Geoelectrical investigation of soils as foundation materials in Umudike area of Abia State, Southeastern Nigeria

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Geoelectrical investigation of soils in Umudike area of Abia State was undertaken in order to determine the competence of the soils as foundation materials. A total of 18Vertical Electrical Sounding (VES), using Schlumberger configuration was carried out. The results revealed three to six distinct geoelectric sequences with resistivities ranging from about 8Ω m to about $38,000\Omega$ m and a variation in topsoil thicknesses with the least as 0.2m at vicinity of VES Station 2 Ahiaeke and the highest as 5.0m at VES Station 14 MOUAU. The topsoils are composed of sands, silts, sandy clays, clays and laterites. The study also revealed the cause of frequent cracking and collapse of a portion of the Umuahia-Ikot-Ekpene road. Based on the results of the survey, the most competent soils within which large civil engineering structures will be founded within the study area are VES 8,9 (inside ABSU), 6 (opposite GCU), 14 and 15 (inside MOUAU).

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Key words: Electrical Resistivity, Foundation failure, Competent soils, Geoelectric layer.

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INTRODUCTION

- The use of shallow geophysical methods of investigation in civil and construction engineering
- for road and building construction and evaluation, dam safety, and solution of related problems;
- engineering and environmental geophysics is defined as geotechnical geophysics (Sheriff, 2001).
- 25 High rising buildings are among large civil engineering structures that are subjected to strong
- 26 dynamic and static loads; and since the statistics of failures of building structures throughout the
- 27 nation has increased geometrically; therefore the design and construction should be preceded by
- adequate investigation in order to prevent such failures. These failures have been attributed to a
- 29 number of factors such as inadequate information about the soil and the subsurface geological
- 30 material, poor foundation design and poor building materials.
- 31 The need for pre-foundation studies is therefore necessary in order to prevent loss of valuable
- 32 lives and properties that always accompany such failure.
- Foundation study usually provides subsurface information that normally assists civil engineers in
- 34 designing the foundation of civil engineering structures. This is because some earth materials due
- 35 to their nature cannot support solid and rigid structures; among these materials are clays and
- 36 clay-bearing earth.
- 37 Similarly, earth materials such as sands and fresh basement rock provide firm support for solid
- 38 foundation.
- To this end, geophysical methods together with or besides other geotechnical approaches are
- 40 routinely used for foundation investigation (Ajayi et al., 2005; Akinrinmade, 2013; Akintorinwa,
- 41 2009; Tabwassah and Obiefuna, 2012).
- 42 Geophysical methods such as the Electrical Resistivity (ER), Seismic Refraction,
- 43 Electromagnetic (EM), Magnetic and Ground Penetrating Radar are used singly or in

- combinations for engineering site investigation (Olorunfemi and Meshida, 1987; Fatoba et al., 44
- 2010; Hunter et al., 2011; Melikan, 1960; Olorunfemi et al, 2000, 2004; Oluwakemi and 45
- Michael, 2011). The applications of such geophysical investigation are in the determination of 46
- layer thickness, depth to bedrock, structural mapping and evaluation of subsoil competence. 47
- The need to provide information in the subsurface sequence and structure disposition necessary 48
- for foundation design necessitated a geoelectrical investigation of the soils of Umudike area and 49
- environs as foundation materials. 50

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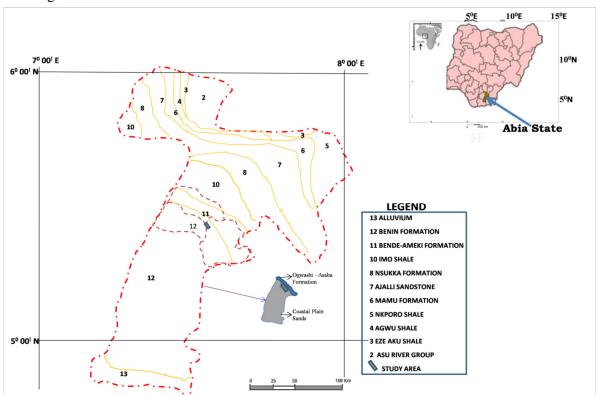
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Geologically, there are about 11 different formations in Abia State of Nigeria, and the selected study area (Umudike and its environs) falls within the transition zone of Ogwashi-Asaba Formation and Coastal plain sands (Fig. 1).

Within a transition zone, there are at times abrupt or gradual changes in lithology; therefore a complex overall situation with respect to defining the competence of near-surface formation as

57 foundation materials could arise in future as a result of attempts in the construction of high rising

buildings. 58



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Fig. 1: Geologic map of Abia State of Nigeria showing the study area (Modified after GSN, 1985).

- 62 Ogwashi-Asaba Formation and Coastal Plain Sands are situated in the Cenozoic Niger Delta 63
- The Cenozoic Niger Delta is situated at the intersection of the Benue Trough and the South 64
- Atlantic Ocean where triple-R junction (rift system) developed during the break-up of Gondwana 65
- leading to the separation of the continents of South America and Africa in the Late Jurassic. The 66

- 67 third arm of the rift after extending to about 1000km northeast from the Gulf of Guinea to Lake
- 68 Chad failed (aulacogen), thus forming the Benue Trough.
- 69 Subsequently sediments from weathering of the basement uplift were deposited into the trough
- 70 through rivers and lakes by Early Cretaceous. By Mid-Cretaceous onwards Marine sedimentation
- 71 took place in the Benue Trough; thus making it possible in conjunction with other geologic
- events for it to be presently underlain by diverse sedimentary basins.
- 73 The Benue Trough is arbitrarily divided into the Lower, the Middle and the Upper Benue
- 74 Trough; and by Santonian times the area underwent intense folding and compression forming
- 75 many anticlines and synclines.
- After the Santonian-Campanian tectonism which formed the Abakiliki anticlinorium, the western
- margin of the Lower Benue Trough subsided, and the corresponding synclinorium became the
- Anambra basin where over 2500m of deltaic complexes accumulated. However by Eocene, the
- 79 inception of Tertiary Niger Delta Basin commenced. Thus, the Late Cretaceous deltaic
- sedimentation in the Anambra Basin was followed by the shift in deltaic deposition southward
- and consequently the construction or outbuilding of the Niger Delta took place. The interplay
- between subsidence and deposition arising from a succession of sea transgressions and
- regressions (Hospers, 1965) gave rise to the deposition of three lithostratigraphic units in the
- Niger Delta (Short and Stauble, 1967). These units are Marine Akata Formation, Paralic Agbada
- 85 Formation, and the Continental Benin Formation. The delta has prograded a distance greater than
- 250km from the Benin and Calabar flanks to the present delta front. Average thickness of
- sediments in the Niger-Delta is about 12,000m with an area of about 140,000km² (Obaje, 2009).
- 88 Ogwashi-Asaba Formation was grouped as the upper member of the Bende-Ameki (Agbada
- 89 Group) Formation (Short and Stauble, 1967). In the grouping, the coastal plain sands of
- 90 (Reyment, 1965) were referred to as Benin formation (Table 1).

Table 1: Stratigraphic correlation chart of eastern Niger Delta outcrops and their subsurface equivalents (Short and Stauble, 1967)

YOUNGEST KNOWN AGE		OLDEST KNOWN AGE	YOUNGEST KNOWN AGE		OLDEST KNOWN AGE
RECENT	BENIN FORMATION Afam Shale Member	OLIGOCENE	PLIO/ PLEISTOCENE	BENIN FORMATION	MIOCENE?
RECENT	AGBADA FORMATION	EOCENE	MIOCENE	OGWASHI-ASABA FORMATION AMEKI FORMATION	OLIGOCENE EOCENE
RECENT	AKATA FORMATION	EOCENE	L. EOCENE	IMO SHALE FORMATION	PALEOCENE
			PALEOCENE	NSUKKA FM	MAESTRICHTIAN
EQUIVALENTS NOT KNOWN			MAESTRICHTIAN	AJALI FORMATION	MAESTRICHTIAN
			CAMPANIAN	MAMU FORMATION	CAMPANIAN
			CAMP./MAEST.	NKPORO SHALE	SANTONIAN
			CONIACIAN/ SANTONIAN	AWGU SHALE	TURONIAN
			TURONIAN	EZE AKU SHALE	TURONIAN
			ALBIAN	ASU RIVER GROUP	ALBIAN

While (Amajor, 1986) grouped the Ogwashi-Asaba Formation as the lower member of the Benin Formation, and the coastal plain sands as the upper member (Table 2).

Ogwashi-Asaba Formation is predominantly sandy with alternating lignite seams and a few beds of clay with sparse marine fauna (Reyment, 1965; Short and Stauble, 1967).

The Coastal plain sands are predominantly yellow and white sands alternating with pebbly layers and a few clay beds (Reyment, 1965).

The formation comprises of shale/sand sediments with intercalation of thin clay beds (Asseez, 100 1976; Murat, 1972).

The sands are mostly medium to coarse grained, pebbly, moderately sorted with local lenses of poorly cemented sands and clays. Petrographic analysis indicates that the composition of the rocks is as follows: 95-99% Quartz grains, 1-2.5% of Na+K-mica (Onyeagocha, 1982).

Table 2: Stratigraphic correlation chart of the Niger Delta (After Amajor, 1986)

AGE	SURFACE OUTCROP EQUIVALENT FORMATIONS	SUBSURFACE FORMATIONS	MEGA-DEPOSITIONL ENVIRONMENTS
PLIOCENE- RECENT	COASTAL PLAIN	BENIN FM	PARALIC
MOCENE	OGWASHI' JJEBU ASABA FM	BETT AFAM CLAY MBR	CONTINENTAL PLAIN
EOCENE RECENT	AMEN ILAROM	AGBADA FM	PARALIC FRONT DELTA
PALEOCENE	INO EMEKORO	AKATA	MARINE
CAMPANIAN- MAASTRICH- TIAN SANTONIAN	NSUKKA FM AJALI SST MAMU FM NKPORO-ENUGU SHALE		UPPER CRETACEOUS PRO NIGER DELTA- SUCCESSION

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The selected study area (Umudike and its environs) is located within the central parts of

Ikwuano-Umuahia area; and lies within latitudes 5 28° 793'N and 5 34° 661'N, and longitudes 7

116 31⁰ 602'E and 7 34⁰ 661'E (Fig 2).

117 Climate of the area is the sub-equatorial climatic belt with tropical rain-forest vegetation. The

mean annual temperature is between 24°C and 27°C; while the annual rainfall varies between

119 1500mm and 3500mm (Leong, 1978).

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- Institutions and research centres such as Forestry Research Institute, New Industrial Market, Soil
- and Water Department of Federal Ministry of Agriculture and Rural Development, and
- Government College Umuahia (GCU) are situated within the study area.
- Others are Abia State University Practical Agricultural Campus (ABSU), National Root Crops
- Research Institute(NRCRI) and Michael Okpara University of Agriculture(MOUAU).
- The area is witnessing rapid increase in population and subsequently expansion in infrastructure.
- 127 It is known that rapid industrialization, urbanization and population growth have attendant
- pressure on all sustainable resources.
- This has led to many geophysical groundwater investigations in the area but not much have been
- done in the area of foundation investigations.
- The land is fixed but there is daily increase in infrastructure. Also, the reduction in available land
- due to increasing infrastructure will eventually give rise to the need of optimally using the
- available ones for sustainable practices.

In light of this, Umudike area and its environs are gradually being faced with the consequent attempts in the construction of high rising buildings

It is therefore essential to assess the foundation competence of the near-surface soil and subsurface geological materials.

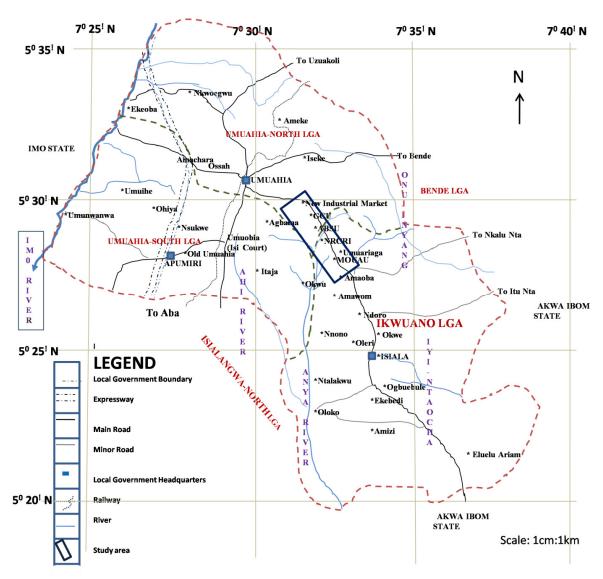


Fig. 2: Map of Ikwuano-Umuahia area of Abia State showing the study area

METHODOLOGY

The instruments used in the geoelectrical survey include resistivity meter (ABEM Terrameter), Geographic Positioning System (GPS), 12Volts heavy duty motor battery with two connecting wires with crocodile clips, four hammers and four electrodes with rolls of wire, two rolls of 100m rope each, Three rods for ropes (one central and two end ones), One big umbrella for shade, Data sheets with K-values and writing pen.

Six traverses were established across the study area (Fig. 3). Three (3) Vertical Electrical Sounding (VES) stations were occupied along each of the traverses and a total of 18 soundings were carried out using the Schlumberger electrode configuration of maximum half current electrodes spacing (AB/2) of 65m (Table 3, Fig. 4).

Table 3: VES stations and their localities in the study area

Data	Data Location	GPS Reading		
Number		Elevation	Latitude °N	Longitude °E
		(m) a.m.s.l		
1	Umuohu-Azueke (Ministry of	(186.5m)	5 ⁰ 34.623 [!] N	7 ⁰ 34.661 [!] E
	Agriculture)			
2	Umuohu-Azueke (New Industrial	(135.4m)	5 ⁰ 30.558 [!] N	7 ⁰ 32.004 [!] E
	Market)			
3	Umuohu-Azueke (New Industrial	(148.9m)	5 ⁰ 30.318 [!] N	7 ⁰ 31.602 [!] E
	Market)			
4	Umuohu-Azueke (Government	(131.5m)	5°30.134 [!] N	7 ⁰ 32.233 [!] E
	College Umuahia)			
5	Umuohu-Azueke (Government	(151.2m)	5°30.070 [!] N	7 ⁰ 32.268 [!] E
	College Umuahia)			
6	Umuohu-Azueke (Igbugbo Opposite	(162.5m)	5°34.645! N	7 ⁰ 32.564 [!] E
	GCU)			
7	Umudike (Ihiuzo American Quarters	(147.0m)	5°29.560! N	7 ⁰ 32.323 ¹ E
2	Plantation)	(12= 0)	7020 (17)27	=000 =01
8	Umuohu-Azueke (Abia State	(137.9m)	5 ⁰ 28.645 [!] N	7 ⁰ 33.721 [!] E
0	University)	(122.0.)	5020 722 1	7022 224 5
9	Umuohu-Azueke (Behind Abia State	(123.0m)	5 ⁰ 29.732 [!] N	7 ⁰ 32.334 [!] E
10	University)	(100.5.)	5 ⁰ 33.232 [!] N	7 ⁰ 26.131 [!] E
10	Umudike (Inside NRCRI)	(108.5m)		
11	Umudike (Inside NRCRI)	(107.5m)	5°28.859! N	7 ⁰ 32.432 [!] E
12	Umudike (V.C'S Lodge)	(126.3m)	5 ⁰ 29.312 [!] N	7 ⁰ 32.761 [!] E
13	Umuariaga (Opposite MOUAU)	(129.4m)	5°28.881 N	7 ⁰ 33.052 [!] E
14	Umudike (Inside MOUAU)	(113.3m)	5 ⁰ 28.793 [!] N	7 ⁰ 32.433 [!] E
15	Umudike (Behind MOUAU)	(108.5m)	5 ⁰ 33.232 [!] N	7 ⁰ 26.131 [!] E
16	Amaoba	(199.4m)	5 ⁰ 29.421 [!] N	7 ⁰ 32.445 [!] E
17	Amaoba	(172.7m)	5 ⁰ 29.633 [!] N	7 ⁰ 32.544 [!] E
18	Amaoba	(190.1m)	5 ⁰ 29.655 [!] N	7 ⁰ 32.632 [!] E

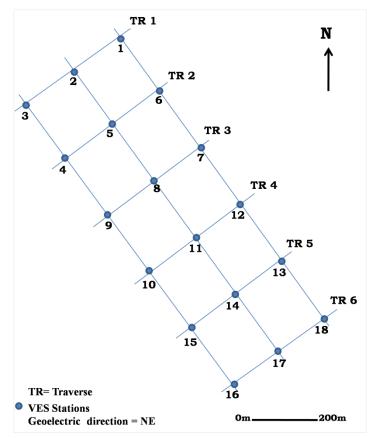


Fig. 3: Data acquisition grid of the study area showing the vertical electrical sounding stations

The 12V direct current (DC) served as current source to the Terrameter, and the current was passed into the subsurface through the two current electrodes 'AB'; while the two potential electrodes 'MN' were linearly arranged along the survey line to determine the ground potential difference (Fig. 4).

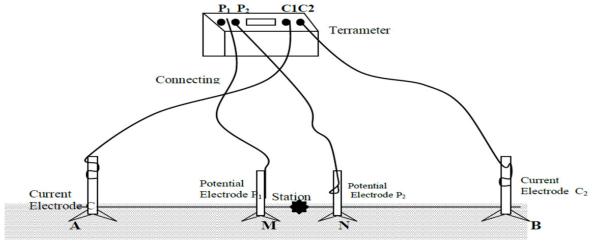


Fig. 4: Schematic diagram of the Schlumberger electrode configuration used.

- 167 The resultant ratio of the current and voltage is the measured data which is the ground resistance
- read off in the Terrameter.
- This ground resistance is used in computing the apparent resistivity using the corresponding k-
- values with the formula:

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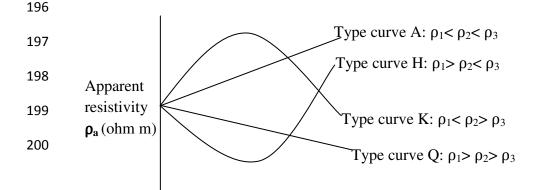
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- 171 $\rho a = kR \qquad \dots \text{ equation (1)}$
- where ρ_a = Apparent resistivity, $k = \pi \left(\frac{L^2 l^2}{2l}\right)$ = Geometric factor, R = Resistance in ohms
- L = AB/2 = Half current electrode spacing (m), l = MN/2 = Half potential electrode spacing (m).
- Substituting the values of k into equation (1), we get
- $\rho a = \pi R \left(\frac{L^2 l^2}{2l} \right) \qquad \dots \text{ equation (2)}$
- 178 The apparent resistivity values were plotted against electrode spacing (AB/2) on a bi-logarithmic
- graph sheet to generate depth sounding curves. The curves were then inspected visually for
- identification of the curve types; and subsequently used for the conventional partial curve
- matching technique and use of auxiliary point diagrams (Zohdy, 1989). From the result,
- estimates of the resistivity and thickness of the various geoelectric layers were obtained and used
- for computer iteration using RESIST version 1.0 software (Varder -Velper, 1988).
- Finally, interpreted results were used for the analysis of sounding curves and preparation of
- 185 geoelectric sections.

RESULTS AND DISCUSSION

4.1.1 Analysis of Sounding Curve

- 190 Table and curves for vertical electrical sounding over layered structures is a function of the
- electrode configuration together with the resistivities and thicknesses of the layers (Orellana and
- Mooney, 1966; Zohdy, 1989; Amos-Uhegbu et al., 2012). Sounding (VES) curves are obtained
- by plotting the calculated apparent resistivity against the corresponding half current electrode
- separation (AB/2), and the letters Q,A,K and H are used to indicate the variation of resistivity
- with depth (Fig. 5).



Electrode Spacing AB/2 (m)

Fig. 5: Schematic diagram of resistivity type curves for layered structures.

Fourteen curve types were identified within the study area, and the number of layers varies between three layers and six layers with five-layered type curves predominant. Resistivity type curves for some locations in the study area are as displayed (Fig. 6 to Fig. 9). While, Table 4 is a profile of the VES data and location points in the study area.

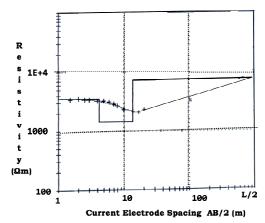


Fig. 6: Resistivity curve of VES 6 (Igbugbo Opposite GCU).

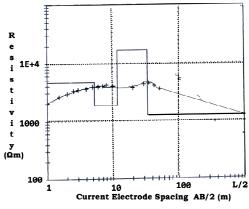


Fig. 7: Resistivity curve of of VES 2 at New Industrial Market.

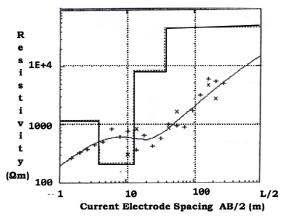


Fig. 8: A computer modelled curve of VES 17 at Amaoba

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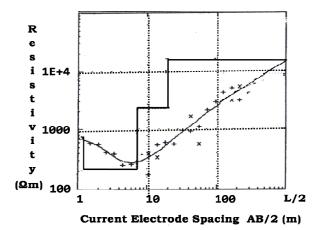


Fig. 9: A computer modelled curve of VES 11 infront of NRCRI

Table 4: A profile of VES data of the various sounding stations in the study area.

VES	Resistivity of	Thickness of	Type
Nos.	layers (Ωm)	layers (m)	Curve
VES	$\rho_1 = 332$	$t_1 = 0.8$	HKH
1	$\rho_2 = 1786.9$	$t_2 = 3.2$	
	$\rho_3 = 1250.9$	$t_3 = 7.0$	
	$\rho_4 = 640.9$	$t_4 = 16.7$	
	$\rho_5 = 3200.8$	$t_5 = ?$	
VES	$\rho_1 = 563$	$t_1 = 0.2$	AKQ
2	$\rho_2 = 1720.0$	$t_2 = 5.1$	
	$\rho_3 = 4680$	$t_3 = 6.4$	
	$\rho_4 = 1250$	$t_4 = 22.2$	
	$\rho_5 = 570$	$t_5 = ?$	
VES	$\rho_1 = 187.7$	$t_1 = 0.6$	AK

3	$\rho_2 = 1626.3$	$t_2 = 4.8$	
	$\rho_3 = 4867.6$	$t_3 = 15.1$	
	$\rho_4 = 231.7$	$t_4 = ?$	
VES	$\rho_1 = 140.6$	$t_1 = 0.8$	HAA
4	$\rho_2 = 8.3$	$t_2 = 1.8$	
	$\rho_3 = 226.5$	$t_3 = 1.4$	
	$\rho_4 = 7147.3$	$t_4 = 22.2$	
	$\rho_5 = 10197.5$	$t_5 = ?$	
VES	$\rho_1 = 2200.0$	$t_1 = 0.4$	HA
5	$\rho_2 = 950.0$	$t_2 = 6.5$	
	$\rho_3 = 3630.0$	$t_3 = 25.2$	
	$\rho_4 = 7710.0$	$t_4 = ?$	
VES	$\rho_1 = 3520.0$	$t_1 = 4.2$	Н

6 VES 7 VES 8	$\rho_2 = 1460.0$ $\rho_3 = 7310.0$ $\rho_1 = 114.0$ $\rho_2 = 1105.0$ $\rho_3 = 295.0$ $\rho_4 = 527.0$ $\rho_1 = 575.0$ $\rho_2 = 7370.0$ $\rho_3 = 519.0$	$t_{2} = 13.9$ $t_{3} = ?$ $t_{1} = 1.0$ $t_{2} = 20.9$ $t_{3} = 9.2$ $t_{4} = ?$ $t_{1} = 0.4$ $t_{2} = 2.4$ $t_{3} = 4.7$	KHK
VES 9	$\rho_4 = 12000.0$ $\rho_5 = 68.6$ $\rho_1 = 5104.2$ $\rho_2 = 2568.2$ $\rho_3 = 845.1$	$t_4 = 17.8$ $t_5 = ?$ $t_1 = 3.1$ $t_2 = 28.1$ $t_3 = ?$	Q
VES Nos. VES 10	Resistivity of layers (Ω m) $\rho_1 = 37999.0$ $\rho_2 = 65.4$ $\rho_3 = 666.8$ $\rho_4 = 51.0$ $\rho_5 = 3276.1$	Thickness of layers (m) $t_1 = 0.4$ $t_2 = 0.8$ $t_3 = 2.3$ $t_4 = 6.7$ $t_5 = 12.4$	Type Curve HKHQ
Nos. VES	layers (Ω m) $\rho_1 = 37999.0$ $\rho_2 = 65.4$ $\rho_3 = 666.8$	layers (m) $t_1 = 0.4$ $t_2 = 0.8$ $t_3 = 2.3$	Curve

VES 13	$ \rho_1 = 518.0 $ $ \rho_2 = 878.0 $ $ \rho_3 = 2768.0 $	$t_1 = 0.6$ $t_2 = 15.0$ $t_3 = ?$	A
VES 14	$\rho_1 = 945.0$ $\rho_2 = 3380.8$ $\rho_3 = 21000.0$ $\rho_4 = 7780.0$	$t_1 = 5.0$ $t_2 = 7.0$ $t_3 = 21.5$ $t_4 = ?$	AK
VES 15	$\rho_1 = 4300.0$ $\rho_2 = 3200.0$ $\rho_3 = 400.0$ $\rho_4 = 30000.0$ $\rho_5 = 611.0$	$t_1 = 1.2$ $t_2 = 1.6$ $t_3 = 4.0$ $t_5 = 21.4$ $t_6 = ?$	QHK
VES 16	$ \rho_1 = 14.5 $ $ \rho_2 = 16.5 $ $ \rho_3 = 86875.0 $	$t_1 = 1.2$ $t_2 = 1.6$ $t_3 = ?$	A
VES 17	$\rho_1 = 132.0$ $\rho_2 = 1200.0$ $\rho_3 = 220.0$ $\rho_4 = 8400.0$ $\rho_5 = 46700.0$	$t_1 = 0.6$ $t_2 = 3.0$ $t_3 = 8.6$ $t_4 = 23.4$ $t_5 = ?$	КНА
VES 18	$ \rho_1 = 5130.0 $ $ \rho_2 = 1400.0 $ $ \rho_3 = 176.0 $	$t_1 = 0.6$ $t_2 = 4.5$ $t_3 = ?$	Q

4.1.2 Geoelectric sections of the study area

Subsurface resistivity is related to the physical property of interest such as lithology, porosity,

water content etc; therefore electrical resistivity measurements determine subsurface resistivity

distributions thereby differentiating layers based on resistivity values.

Sounding curves obtained over a horizontally stratified medium could be presented as a

230 descriptive profile displaying variation of apparent resistivity with depth. The profile is a scale

drawing of the successive layer resistivities and thicknesses; so, a geoelectric section is a profile

displaying variation of apparent resistivity with depth (Fig. 10, 11, and 12).

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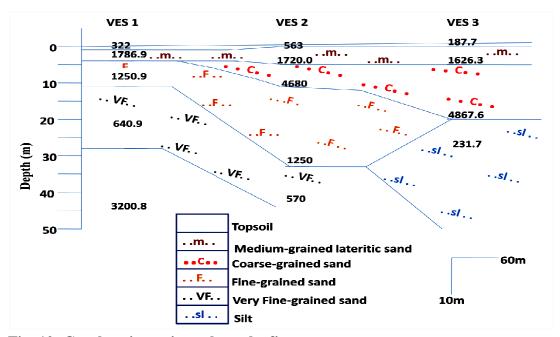


Fig. 10: Geoelectric sections along the first traverse

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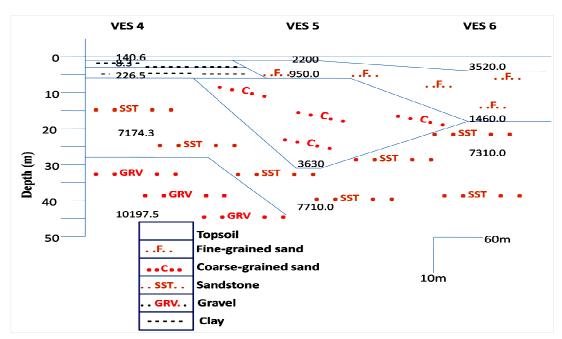


Fig. 11: Geoelectric sections along the second traverse

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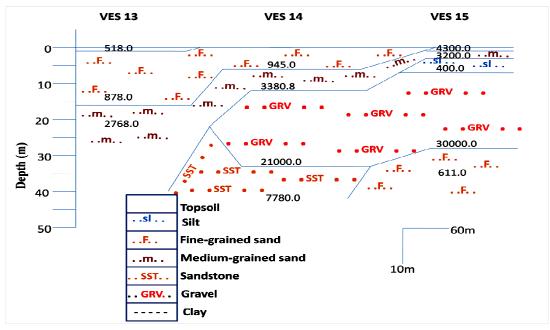


Fig. 12: Geoelectric sections along the fifth traverse

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4.1.3 Subsurface Engineering Evaluation of the Study Area

Excavation for footings or foundation walls shall extend below depth of soil subjected to seasonal or characteristic volume change to undisturbed soil that provides adequate bearing capacity. So, topsoil is normally removed and variations in ground level corrected. Therefore, the best recommended depth of foundation is from 1.0 m to 1.5 m from original ground level (NHBC, 2011). The depth of foundation depends on some factors such as the availability of soil with adequa-

The depth of foundation depends on some factors such as the availability of soil with adequate bearing capacity, depth of shrinkage and swelling as in case of clayey soils, due to seasonal changes which may cause appreciable movements; and the depth of frost penetration in case of fine sand and silt. Also, proximity of excavation and depth of ground water table are considered. Geoelectrical foundation engineering competence of soils can be qualitatively evaluated from

layer resistivity; the higher the value of a layer resistivity, the higher the competence.

Amos-Uhegbu et.al (2012, 2014) extensively worked within the study area and lithologically deduced from drill-hole and geoelectric data that sediments with resistivity < $100\Omega m$ are clays, $100\Omega m$ - $500\Omega m$ are silts, $500\Omega m$ - $1500\Omega m$ are fine-grained sands, $1500\Omega m$ - $3000\Omega m$ are medium-grained sands, $3000\Omega m$ - $5500\Omega m$ are coarse-grained sands, and > $5500\Omega m$ as sandstone.

By using a depth of 1.2m in the evaluation, and from the point of view of the resistivity values; the vicinity of VES 8 is the most suitable site for the construction of high rising building. This is followed by VES station 9, 6, 14 and 15. While the unsuitable sites for the construction of high rising building are VES 4, 10, 11, 12 and 16 (Fig. 13).

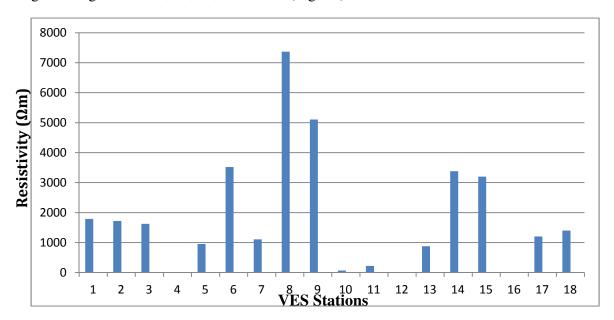


Fig. 13: A histogram of the foundation competence of the subsurface based on resistivity values of the study area

Recall that the higher the value of a layer resistivity, the higher the competence; therefore the lower the value, the lesser the competence. From the resistivity values of topsoils, the vicinity of VES 3, 4, 7, 16 and 17 are poor materials for any structural engineering purpose (Fig. 14). This is evident from the usual cracking and collapse of the portion of road along Umuahia-Ikot-Ekpene highway where the data of VES 17 was acquired.

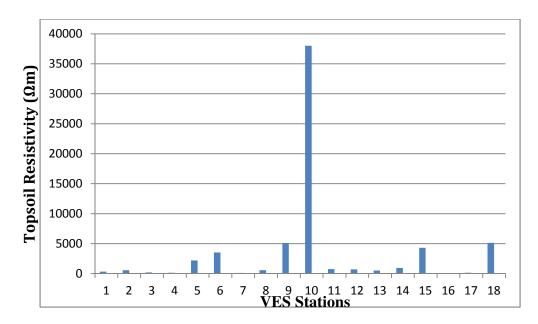


Fig. 14: A histogram of Topsoil resistivity of the study area

CONCLUSIONS

The geophysical results revealed three to six geoelectric sequences within the study area which comprises topsoil, sands, silts, clays and possibly gravel. The thickness of the topsoils range from about 0.2m to about 5.0m; but most are less than 2m. The thickness of the topsoils of the vicinity of VES 6, 9, and 14 are by far greater than 2m probably because construction work have been done in the area and the topsoils must have been removed during the levelling of the area for the construction.

By using the resistivity values together with depth of 1.2m in the evaluation, the vicinity of VES 8, 9, 6, 14 and 15 are suitable for the construction of high rising building; while the unsuitable sites are VES 4, 10, 11, 12 and 16. Also, the vicinity of VES 1, 2, 3, 5, 7, 13, 17 and 18 can be considered for such construction under the supervision of structural and geotechnical experts.

Further foundation investigation using alternative detailed geophysical (seismic) and geotechnical investigations of the area is also recommended.

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