismic analysis used horizontal input motion of earthquake with moderate horizontal peak ground acceleration (PGA_H). The results of the analysis are shown in Tables 2 to 5 and Figures to show the relations between displacements for fixed and pinned restraints, using four values of damping ratios.

Results of N-S Frame Building:

r													
Joints	Displa	cements o	due to se	ismic		-	ents due				nce (%):		
		load o	only		(seismic+gravity) loads				{(LC2 – LC3)/LC2}*100				
		(LC	C2)			(LC	C 3)						
	2	3	4	5	6	7	8	9	2-6	3-7	4-8	5-9	
	0%	5%	10%	20%	0%	5%	10%	20%	0%	5%	10%	20%	
5	7.533	2.460	1.840	1.516	5.647	1.842	1.376	1.134	25.044	25.134	25.179	25.216	
6	7.551	2.466	1.844	1.519	5.662	1.848	1.382	1.138	25.015	25.070	25.060	25.076	
7	7.551	2.466	1.844	1.519	5.665	1.851	1.384	1.141	24.985	24.956	24.935	24.931	
8	7.533	2.460	1.840	1.516	5.653	1.847	1.383	1.140	24.957	24.866	24.821	24.781	
9	14.380	4.703	3.514	2.888	10.787	3.529	2.637	2.167	24.990	24.971	24.957	24.952	
10	14.371	4.700	3.511	2.886	10.778	3.526	2.634	2.165	24.997	24.990	24.988	24.985	
11	14.371	4.700	3.511	2.886	10.777	3.525	2.633	2.164	25.003	25.010	25.014	25.016	
12	14.380	4.703	3.514	2.888	10.784	3.526	2.634	2.165	25.010	25.031	25.040	25.048	
13	22.173	7.265	5.421	4.439	16.629	5.448	4.064	3.328	25.005	25.015	25.022	25.024	
14	22.177	7.266	5.421	4.439	16.632	5.449	4.066	3.329	25.002	25.006	25.007	25.009	
15	22.176	7.266	5.421	4.439	16.633	5.450	4.066	3.330	24.998	24.995	24.992	24.991	
16	22.173	7.265	5.421	4.439	16.631	5.450	4.067	3.330	24.995	24.983	24.979	24.972	
17	28.476	9.340	6.961	5.679	21.359	7.007	5.223	4.261	24.993	24.980	24.972	24.967	

 Table 2: The Effect of gravity load on lateral displacements for fixed restraint using four values of damping ratios

	1											
18	28.470	9.338	6.970	5.678	21.354	7.005	5.220	4.259	24.998	24.993	25.102	24.987
19	28.470	9.338	6.959	5.678	21.352	7.003	5.219	4.258	25.002	25.008	25.010	25.012
20	28.476	9.340	6.961	5.679	21.355	7.003	5.219	4.258	25.007	25.021	25.028	25.033
21	35.516	11.651	8.671	7.043	26.636	8.737	6.503	5.281	25.003	25.008	25.011	25.013
22	35.519	11.652	8.672	7.043	26.639	8.739	6.504	5.282	25.001	25.003	25.003	25.004
23	35.519	11.652	8.672	7.043	26.639	8.739	6.504	5.283	24.999	24.998	24.997	24.995
24	35.516	11.651	8.671	7.043	26.638	8.739	6.504	5.283	24.997	24.992	24.989	24.986
25	39.168	12.842	9.552	7.740	29.381	9.636	7.168	5.809	24.988	24.963	24.950	24.938
26	39.168	12.842	9.551	7.740	29.377	9.633	7.165	5.806	24.996	24.988	24.983	24.980
27	39.168	12.842	9.551	7.740	29.374	9.630	7.162	5.803	25.004	25.013	25.016	25.021
28	39.168	12.842	9.552	7.740	29.371	9.627	7.159	5.800	25.012	25.037	25.049	25.061
	% Average Difference										25.000	25.000

 Table 3: The Effect of gravity load on lateral displacements for pinned restraint using four values of damping ratios

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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	S			•		(sei	0	•	ds	{(L	C2 - LC.	3)/LC2}*	100
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$,	1			1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		2	3	4	5	6	7	8	9	2-6	3-7	4-8	5-9
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		0%	5%	10%	20%		5%	10%					
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	5	23 205	9 162	6 7 2 7	5 310		6 867	5 041	3.97		25.04		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		25.205	7.102	0.727	5.510		0.007	5.041					
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	6	23 230	9 1 7 2	6 7 3 4	5 3 1 5	17.42	6 877	5 049			25.01		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0	23.230	2.172	0.751	5.515		0.077	5.017					
8 23.205 9.162 6.727 5.310 8 4 1.40 8 8 4 4 4 9 3.9 9 30.229 11.94 8.765 6.913 22.67 8.957 6.575 5.18 24.99 24.98 24.98 24.98 24.98 24.98 24.98 24.98 24.98 24.98 24.98 24.99 24.91 25.00 25.00 <t< td=""><td>7</td><td>23 230</td><td>9 172</td><td>6 7 3 4</td><td>5 315</td><td></td><td>6 880</td><td>5.052</td><td></td><td></td><td></td><td></td><td></td></t<>	7	23 230	9 172	6 7 3 4	5 315		6 880	5.052					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$,	23.230	2.172	0.751	5.515		0.000	5.052					
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	8	23.205	9.162	6.727	5.310		6.876	5.049					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	9	30.229		8.765	6.913		8.957	6.575					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	10	30.210		8.760	6.909		8.950	6.570					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	11	30.210		8.760	6.909		8.950	6.569					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	12	30.229		8.765	6.913		8.954	6.572					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				10.51		-	10.74						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	36.259			8.284			7.886					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									_				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	36.262			8.284			7.887					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				-						-			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	36.262			8.284			7.888					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										4			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	16	36.259			8.284			7.888					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<u> </u>										I		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17	40.789			9.305			8.874					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	L			1		-			-	•			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	40.785			9.304			8.872					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		10 - 0 -		•		•			-				
	19	40.785			9.304			8.870					
	20	40.789			9.305			8.870	6.97				

		8	9		0	4		7	5	2	7	1
21	45 617	18.03	13.22	10.38	34.21	13.52	9.914	7.78	25.00	25.00	25.00	25.00
21	45.617	2	0	1	2	3	9.914	4	2	5	7	9
22	45.619	18.03	13.22	10.38	34.21	13.52	9.915	7.78	25.00	25.00	25.00	25.00
22	45.019	3	1	1	4	4	9.915	6	0	2	2	2
23	45.619	18.03	13.22	10.38	34.21	13.52	9.916	7.78	24.99	24.99	24.99	24.99
23	45.019	3	1	1	4	5	9.910	6	9	8	8	8
24	45.617	18.03	13.22	10.38	34.21	13.52	9.916	7.78	24.99	24.99	24.99	24.99
24	45.017	2	0	1	4	5	9.910	6	8	5	3	0
25	48.063	18.99	13.92	10.92	36.05	14.24	10.44	8.19	24.99	24.97	24.96	24.95
23	40.003	1	0	0	2	5	5	5	0	4	6	7
26	48.063	18.99	13.92	10.92	36.04	14.24	10.44	8.19	24.99	24.99	24.98	24.98
20	46.005	1	0	0	9	6	2	2	7	2	9	5
27	48.063	18.99	13.92	10.92	36.04	14.24	10.43	8.18	25.00	25.01	25.01	25.01
27	46.005	1	0	0	5	0	8	8	3	4	2	5
28	48.063	18.99	13.92	10.92	36.04	14.23	10.43	8.18	25.01	25.02	25.03	25.04
28	40.005	1	0	0	3	8	5	5	0	5	4	4
	07 American Difference										25.00	25.00
	% Average Difference										0	0

Results of E-W Frame Building:

 Table 4: The Effect of gravity load on lateral displacements for fixed restraint using four values of damping ratios

Joint	Disp	laceme	nts du	e to	Disp	laceme	ents du	ie to		Differer	nce (%):	
S	se	ismic lo	ad onl	у	(seisn	nic+gra	avity) l	loads	{(LC	C2 - LC	3)/LC2}*	*100
		(LC	C2)			(LC	23)					
	2	3	4	5	6	7	8	9	2-6	3-7	4-8	5-9
	0%	5%	10%	20%	0%	5%	10%	20%	0%	5%	10%	20%
5	6.859	2.153	1.61	1.34	5.141	1.61	1.20	1.00	25.043	25.142	25.187	25.229
			5	1		2	8	3				
6	6.878	2.160	1.62	1.34	5.159	1.61	1.21	1.00	25.004	25.014	25.021	25.022
			0	5		9	5	8				
7	6.878	2.160	1.62	1.34	5.159	1.62	1.21	1.00	24.996	24.986	24.985	24.978
			0	5		0	5	9				
8	6.859	2.153	1.61	1.34	5.147	1.61	1.21	1.00	24.956	24.858	24.816	24.774
			5	1		8	4	9				
9	12.87	4.048	3.03	2.51	9.661	3.03	2.27	1.88	24.988	24.964	24.952	24.941
	9		3	3		7	7	6				
10	12.86	4.043	3.03	2.51	9.649	3.03	2.27	1.88	24.999	24.997	24.999	24.997
	5		0	0		3	3	3				
11	12.86	4.043	3.03	2.51	9.648	3.03	2.27	1.88	12.865	25.002	25.002	25.001
	5		0	0		2	3	2				
12	12.87	4.048	3.03	2.51	9.658	3.03	2.27	1.88	12.879	25.036	25.048	25.057
	9		3	3		4	4	3				
13	19.90	6.263	4.68	3.87	14.92	4.69	3.51	2.90	19.904	25.016	25.023	25.029
	2		8	0	6	6	5	1				
14	19.90	6.263	4.68	3.87	14.92	4.69	3.51	2.90	19.903	25.002	25.004	25.005
	3		8	0	7	7	6	2				
15	19.90	6.263	4.68	3.87	14.92	4.69	3.51	2.90	19.903	24.998	24.997	24.997
	3		8	0	7	8	6	2				
16	19.90	6.263	4.68	3.87	14.92	4.69	3.51	2.90	19.902	24.982	24.977	24.972
	2		8	0	8	9	7	3				

			70 AVE	age D	merence	C			0	0	0	0
			0% A 10	rogo D	ifferenc	0			25.00	25.00	25.00	25.00
	6	6	1	2	5	8	4	7				
28	35.62	11.21	8.37	6.84	26.71	8.40	6.27	5.12	35.626	25.039	25.053	25.066
	6	6	1	2	9	2	8	1				
27	35.62	11.21	8.37	6.84	26.71	8.41	6.27	5.13	35.626	25.002	25.006	25.00
	6	6	1	2	0	3	9	2				
26	35.62	11.21	8.37	6.84	26.72	8.41	6.27	5.13	35.626	24.996	24.993	24.992
	6	6	1	2	4	7	3	6				
25	35.62	11.21	8.37	6.84	26.72	8.41	6.28	5.13	35.626	24.960	24.947	24.93
	1	9	8	7	7	2	5	7	02.221		,	> 0.
24	32.22	10.14	7.57	6.20	24.16	7.61	5.68	4.65	32.221	24.990	24.987	24.98
20	1	9	8	7	6	2	4	6	52.221	21.999	21.777	2
23	32.22	10.14	7.57	6.20	24.16	7.61	5.68	4.65	32.221	24.999	24.999	24.99
22	1	9	8	0.20	6	1	4	05	52.221	25.001	25.001	25.00
22	32.22	10.14	7.57	6.20	24.16	7.61	5.68	4.65	32.221	25.001	25.001	25.00
21	32.22	9	8	0.20	24.10 5	0	3.08	4.05	32.221	23.010	25.015	23.010
21	32.22	10.14	7.57	6.20	24.16	o 7.61	5.68	4.65	32.221	25.010	25.013	25.01
20	23.03	8.079	0.04	4.90 9	19.23 9	8	4.32 9	5.72 6	23.034	23.022	25.050	23.05
20	6 25.65	8.079	9 6.04	8 4.96	4 19.23	7 6.05	9 4.52	6 3.72	25.654	25.022	25.030	25.034
19	25.64	8.077	6.03	4.96	19.23	6.05	4.52	3.72	25.646	25.002	25.003	25.003
10	6	0.077	9	8	5	8	9	6	25.616			
18	25.64	8.077	6.03	4.96	19.23	6.05	4.52	3.72	25.646	24.998	24.996	24.99
	4		1	0	2	1	2	9				
17	25.65	8.079	6.04	4.97	19.24	6.06	4.53	3.72	25.654	24.979	24.972	24.96

 Table 5: The Effect of gravity load on lateral displacements for pinned restraint using four values of damping ratios

Joint		placem		-	Ŭ	olaceme	ents du	e to		Differer	nce (%):	:	
S	se	eismic l	oad onl	у	(seisi	nic+gra	avity) l	oads	{(LC2 – LC3)/LC2}*100				
		(L	C2)		(LC3)								
	2	3	4	5	6	7	8	9	2-6	3-7	4-8	5-9	
	0%	5%	10%	20	0%	5%	10	20	0%	5%	10%	20%	
				%			%	%					
5	21.45	8.246	6.075	4.813	16.09	6.180	4.552	3.606	25.018	25.047	25.065	25.082	
	8				0								
6	21.48	8.257	6.083	4.820	16.11	6.192	4.562	3.614	25.002	25.005	25.007	25.007	
	7				5								
7	21.48	8.257	6.083	4.820	16.11	6.193	4.563	3.615	24.998	24.995	24.993	24.992	
	7				5								
8	21.45	8.246	6.075	4.813	16.09	6.188	4.560	3.614	24.982	24.952	24.936	24.917	
	8				7								
9	27.59	10.60	7.813	6.186	20.69	7.957	5.862	4.641	24.994	24.985	24.979	24.973	
	4	8			7								
10	27.56	10.59	7.806	6.181	20.67	7.949	5.858	4.636	25.000	24.999	24.999	24.999	
	8	8			6								
11	27.56	10.59	7.806	6.181	20.67	7.948	5.854	4.635	25.001	25.000	25.001	25.002	
	8	8			6								
12	27.59	10.60	7.813	6.186	20.69	7.954	5.858	4.638	25.006	25.016	25.021	25.026	
	4	8			4								

			% Ave	erage D	ifferenc	e			25.00 0	25.00 0	25.00 0	25.00 0
	8	7	8		1	0						
28	44.04	16.93	12.45	9.812	33.03	12.70	9.339	7.355	25.010	25.026	25.036	25.045
20	8	7	8	0.010	6	2	0.000	7.055	25.010	25.026	25.026	25.045
27	44.04	16.93	12.45	9.812	33.03	12.70	9.343	7.359	25.001	25.003	25.004	25.005
	8	7	8		7	4						
26	44.04	16.93	12.45	9.812	33.03	12.70	9.344	7.360	24.999	24.997	24.995	24.995
23	44.04 8	10.95 7	12.43 8	7.012	55.04 0	12.70	7.340	1.505	24.990	24.974	24.905	24.934
25	44.04	4	12.45	9.812	33.04	12.70	9.348	7.363	24.990	24.974	24.965	24.954
24	41.73 6	16.05 4	11.81 1	9.311	31.30 3	12.04 2	8.859	6.984	24.998	24.994	24.991	24.990
24	6	4	1	0.011	2	1	0.050	6.001	24.000	24.001	24.001	24.000
23	41.73	16.05	11.81	9.311	31.30	12.04	8.858	6.983	25.000	25.000	24.999	24.999
	6	4	1		2	1						
22	41.73	16.05	11.81	9.311	31.30	12.04	8.858	6.983	25.000	25.001	25.001	25.001
	6	4	1		1	0						
21	41.73	16.05	11.81	9.311	31.30	12.04	8.857	6.982	25.002	25.006	25.009	25.011
	6	1	3		5	1						
20	37.19	14.31	10.53	8.318	27.89	10.73	7.898	6.237	25.005	25.013	25.016	25.020
1)	1	9	10.55	0.517	3	1	1.070	0.237	23.000	23.001	23.002	23.002
19	37.19	14.30	10.53	8.317	27.89	10.73	7.898	6.237	25.000	25.001	25.002	25.002
18	37.19 1	14.30 9	10.53 1	8.317	27.89 3	10.73 2	7.899	6.238	25.000	24.999	24.999	24.999
10	6	1	2	0.217	9	5	7.000	()))	25.000	24.000	24.000	24.000
17	37.19	14.31	10.53	8.318	27.89	10.73	7.901	6.240	24.995	24.988	24.983	24.979
	8	4			2							
16	33.02	12.70	9.354	7.396	24.77	9.529	7.016	5.548	24.997	24.991	24.989	24.984
	8	4			1							
15	33.02	12.70	9.354	7.396	24.77	9.528	7.015	5.547	25.000	24.999	24.999	24.998
	8	4	2.551	1.570	1	2.020	1.015	0.017	20.001	20.001	20.002	20.002
14	33.02	12.70	9.354	7.396	24.77	9.528	7.015	5.547	25.001	25.001	25.002	25.002
	33.02 8	12.70 4	9.354	7.396	24.77 0	9.527	7.014	5.546	25.003	25.009	25.012	25.014

Discussion of the Results:

From the results obtained, see the above Tables and Figures, it is shown that the displacements increase when using pinned restraint, being nearly double (sometimes triple) that for fixed restraint. The effect of damping ratios is clearly noticed for fixed and pinned restraints, i.e., when damping ratio increases, displacements decrease. It is found that the presence of gravity load in the analysis resulted in decreasing the lateral displacements by an amount of 25%. This effect of gravity load on displacements occurred in all cases of analysis, regardless of types of restraints, values of damping ratios and orientation of frames, whether in N-S or E-W direction, for the vertical downward line of action of gravity load to the base of building. Or by another expression, the perpendicularity of line of action of gravity load to the horizontal excitation of motion affected in decreasing the values of lateral displacements in the studied frames.

Conclusions:

This paper presents an investigation of the role of gravity load in seismic lateral displacements generated from a horizontal component of ground motion. From the results obtained in this analysis, it can be concluded that:

- 1. It was found that the gravity load contributed in reducing the lateral displacements by an average amount of 25% for all cases of damping ratios and types of restraints.
- 2. The damping ratios used in the analysis have significant effect in the values of lateral displacements, as displacements decrease with the increase of damping ratios.

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