Dynamic Model of a DC Motor-gear-alternator (MGA) System

Abstract :

Mathematical models of control systems are mathematical expressions which describe the relationships among system inputs, outputs and other inner variables. Establishing the mathematical model describing the control system is the foundation for analysis and design of control systems. The present study designed a DC motor- gear-alternator (MGA) model where DC motor is the prime mover used to drive an alternator through specialized gears employed in between alternator and DC motor. The fundamental equations that describe the system were presented, and then developed transfer function and Simulink model for the system. The workability of the model is then tested using some numerical values. Results showed that the output voltage increases exponentially with time. Finally, the effect of each of the PID parameters on the closed-loop dynamics were discussed and demonstrated how to use a PID controller to improve the system performance.

Aims :

- (i) To construct a mathematical model describing the dynamics of the MGA set coupled through a gear ratio.
- (ii) To design transfer function, which is a compact description of the input/output relation for the model.
- (iii) To construct a Simulink model of MGA System.
- (iv) Test the model using numerical values(assumed data)

Place and Duration of Study:

Moi University, Department of Mathematics and Physics, between May 2015 and July 2016.

Keywords: DC motor, alternator, gears, transfer function, Simulink.

1.0 Introduction:

A DC Motor-Gear-Alternator (MGA) system is a device for converting electrical power to another form. Typically, MGA sets are used to convert frequency, voltage, or phase of power. Large motor-alternators are widely used to convert industrial amounts of power while smaller motor-alternators are used to convert battery power to higher voltages. A need exists for a low cost, high power electrical alternator capable of operating at low energy. Such alternators may be directly wind-driven by large propellers or may also be directly driven by water wheels or turbines in streams or dams or the one driven by DC motor. Some of these require high efficiency conversion of motive power to electrical power. Such systems, when operated as vehicle propeller, can eliminate the need for internal combustion engine. Shaik Rasheed Ahameed designed a simple recycling AC electrical energy generation system

with small DC input & high efficiency with good load handling capability. The main intention of his research work is to design low cost AC electrical energy generation implementation system without any mechanical energy input [1]. The present study intends to construct a Mathematical model for a Motor-Gear- Alternator set which is used to describe the dynamics of the system.MGA is very often used in industrial applications, for instant, motors have application in servo systems used in robotics and other motion control devices [2], in many engineering fields such as model analysis, control system design, and condition monitoring [3]. The mathematical model can be used to explain the behavior of such system and to predict its response to various inputs at different conditions [4].

1.1 Methodology:

The Laplace transform method is a very useful mathematical tool[5, 6] for solving linear differential equations. By use of Laplace transforms, operations like differentiation and integration can be replaced by algebraic operations such that, a linear differential equation can be transformed into an algebraic equation in a complex variable *s*. The solution of the differential equation may be found by inverse Laplace transform operation simply by solving the algebraic equation involving the complex variable *s*.

1.2 System Modeling:

Since some mathematical problems are to be solved, a mathematical model of the dynamics of the control system components and subsystems are to be formulated. The differential equation and the state variable representation are very popular mathematical models for describing the dynamics of a control system. The transfer function model is applicable if the system is linear. If the description of the system behavior is linguistic then fuzzy logic and fuzzy model of the system will be needed [7-9].

2.0 Simulation diagram from transfer function:

We presented here one method for deriving a simulation diagram from the transfer function[10]. Since the statevariable representation is not unique, there are, theoretically, an infinite number of ways of writing the state equations. Analogous procedure may be followed for writing the discrete state equation from transfer function. The transfer function of single-input-single-output system of the form [10],

$$G(s) = \frac{a_{n-1}s^{n-1} + a_{n-2}s^{n-2} + \dots + a_{1}s + a_{0}}{b_{n}s^{n} + b_{n-1}s^{n-1} + \dots + b_{1}s + b_{0}}$$
(1)

Where a_i , b_i ; i = 0, 1, 2, ..., n - 1 are constants and n is the degree of polynomial in s. It can be written, after introducing an auxiliary variable E (s), as [10],

$$\frac{Y(s)}{U(s)} = G(s) = \frac{a_{n-1}s^{n-1} + a_{n-2}s^{n-2} + \dots + a_1s + a_0}{s^n + b_{n-1}s^{n-1} + \dots + b_1s + b_0} \frac{E(s)}{E(s)}$$
(2)

Another convenient and useful representation of the continuous system is the signal flow graph or the equivalent simulation diagram. These two forms can be derived, after dividing both the numerator and denominator of Equation

(2) by 💅.

$$G(s) = \frac{Y(s)}{U(s)} = \frac{a_{n-1}s^{n-1} + a_{n-2}s^{n-2} + \dots + a_{1}s^{-n+1} + a_{0}s^{-n}}{1 + b_{n-1}s^{-1} + \dots + b_{0}s^{-n}} \frac{E(s)}{E(s)}$$
(3)

From this expression we obtain two equations

$$Y(s) = (a_{n-1}s^{n-1} + a_{n-2}s^{n-2} + \cdots + a_1s^{-n+1} + a_0s^{-n})E(s)$$
(4)

is the Laplace transform of y(t)

$$U(s) = (1 + b_{n-1}s^{-1} + \dots + b_1s^{1-n} + b_0s^{-n})E(s)$$
(5)

is the Laplace transform of u(t). And Equation (4) can be rewritten in the form

$$E(s) = U(s) - b_{n-1}s^{-1}E(s) - \dots - b_1s^{1-n}E(s) - b_0s^{-n}E(s)$$
(6)

Equations (4) and (6) may be used to draw the signal flow graph shown in Figure 1, whose transfer function is given by Equation (1).



Figure 1: Signal flow graph representation of Equation (1)

In signal flow graph the term $s^{-1} = 1/s$ represents pure integration. The signal flow graph of Figure 1 can also be represented by the equivalent simulation diagram, with the states indicated as in Figure 2.Noting the structure of the signal flow graph in Figure 1 and its association with the numerator and denominator polynomials represented by Equations (4) and (5) respectively, it is apparent that the signal flow graph or simulation diagram can be obtained by inspection of the transfer function in Equation (1). The structure of Figure 1, together with Equations (4) and (5), is referred to as the phase variable canonical form of system representation.



Figure 2: Simulation diagram equivalent to the signal flow graph in Figure 1 [10]

Another standard form called observer canonical form is shown in Figure 3. The equivalence of the system in Figure 3 to the Equation (1) may be established by computing the transfer function Y(s)/U(s) from the figure.



Figure 3: Observer Canonical Form

2.1 Open-loop system:

The physical model for the DC Motor-Gear-Alternator assembly used in this study is shown in Figure 4



Figure 4: Physical model for the DC motor-gear-alternator.

The gear unit is introduced between the motor and the alternator as an amplifying system of any input parameter including voltage and current. The amplification power of the gear unit requires an establishment of the relationship between the gear ratio, the input voltage and the voltage output. This is primarily made possible by developing a mathematical model incorporating this correlation.

The schematic representation for the DC motor- gear-alternator set components is shown in Figure 5.



Figure 5: Schematic representation of the DC motor-gear-alternator

2.2 System equations:

The mathematical model for DC motor-gear-alternator is found using Kirchhoff's voltage law[11], ohm's law [12] and Newton's second law of motion[13].

The electric circuit of the motor is shown in Figure 6



Figure 6: DC Motor model

In a more general case, inductance [14] is defined as

$$\mathbf{L} = \frac{\mathrm{d}\boldsymbol{\phi}}{\mathrm{d}\mathbf{i}}$$

Any change in the current through an inductor creates a changing flux, inducing a voltage across the inductor. By Faraday's law of induction, the voltage induced by any change in magnetic flux through the circuit is,

(7)

$$\mathbf{v} = \frac{\mathrm{d}\boldsymbol{\varphi}}{\mathrm{d}\mathbf{t}} \tag{8}$$

Substituting for du in (8), above using (7) yields,

$$\mathbf{v} = \frac{\mathrm{d}}{\mathrm{d}\mathbf{t}} \left(\mathrm{L}\mathbf{i} \right) = \mathrm{L} \frac{\mathrm{d}\mathbf{i}}{\mathrm{d}\mathbf{t}} \tag{9}$$

The voltage \mathbf{v} of the motor is proportional to the angular velocity of the shaft by a constant factor \mathbf{k}_{e} .

 $\mathbf{v} = k_{e} \boldsymbol{\omega}$

Where $\mathbb{R}_{\mathfrak{g}}$ is the electrical constant, inherent to the motor, and ω is the angular velocity of the motor. The current through the conductor can be obtained using Ohm's law. Ohm's law states that the current through a conductor between two points is directly proportional to the voltage across the two points. Introducing the constant of proportionality, the resistance, mathematical equation that describes this relationship is,

(10)

$$i = \frac{v}{R}$$
(11)

Where, i, is the current through the conductor, v, is the voltage measured across the conductor in units of volts, and R is the resistance of the conductor in units of ohms. Applying Kirchhoff's voltage law to the motor we obtain,

$$\mathbf{V}_{\mathrm{m}}(t) = \mathbf{R}_{\mathrm{m}}\mathbf{i}_{\mathrm{m}}(t) + \mathbf{L}_{\mathrm{m}}\frac{\mathrm{d}\mathbf{i}_{\mathrm{m}}}{\mathrm{d}\mathbf{t}}(t) + \mathbf{K}_{\mathrm{e}}\mathbf{\omega}_{\mathrm{m}}(t).$$
(12)

Whereas,

$$\mathbf{i}_{\mathrm{m}} = \frac{\mathbf{T}_{\mathrm{m}}}{k_{\mathrm{f}}} \tag{13}$$

Where, V_{m} is the motor voltage, R_{m} is the armature resistance of the motor, i_{m} is the motor current, L_{m} is the inductance of the motor, k_{t} is the torque constant of the motor, ω_{m} is the motor angular velocity and T_{m} is the torque of the motor. For DC motors, the torque and electrical constants, k_{e} and k_{t} are equal Taking the Laplace transform with zero initial condition, we obtain

$$\mathbf{V}_{\mathrm{m}}(\mathbf{s}) = \mathbf{R}_{\mathrm{m}} \frac{\mathbf{T}_{\mathrm{m}}}{\mathbf{K}_{\mathrm{m}}}(\mathbf{s}) + \mathbf{L}_{\mathrm{m}} \mathbf{s} \frac{\mathbf{T}_{\mathrm{m}}}{\mathbf{K}_{\mathrm{m}}}(\mathbf{s}) + \mathbf{K}_{\mathrm{m}} \boldsymbol{\omega}_{\mathrm{m}}(\mathbf{s})$$
(14)

The unbalanced torque on a body along axis of rotation determines the rate of change of the body's angular momentum,

$$\mathbf{T} = \frac{\mathrm{dl}}{\mathrm{dt}} \tag{15}$$

Where] is the angular momentum vector, T is the torque and t is time. For rotation about a fixed axis,

$$\mathbf{l} = \mathbf{J}\boldsymbol{\omega} \tag{16}$$

Where J is the moment of inertia and ω is the angular velocity. It follows that

$$\mathbf{T} = \frac{\mathrm{dl}}{\mathrm{dt}} = \frac{\mathrm{d}(\mathrm{j}\omega)}{\mathrm{dt}} = \mathbf{J}\frac{\mathrm{d}\omega}{\mathrm{dt}}$$
(17)

The frictional force, F, is proportional to the object's velocity, \mathbf{v} , giving the relationship. $\mathbf{F} = -\mathbf{B}\mathbf{v}$, where **B** is the frictional drag. Relating this equation to rotational motion results in

$$\mathbf{T} = -\mathbf{B}\boldsymbol{\omega} \tag{18}$$

Torque, is proportional to the armature current i by a constant factor \mathbf{k}_{e} as defined in (7)

$$\mathbf{T} = \mathbf{k}_{\mathbf{e}}\mathbf{i} \tag{19}$$

Applying Newton's second law of motion, it follows that the torque, T, as defined in equation (17), (18) and (19) for a motor, m becomes;

$$J_{m}\frac{d\omega_{m}}{dt} = T - B_{m}\omega_{m}$$

(20)

Where, J_m is the moment of inertia of the motor and \mathbb{B}_m is the viscous friction coefficients. Taking the Laplace transform with zero initial condition, we obtain,

$$\mathbf{T}_{m} = \mathbf{J}_{m} \mathbf{s} \boldsymbol{\omega}_{m}(\mathbf{s}) + \mathbf{B}_{m} \boldsymbol{\omega}_{m}(\mathbf{s})$$
(21)

Substituting into equation (14) we obtain,

$$\frac{\omega_{\rm m}}{v_{\rm m}} = \frac{\kappa_{\rm m}}{(\kappa_{\rm m} + L_{\rm m} \circ) (J_{\rm m} \circ + E_{\rm m}) + \kappa_{\rm m}^2}$$
(22)

This is the transfer function for the motor.

Similarly, electric circuit of the alternator, a, is shown in Figure 7.



Figure 7: Alternator model

Applying Kirchhoff's voltage law, the voltage definition is similar to that of the motor, equation (12), but with alternator definitions as follows,

$$K_{a}\omega_{a} = R_{a}i_{a}(t) + L_{a}\frac{di_{a}}{dt}(t) + v_{a}(t)$$
(23)

Applying Newton's second law of motion, the torque, T, for the alternator as defined by equation (17), (19), (20) and (21) in Laplace domain we have,

$$\frac{\mathbf{v}_{a}}{\omega_{a}} = \frac{\mathbf{K}_{a}^{\Xi} - (\mathbf{R}_{a} + \mathbf{L}_{a}s)(\mathbf{J}_{a}s + \mathbf{B}_{a})}{\mathbf{K}_{a}}$$
(24)

Equation (24) gives the transfer function for the alternator.

For amplification purposes, a relationship between the motor and the alternator is achieved by introducing gears as the coupling unit for the motor-alternator assembly. The Figure 8 below is used to derive the relationship between voltage entering the motor, gear ratio and voltage leaving the alternator.



Figure 8: Voltage relationship

The gear ratio, $\mathbf{G}_{\mathbf{r}}$ expresses the ratio of the frequency of the motor shaft to the frequency of the alternator shaft. Thus, we can multiply the frequency $\mathbf{f}_{\mathbf{rrr}}$ of the motor shaft (the input) with the gear ratio to find the frequency $\mathbf{f}_{\mathbf{s}}$ of the alternator rotor (the output). We can calculate as follows,

$$\mathbf{f_a} = \mathbf{G_r} \ \mathbf{f_m} \tag{25}$$

The relationship between angular speed of the shaft and the frequency [15] is given by

$$\omega = \frac{2\pi}{t} = 2\pi i \tag{26}$$

Where, \mathbf{u} is the angular speed measured in radians per second, \mathbf{t} is the period measured in seconds, \mathbf{f} is the ordinary frequency measured in hertz.

The transfer function from the input armature voltage to the resulting voltage of the alternator is found by using equations, (22), (23), (25) and (26). We obtained the transfer function of the DC motor-gear-alternator system as

$$\frac{\mathbf{v}_{a}}{\mathbf{v}_{m}} = \mathbf{G}_{r} \left[\frac{\mathbf{k}_{m}}{\mathbf{k}_{a}} \frac{\mathbf{k}_{a}^{2} - (\mathbf{J}_{a} \mathbf{s} + \mathbf{B}_{a})(\mathbf{R}_{a} + \mathbf{L}_{a} \mathbf{s})}{(\mathbf{R}_{m} + \mathbf{L}_{m} \mathbf{s})(\mathbf{J}_{m} \mathbf{s} + \mathbf{B}_{m}) + \mathbf{k}_{m}^{2}} \right]$$
(27)

For this system \mathbf{k}_{m} and \mathbf{k}_{a} are approximately equal, hence,

$$\frac{\mathbf{V}_{\mathbf{z}}}{\mathbf{V}_{\mathbf{m}}} = \mathbf{G}_{\mathbf{r}} \left[\frac{\mathbf{k}^{2} - (\mathbf{J}_{\mathbf{z}}\mathbf{s} + \mathbf{B}_{\mathbf{z}})(\mathbf{R}_{\mathbf{z}} + \mathbf{L}_{\mathbf{z}}\mathbf{s})}{(\mathbf{R}_{\mathbf{m}} + \mathbf{L}_{\mathbf{m}}\mathbf{s})(\mathbf{J}_{\mathbf{m}}\mathbf{s} + \mathbf{B}_{\mathbf{m}}) + \mathbf{k}^{2}} \right]$$
(28)

or

$$G(s) = G_{r} \left[\frac{-J_{a} L_{a} s^{2} - (J_{a} R_{a} + B_{a} L_{a}) s - (B_{a} R_{a} - k^{2})}{J_{m} L_{m} s^{2} + (J_{m} R_{m} + B_{m} L_{m}) s + (B_{m} R_{m} + k^{2})} \right]$$
(29)

Equation (29) gives the transfer function of motor-gear-alternator system.

3.0 Simulink Model of the Motor-Gear- Alternator System:

By implementing equations (29) in a block diagram, the Simulink model for the system shown in Figure 9 is obtained.



Figure 9: Simulink model of DC Motor-Gear- Alternator System

The model is complete. We simply need to supply the proper input and define the output of interest. The input to the system is the voltage supplied to the DC motor. The output of the system, which we will observe and ultimately try to control, will be the voltage of the alternator.

3.1 Running the model:

The design parameters are the R_m armature resistance of the motor, R_a Armature Resistance of alternator, L_m inductance of the motor, L_a Inductance of the alternator, B_m viscous friction coefficients of the motor, B_a viscous friction coefficients of the alternator, K_m torque constant of the motor, K_a torque constant of the alternator and the G_r gear ratio. Before running the model, we need to assign numerical values to each of the variables used in the model. For the MGA system, we assume the following values in table 1.

Table 1: Specification of the MGA Parameters used for the experiment

No	Parameter description(units)	Motor values	Alternator values			
1.	Gear ratio	1				
2.	Armature Resistance (Ω)	1	1			
3.	Inductance(H)	0.5	0.5			
4.	Viscous friction coefficients (Nm/(rad/s))	0.1	0.1			
5.	Moment of inertial (kgm ²)	0.01	0.01			

3.2 Results and discussion:

When the simulation is run the voltage output is as shown in figure 10.



Figure 10: Voltage response of our model using the initial parameter values

Figure 10 shows the voltage response of our model using the initial parameter values in the model with a unit input voltage. Figure 11 show the required step response. It is obvious that we need to introduce a tuning controller. The Ziegler–Nichols step response method is based on the idea of tuning controllers based on simple features of the step response [16]. In his paper the idea is investigated from the point of view of robust loop shaping. The results are insight into the properties of PI and PID control and simple tuning rules that give robust performance for processes with essentially monotone step responses.



Figure 11: Typical 2nd Order Step Response and Transient Characteristics[17]

We can easily compare the effect of each of the PID parameters on the closed-loop dynamics and demonstrate how to use a PID controller to improve the system performance. The PID controller works in a closed loop system using the schematic shown in figure12. The variable (ϵ) represents the tracking error, the difference between the desired input value (r) and the actual output (y). This error signal (ϵ) will be sent to the PID controller, and the controller computes both the derivative and the integral of this error signal. The control signal (u) to the plant is equal to the proportional gain (K_p) times the magnitude of the error plus the integral gain (K_i) times the integral of the error.



Figure 12: Unity feedback system [18]

The Simulink block with PID controller is shown in figure 13.



When the Simulink figure 13 is run using numerical values of table1, the output is shown in figure14 a



Figure 14: Step Response with PID Controllers.

For this set up, K_p , K_i and K_d controllers having gains of 1000,1000 and 350 respectively were used. Figure 14 b, c and d shows the closed loop step voltage response of the actual and estimated model for the PID controllers. It can be observed that the proportional controller K_p reduces the rise time, increase the overshoot, and reduces the steady-state error. An integral controller K_i decreases the rise time, increases both the overshoot and the settling time, and eliminates the steady-state error, while the derivative controller K_d reduced both the overshoot and the settling time, and had a small effect on the rise time and the steady-state error.

Conclusion:

In this study, detailed mathematical derivations from first principles have been presented and then represented the derived equations within Simulink. The model is then tested using some numerical values (assumed value). Comparative study of MGA model for optimal performance using proportional controller, integral controller and derivative controller was done. It is observed that PID controller rectify the overall performance of system and it improves transient as well as steady state response.

The effects of each of controller parameters, K_{p} , K_{i} and K_{d} on a closed-loop system are summarized in the table 2.

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Table 2: Table of different values of PID parameters

Controller	Rise Time	Overshoot	Settling Time	S-S Error
K _p	Decrease	increase	Small Change	Decrease
K _i	Decrease	Increase	Increase	Eliminate
K _d	Small Change	Decrease	Decrease	No Change

There is work underway on parameter identification and stability analysis of the MGA system for practical applications.

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DEFINITION, ACRONYMS AND ABBREVIATIONS

ODE: Ordinary Differential Equation

- DC: Direct Current
- AC: Alternating Current
- $\boldsymbol{\mathsf{R}}_{\mathbf{m}}$ Armature Resistance of the Motor
- R_a Armature Resistance of alternator
- im Motor current
- ia Alternator current
- V_m Motor Voltage
- Va Alternator Voltage
- L_m Inductance of the motor
- L_a Inductance of the alternator
- J_m Moment of inertial of motor
- Ja Moment of inertial of alternator
- $\boldsymbol{\Theta}_{\mathbf{m}}$ Angular displacement of motor
- B_a Angular displacement of alternator
- ω_m Motor angular velocity
- ω_a Alternator angular velocity
- T_m Torque of motor
- T_a Torque of alternator
- $\mathbf{B}_{\mathbf{m}}$ Viscous friction coefficients of the motor
- **B**_a Viscous friction coefficients of the alternator
- K_m Torque Constant of the motor
- K_a Torque Constant of the alternator

DEFINITION OF TERMS

Rise time is the amount of time it takes to first reach the new steady-state value. Typically, these values are 10% and 90% of the input step size.

Overshoot is the distance between the first peak and the new steady state. This is usually expressed as the overshoot ratio.

Settling time is the time elapsed from the application of an ideal instantaneous step input to the time at which the output has entered and remained within a specified error band (typically within 2 % or 5% within the final value).

Steady-state error is the difference between the desired final output y_{des}^{ss} and the actual response when the system reaches a steady state (y_{ss}), when its behavior may be expected to continue if the system is undisturbed.

Torque

Torque	is	а	measure	of	the	tendency	of	а	force	to	rotate	an	object	about	some	axis	[19].
Torque = Force × Distance										(30)							

The SI unit of force is the newton, and the unit of distance is meters. Since torque is the product of force and distance, the unit of torque is newton-metres.

Newton's Second law

Newton's Second Law states that the acceleration of an object is directly proportional to the net force acting on it, and inversely proportional to its mass [19]. This can be expressed by the equation, F = ma(31)

Gear Ratios and Torque

The gear ratio, $\mathbf{G}_{\mathbf{r}}$, is the ratio of the number of teeth on the output gear to the number of teeth on the input gear [19]. The gear ratio expresses the ratio of the output torque to the input torque. Thus, we can multiply the torque supplied at the motor shaft (the input) by the gear ratio to find the torque at the alternator axle as follows,

 $Alternator Torque = Motor Torque \times G_r$ (32)

Electricity Generation

Electricity generation is the process of generating electrical power from other sources of primary energy [19]. Turbines are used to spin the magnets inside the generator and different kinds of power plants get that energy from different sources. In a hydroelectric station, falling water is used to spin the turbine, in nuclear stations and in thermal generating stations powered by fossil fuels, steam is used. A wind turbine uses the force of moving air. Figure below is an example of such a generator.



Figure 15: Hydroelectric turbine generator[20]

Motor

A motor is an electrical machine that converts electrical energy into mechanical energy [21]. The first electric motors were simple electrostatic devices created by the Scottish monk Andrew Gordon in the 1740s. The theoretical principle behind production of mechanical force by the interactions of an electric current and a magnetic field, Ampere's force law, was discovered later by André-Marie Ampere in 1820 [22].





Figure 16: DC motor[20]

Alternator

An alternator is an electrical generator that produces alternating current [20]. Dynamos were the first electrical generators capable of delivering power for industry, and the foundation upon which many other later electric power conversion devices were based, including the electric motor, the alternating-current alternator, and the rotary converter. Today, the simpler alternator dominates large scale power generation, for efficiency, reliability and cost reasons.



Figure 17: Alternator